

Figure 4-33. U25 Status Word Format (IEEE Input Parameters)


Figure 4-34. U26 Status Word Format (Cable Correction Parameters)

### 4.9.16 SRQ (M) and Status Byte Format

Purpose To program which conditions will generate an SRQ (service request).

## Format Mn

## Parameters M0 SRQ disabled

M1 Reading overflow
M2 Module input overload
M4 Sweep done
M8 Reading done
M16 Ready
M32 Error
M128 IEEE-488 output done
Default Power-up/DCL/SDC Configuration: Factory default configuration is M0 (SRQ disabled).

Description The SRQ command controls which of a number of conditions will cause the Model 590 to generate an SRQ (service request). Once an SRQ has been generated, the status byte can be checked to determine if the Model 590 was the instrument that generated the SRQ, and, if so, what conditions caused it to do so.

The general format of the SRQ mask used to generate SRQs is shown in Figure 435. By sending the appropriate $M$ command, you can set the appropriate bit or bits to enable SRQ generation if those particular conditions occur. Possible conditions include:

1. An overflowed reading has occurred (M1).
2. The input stage of the CV module is overioaded (M2).
3. A reading sweep has been completed (M4).
4. A single reading is completed (M8).
5. The instrument has processed a command is ready to accept another (M16).
6. An error has occurred (M32). The nature of the error can then be determined by reading the U1 error word as described in paragraph 4.9.15.
7. Any IEEE-488 output sequence has been completed (M128).


Figure 4-35. SRQ Mask and Status Byte Format

## SRQ Timing and Trigger Modes

Timing of SRQ generation depends on the trigger mode and reading rate in effect. Figure 4-36 shows general SRQ timing for the one-shot trigger mode, and Figure $4-37$ shows the general timing for the sweep trigger mode. Keep in mind that these figures are not to scale and show only approximate relationships.


Figure 4-36. SRQ Timing with One-Shot Trigger Mode


Figure 4-37. SRQ Timing with Sweep Trigger Mode

## Status Byte Format

The general format of the status byte is shown in Figure 4-35. Note that all bits except for bit 6 correspond to the bits in the SRQ mask. These bits flag the following conditions.

Reading Overflow (bit 0 )-Set when an overflowed reading has been generated. Cleared when an on range reading is available or requested from the instrument.

Module Overload (bit 1)-Set when the input stage of the selected CV module is in saturation (overloaded). Cleared when the overload condition is eliminated.

Sweep Done (bit 2)-Set when a reading sweep has been completed. Cleared when no sweep has been triggerered or if a sweep is in process.

Reading Done (bit 3)-Set when a reading is ready to be sent over the bus. Cleared by requesting a reading over the bus.

Ready (bit 4)-Set when the unit has processed all commands and is ready to accept additional commands over the bus. Cleared while processing commands.

Error (bit 5)-Set if an error condition occurs. Cleared by reading the U1 error word (paragraph 4.9.15).

RQS (Bit 6)-Set if the Model 590 has requested service via the SRQ line; cleared otherwise.

IEEE-488 Output Done (bit 7)-Set after any IEEE-488 output sequence has been completed. Cleared by initiating an output sequence. Typical output sequences include plot generation and sending data strings.

Programming 1. The status byte should be read once the instrument has generated an SRQ in order Notes to clear the SRQ line.
2. All bits in the status byte will latch when the instrument generates an SRQ.
3. If an error occurs, bit 5 (error) in the status byte will latch and remain so until the U1 word is read (paragraph 4.9.15).
4. Multiple error conditions can be programmed by adding up the individual command values. For example, send M12X for SRQ under sweep done and reading done conditions.
5. A sweep done SRQ will occur (and the sweep done bit in the status byte will be set) only after the programmed number of readings are taken. For pulse and staircase waveforms, the number of readings is defined by the first, last, and step bias voltage parameters. For the DC and external waveforms, the number of readings is defined by the count parameter.
6. At the $1000 / \mathrm{sec}$ reading rate, a reading done $S R Q$ (and setting of the reading done bit in the status byte) will occur only at the end of the sweep.

| Programming | 100UTPUT 7 15; "ME2\%" | ! Program for SRQ on error. |
| :---: | :---: | :---: |
| Examples | 20 OUTFUT $715 ; 4 E 1 \%$ " | ! Attempt to program illegal command. |
|  | sa status $7.2: 5$ | ! Check interface status. |
|  |  | ! Wait for SRQ to occur. |
|  | 50 S SPOLL ( 715 ) | ! Serial poll the instrument. |
|  |  | ! Label the bit positions. |
|  | 76 FOR I $=7$ T0日STEF-1 | ! Loop eight times. |
|  | S0IISFPITCS, ${ }^{\text {P }}$ | ! Display the bit positions. |
|  | 90 HERT I |  |
|  | 100 IIISF |  |
|  |  | ! Program for error status. |
|  | 120 ENTER 715 ; A | ! Get U1 status to clear error. |
|  | 130 IISP A ${ }^{\text {a }}$ | ! Display error status. |
|  | 14 AEND |  |

### 4.9.17 Save and Recall (L)

Purpose To save and recall instrument setups stored in NVRAM.

| Format | Ln,m |
| :--- | :--- |
| Parameters | L0,m Recall configuration \#m $(0 \leq m \leq 7)$ |
|  | L1,m Save configuration \#m $(1 \leq m \leq 7)$ |

Description The L command combines the functions of the front panel SAVE and RECALL keys by allowing the storage or recall of instrument setups. Up to eight instrument configurations can be recalled (0-7) while seven can be saved (1-7).

To save a particular configuration, simply program other operating modes by sending appropriate commands over the bus, then use the L1 command with the number of the position you wish to save. To recall a particular position, send the L0 command along with the number of the position you wish to retrieve.

Programming 1. The instrument assumes save/recall state 1 upon power up or after receiving a Notes DCL or SDC command over the bus.
2. Recall state 0 is permanently stored in ROM and cannot be altered by save.
3. The following modes can be saved and recalled:

Range (R)
Frequency ( F )
Filter (P)
Rate (S)
Zero (Z)
Trigger source and mode (T)
Bias on or off ( N )
Waveform type and times (W)
Bias voltage parameters (V)
4. Recall state 0 returns all units to 100 kHz frequency, including $590 / 1 \mathrm{M}$ models.

### 4.9.18 Measure and Assign Cable Parameters (I)

Purpose To perform the driving point method of cable correction, and to program parameters associated with the matrix and standards methods of cable correction.

## Formats In(,parameters)

Parameters $\quad 10$ Measure cable parameters (driving point)
$\mathrm{I} 1, \mathrm{n} 1, \mathrm{n} 2, \mathrm{n} 3, \mathrm{n} 4$ Assign cable parameters: $\mathrm{K} 0(\mathrm{n} 1+\mathrm{jn} 2), \mathrm{K} 1(\mathrm{n} 3+\mathrm{jn} 4)$
$\mathrm{n} 2, \mathrm{n} 1, \mathrm{n} 2, \mathrm{n} 3, \mathrm{n} 4, \mathrm{n} 5, \mathrm{n} 6, \mathrm{n} 7, \mathrm{n} 8$ Assign test OUTPUT matrix parameters:
$A(n 1+j n 2), B(n 3+j n 4), C(n 5+j n 6), D(n 7+j n 8)$
I3, n1,n2,n3,n4,n5,n6,n7,n8 Assign test INPUT matrix parameters:
$A(n 1+j n 2), B(n 3+j n 4), C(n 5+j n 6), D(n 7+j n 8)$
I4 Perform offset correction
I5,C,G Measure C and G values, step 1
I6,C,G Measure $C$ and $G$ values, step 2

## Description

The I command allows you to perform the three methods of cable correction over the IEEE- 488 bus: driving point, matrix parameter, and calibration capacitor method. Of these three cable correction methods, only the driving point method is available from the front panel, as discussed in paragraph 3.21. All methods are covered in detail in paragraph 4.11 of this section.

Cable correction commands include:

## I0: Driving Point Method

This method involves connecting two identical cables to the INPUT and OUTPUT jacks with the opposite ends left open. Cable correction is then performed either by pressing CABLE CAL or by sending IO over the bus. While this method is the simplest, it cannot be used with complex transmission paths with multiple connecting points.

## I1: Assigning Internal Correction Constants

$I 1$ allows you to send the actual internal constants used by the insrument to perform corrections. These constants are derived by the instrument when it performs any form of cable correction, and can be read from the unit by using the U26 command. By combining I1 and U26, the number of correction setups that can be saved can be extended beyond the seven setups that can be stored within the instrument. See paragraph 4.11 for details.

## 12 and I3: Matrix Parameter Method

Here, real and imaginary parameters are programmed with the I2 and I3 commands. These parameters are components of the A, B, C, and D matrix parameters.

## 14, I5, and 16: Calibration Capacitor Method

With this method, two precisely known capacitance sources are measured. The resulting constants are then used to perform correction with subsequent measurements. I4 is used to perform correction offset, while I5 and I6 are used to send the actual source values over the bus.

Programming Use the $C$ command (paragraph 4.9.19) to save and recall cable correction parameters. Note

Programming 10 OUTPUT $715 ;$ :IQX': ! Perform driving point correction.
Examples 20 OUTPUT $715 ;$ " $14 \times$ " "
30 OUTFUT 715; "I5K,470E-12K"; ! Send first source value. 40 OUTPUT 715 ; "IG:180E-12K": ! Send second source value.

### 4.9.19 Save and Recall Cable Corrections (C)

Purpose To save or recall of cable correction parameters.

## Format Cn,m

Parameters $\quad \mathrm{C} 0, \mathrm{~m}$ Recall cable correction ${ }^{\#} \mathrm{~mm}(0 \leq \mathrm{m} \leq 7)$
C 1 , m Save cable correction \#m ( $1 \leq \mathrm{m} \leq 7$ )
Default Power-up/DCL/SDC Configuration: Factory default is $\mathrm{C} 0,0$ (disable external cable correction)

Description The $C$ command allows you to save and recall up to seven different external sets of cable correction parameters for use when measuring at 100 kHz or 1 MHz . This process is similar to using the front panel CABLE \# key. Before using this command to save corrections you must first perform one of the cable correction processes, as discussed in paragraph 4.9.19.

Programming 1. To disable external cable correction, send a $\mathrm{C} 0,0 \mathrm{X}$ command (correction to front Notes panel jacks remains in effect).
2. Saved and recalled corrections at each position must be at the same frequency, or inaccurate readings will result.

Programming 10 OUTPUT $715 ;$ "C0, 48:" ! Recall correction \#4.
Examples 20 OUTFUT $715 ;$ " $\mathrm{C} 1: 2 \mathrm{Z}$ :" ! Save correction \#2.
30 OUTFUT 715; "COs明: ! Disable correction.

### 4.9.20 Calibration (Q)

## Purpose To calibrate the instrument to known standards.

| Format | Qn(,parameters) |
| :--- | :--- |
| Parameters | Q0 Thermal drift correction (same as CAL key) |
|  | Normal Mode: |
|  | Q1 Null offsets |
|  | Q2,C,G First capacitance calibration point |
|  | Q3,C,G Second capacitance calibration point |
|  | Q4,C,G Conductance calibration point |
| Driving Point Mode: |  |
|  | Q5 Null offsets |
|  | Q6,C,G First capacitance calibration point |
|  | Q7,C,G Second capacitance calibration point |
|  | Voltage Calibration: |
|  | Q8 Null offsets |
|  | Q9,V Calibrate voltmeter gain |

Description The Q 0 command performs the same operation as the front panel CAL key by verifying instrument accuracy to internal capacitance standards. This process should be repeated periodically, as discussed in paragraph 3.11.

The remaining Q commands perform complete instrument calibration to precisely known sources. For complete information on using these commands to calibrate the instrument, including required standards, necessary equipment, and detailed calibration procedures, refer to paragraph 7.3 in Section 7 of this manual.

Programming 1. A CAL LOCKED error message will occur if you attempt to use the Q1-Q9 comNotes mands with the internal calibration switch in the disabled (locked) position.
2. Calibration should be performed only with precisely known sources, as discussed in paragraph 7.3.
3. Sending DCL or SDC will cancel drift correction (Q0) constants.

Programming 10 OUTFUT 715; "G0N": ! Perform internal calibration. Examples 20 OUTFUT 715; "REX': ! Calibrate voltage offsets.

### 4.9.21 Terminator $(\mathbf{Y})$

Purpose To program the terminator(s) the instrument sends at the end of its data string.
Format Yn

Parameters $\quad \mathrm{Y} 0<\mathrm{CR}><\mathrm{LF}\rangle$
$\mathrm{Y} 1<\mathrm{LF}><\mathrm{CR}>$
$\mathrm{Y} 2<\mathrm{CR}>$ $\mathrm{Y} 3<\mathrm{LF}>$

Default Power-up/DCL/SDC Configuration: Factory default is Y 0 ( $<C R><L F>$ ).
Description By using the $Y$ command, you can program the number and type of terminator characters the instrument sends at the end of its data string. Available terminator characters are the commonly used CR (carriage return) and LF (line feed) characters. These terminator characters are recognized by most controllers. The ASCII value of the CR character is 13, and the ASCII value of the LF character is 10.

Programming 1. EOI is another method that can be used to terminate the controller input sequence, Notes as discussed in paragraph 4.9.22. EOI is asserted with the last terminator byte when enabled.
2. The programmed terminator will also be transmitted at the end of the status words. Status word programming is covered in paragraph 4.9.15.
3. The programmed terminator is sent only at the end of the complete data transmission sequence regardless of the selected data format.

Programming 10 OUTPUT 715 ; "Y2X: ! Program CR only as terminator. Examples 20 OUTPUT $715:$ : $13 \mathrm{X}:$ : Terminate on LF. 30 OUTPUT 715; "Y@x"; ! Restore default terminator.

### 4.9.22 EOI and Bus Hoid-off on X (K)

Purpose To enable/disable EOI and bus hold-off.

## Format Kn

Parameters K0 Both EOI and bus hold-off on X enabled K1 EOI disabled, bus hold-off on $X$ enabled K2 EOI enabled, bus hold-off on $X$ disabled K4 Both EOI and bus hold-off on $X$ disabled

Default Power-up/DCL/SDC Configuration: Factory default is K0 (both EOI and bus holdoff enabled).

Description The EOI line provides one method to positively identify the last byte in the data string sent by the instrument. When enabled, EOI will be asserted with the last byte the instrument sends over the bus.

Bus hold-off allows the instrument to temporarily hold up bus operation via the NRFD line when it receives the $X$ character until all commands are processed. The advantage of using bus hold-off is that no commands will be missed while the instrument is processing previously received commands. Table $4-15$ summarizes NRFD hold-off times for various commands.

Programming 1. Some controllers rely on EOI to terminate their input sequences. Suppressing EOI Notes may cause the controller input sequence to hang.
2. When reading a buffer, EOI is asserted only at the end of the entire buffer transmission.
3. When enabled, EOI will be asserted with the last byte in the terminator (if enabled), or with the last byte in the data string if the terminator has been disabled.
4. When bus hold-off is enabled, all bus activity will be held up for the duration of the hold-off period-not just-activity associated with the Model 590.

Programming 10 OUTPUTT 15 ; : K 18 :" ! Disable EOI, enable hold-off.
Examples 20 UUTPUT 715 ;"Kex"; ! Enable EOI, disable hold-off.

Table 4-15. Typical Bus Hold-off Times

| Command | Typical Hold-off Period |
| :---: | :---: |
| Function (F0 $\rightarrow$ F1) | 151msec |
| Range (R1-R2) | 151 msec |
| Rate ( $\mathrm{SO} \rightarrow \mathrm{SO}$ ) | 93 msec |
| (S1-S1) | 110 msec |
| (S3-S3) | 151 msec |
| (S4-S4) | 555 msec |
| Trigger ( $\mathrm{T} 0,1 \rightarrow \mathrm{~T} 1,1$ ) | 160 msec |
| Waveform ( $\mathrm{W} 1,1,1,1 \rightarrow W 2,2,2,2$ ) | 200 msec |
| Bias Voltage (V1,2,3,4 $\rightarrow$ V2,4,6,8) | 200 msec |
| Bias Control (NO $\rightarrow$ NO) | 150 msec |
| (N1 $\rightarrow$ ' 1 1) | 690 msec |
| Data Format (G0 - G1) | 61 msec |
| Operation ( $\mathrm{O} 0,0,0 \rightarrow \mathrm{O1}, 0,0$ ) | 88 msec |
| Buffer ( $\mathrm{B0} \rightarrow \mathrm{B0}$ ) | 75 msec |
| (B1 - B1) | 87 msec |
| (B2 $\rightarrow$ B2) | 87 msec |
| (B3 $-\mathrm{B} 3)$ | 160 msec |
| Plotter (A0 - A1) | 74 msec |
| Zero ( $\mathrm{Z0} \rightarrow \mathrm{Z1}$ ) | 150 msec |
| Filter (P0 $\rightarrow$ P1) | 153 msec |
| Status (U1 - U2) | 61 msec |
| SRQ (M1 $\rightarrow$ M5) | 61 msec |
| Save/Recall (L0, $1 \rightarrow \mathrm{~L} 0,2)$ | 176 msec |
| (L1,1 $\rightarrow$ L1,2) | 624 msec |
| Cable Parameters ( $10 \rightarrow \mathrm{IO}$ ) | 1.96 msec |
| Save/Recall Cable ( $\mathrm{CO} \rightarrow \mathrm{C0}$ ) | 77 msec |
| (C1 -C 1 ) | 246 msec |
| Calibration ( $\mathrm{Q} 0 \rightarrow \mathrm{Q} 0$ ) | 3.5 sec |
| $(\mathrm{Q} 8 \rightarrow \mathrm{Q} 8)$ | 2 sec |
| Terminator (Y0 $-\mathrm{Y1}$ ) | 61 msec |
| EOI + Hold-off ( $\mathrm{K0} \rightarrow \mathrm{~K} 1$ ) | 67 msec |
| Self Test (J1) | 32 sec |
| Display (DAAAA $\rightarrow$ DLLLL) | 67 msec |

### 4.9.23 Display (D)

Purpose To write messages to the front panel display.

## Format Daaa

Parameters aaa ASCII characters ( 20 maximum)
Description The D command allows you to display messages on the front panel. To send a message, simply follow the D command with the appropriate ASCII characters. Many displayable ASCII characters can be sent, including upper case characters, and numbers. Characters that can be displayed include: A-Z, $0-9$ and $+-=/$ ? ( ).

If a character cannot be displayed (for example !), all segments of that particular character will turn on.

Programming 1. Spaces in the command string are ignored and will not be displayed. However, Notes you can display a <space> by placing the * character in that position.
2. As with other device-dependent commands, the D command string should be terminated with the $X$.
3. The maximum number of characters is 20 ; any extra characters in the string will be ignored.
4. To return the display to normal, send DX or press the front panel LOCAL key.

[^0]
### 4.9.24 Hit Button (H)

Purpose To allow emulation of front panel key press sequence.
Format Hn
Parameters The parameter n represents the number of the front panel button. Table 4-16 lists the numbers of all front panel keys that can be used with the hit command.

Table 4-16. Hit Button (H) Command Summary

| Command | Button | Command | Button |
| :--- | :--- | :---: | :--- |
| H12 | SHIFT/QUTT | H25 | ZERO |
| H15 | ENTER | H26 | CAL |
| H16 | (ATB) | H27 | FILTER |
| H20 | ON | H29 | RANGE |
| H23 | MANUAL | H30 | FREQ |
|  |  | H31 | MODEL |

*Shifted modes are shown in parenthesis, send H12X before these commands to implement them.

Description The H command and its options allow you to emulate front panel keystroke sequence. To emulate any such sequence, simply send the appropriate commands in the necessary order.
Programming 1. The instrument may respond to H command options for keys not listed in Table Notes 4-16; however, it is recommended that you not use them because the instrument will hold off the bus in those cases. To restore bus operation, use the appropriate front panel key to return to normal front panel display.
2. The $X$ character must follow each command in a multiple command string.
3. The H command is functional even if LLO (Local Lockout) is in effect.

Programming 10 DUTFUT 715; " $\mathrm{H} 29 \%$ : ! Emulate RANGE button press. Examples 20 OUTPIT 715 : "H3日RH318": !Emulate FREQ, MODEL button presses. 30 OUTFUT 715; "H12XH16\%": Emulate SHIFT, A $\rightarrow$ presses.

### 4.9.25 Self Test (J)

Purpose To test front panel display and internal circuitry.

## Format Jn

Parameters J1 Perform self test
Description The self test command allows you to test much of the internal circuitry, including front panel display segments, and internal reference capacitors. If a problem is found, the instrument will display an error message:

MULTIPLIER FAL: hardware multiplier failure.
INVALID: excessive offsets or reference capacitor problem.
Programming 1. Allow 30 seconds for the instrument to complete the self test:
Notes 2. The instrument will hold off bus operation with the NRFD line during self test operation. Thus, no commands can be sent during the self test.

Programming i6 OUTPUT 715; "A18' ! Perform self test.
Examples 20 HAIT 5000 O ! Wait for test completion.

### 4.10 TRANSLATOR

The enhanced Translator software allows you to define your own programming words in place of standard Keithley device-dependent commands or command strings. For example, the word BIAS could be used in place of $\mathrm{V} 1,3,0.1,2 \mathrm{X}$ to program bias voltage parameters. In a more complex example, the word SETUP1 could be used in place of R0F1T2G4X.

The Translator can also be used to emulate the command syntax of other manufacturers' products. For example, Hewlett-Packard uses the command RA to place their instruments in autorange, while the Keithley equivalent is RO. By using Translator, a kind-of standard programming language could be developed for a variety of different instruments on the bus.

Translator uses a number of reserved words and character, as summarized in Table 4-17. Note that these words and character are reserved and cannnot be used as Translator words. In addition, the $X$ (execute) character cannot be used in a Translator word.

## Table 4-17. Translator Reserved Words and Characters

| Word or <br> Character | Description |
| :---: | :--- |
| ALIAS | Define words, enable Translator |
| NEW | Enable Translator, combine words |
| OLD | Disable Translator |
| LIST | Get list of Translator words |
| FORGET | Erase Translator words |
| $;$ | Terminate Translator definition string |
| $\$$ | Wildcard to define parameter position |

One enhanced feature of the 590 Translator is the wildcard method of parameter handling. Wildcard parameter handling allows you to intermix defined Translator words with standard device-dependent command options.

Commands associated with Translator are discussed in the following paragraphs.

### 4.10.1 Defining Translator Words (ALIAS)

| Purpose | To define Translator words and associate them with a particular device-dependent <br> command string. |
| :--- | :--- |
| Format | ALIAS WORD COMMAND ; | Parameters | ALIAS: The reserved word used to define Translator words. |
| :--- |
| WORD: The user-defined Translator word. |
| COMMAND: A device-dependent command or command string. |
| (semicolon): This character is necessary to terminate the Translator definition string. |
| <space > : Spaces must be included between the words and semicolon. |

All upper and lower case letters as well as most other displayable ASCII characters can be used in Translator words. Note, however, that the <space> ; or \$ characters cannot be used as these characters are reserved for other purposes.

Programming 1. Sending the ALIAS command automatically enables Translator.
2. Spaces must be included in the ALIAS command string as indicated above.
3. Defining a Translator word that already exists will cause the following error message to be displayed:

## TRANSLATOR-ERR

4. A Translator word cannot exceed 31 characters.
5. A device-dependent command string associated with a Translator word cannot be longer than 128 characters.
6. The number of Translator words that can be defined depends on the relative size of the various Translator words and device-dependent command strings. A maximum of 969 bytes (characters) are available for Translator memory. Each word requires a 5 -byte overhead plus one byte per letter in the Translator word and device-dependent command string.
7. The $X$ (execute) character cannot be used in the Translator word itself, but it must be included as the last character in the device-dependent command string, if that particular Translator word is to be executed when sent.
8. The DCL and SDC commands will clear Translator words from memory and disable the Translator.

Programming 10 OUTPLIT 715; "ALIASSETUP1F1REX;"; ! Define SETUP1 word for Examples

20 OUTFUT 715; "ALIAESETUFERETBEA: " ! Define SETUP2 word for R2T3S2X
S6 OUTPUT 715: "SETUFi": ! Execute SETUP1 word (F1R0X).
4日 OUTPUT 715: "SETUFこ"
! Execute SETUP2 word (R2T3S2X).

### 4.10.2 Enabling the Translator (NEW)

Purpose To enable Translator using previously defined words.
Format NEW
Parameters None
Description NEW enables Translator and informs the instrument that the following command strings may contain Translator words. The instrument will then respond both to Translator words as well as the usual device-dependent commands. NEW can also be used to combine Translator words, as described in paragraph 4.10.4.

Programming 1. The ALIAS command, which is used to define Translator words, automatically Notes enables the Translator.
2. Using NEW does not in any way change defined Translator words or the associated command strings.
Programming 10 OUTPUT 715 ; "HEW": ! Send NEW to enable Translator.
Example

### 4.10.3 Disabling the Translator (OLD)

Purpose To disable the Translator without erasing previously-defined words.

## Format OLD

Parameters None
Description OLD performs the opposite function from NEW in that Translator will be disabled. After OLD is sent, the Model 590 will respond only to device-dependent command strings.

Programming Using OLD does not erase previously-defined Translator words from memory. Such Note words can be used again simply by sending NEW to re-enable the Translator.

Programming 16 OUTFUT 715; "aLI": ! Disable Translator. Example

### 4.10.4 Combining Translator Words (ALIAS and NEW)

Purpose To combine existing Translator words into a new word with the combined func-
tions of the original words.
Format ALIAS NEWWORD NEW OLDWORD1 NEW OLDWORD2;

Parameters ALIAS: Defines the Translator word. NEWWORD: The new word to be defined. OLDWORD1 and OLDWORD2: Existing Translator words. NEW: Reserved word indicating that OLDWORD1 and OLDWORD2 are existing Translator words.
; (semicolon): A terminator that marks the end of the ALIAS sequence.
<space>: A space must be included between each word.
Description ALIAS and NEW can be used together to combine the functions of two or more existing Translator words into a single word. This new word will then include the functions of the device-dependent commands associated with the original words.
Programming 1. Using ALIAS will automatically enable the Translator.
2. The instrument will still recognize any original words even if combined in this manner.
3. Reserved words or the $X$ (execute) character cannot be used in a Translator word.

Programming
Examples

10 OUTPUT 715; "ALIAS SETUF1 F1X;': ! Define SETUP1 as F1X.
20 OUTPIT 715 ; "ALIAS SETUPZ REX;": $!$ Define SETUP2 as ROX.
30 OUTPUT P15; "ALIAS SETUFS HEN !-Combine SETUP1 and SETUP2 SETUP LNEN SETUPE;"
4G DUTPUT P15: "SETUPS":
into SETUP3.
! Execute SETUP3 (F1XROX).

### 4.10.5 Reading Back Translator Words (LIST)

Purpose To obtain a list of defined Translator words.
Format LIST

Parameters None
Description Programmed Translator words can be obtained from the instrument by the controller by using the LIST command. After sending LIST to the instrument, the words can be obtained in the same manner used to access normal instrument data. The various words will be delimited by spaces, and the most recently programmed word will be transmitted first.

Programming 1. If no Translator words exist in memory, none will be transmitted when the word Notes list is requested.
2. Only the Translator words will be sent following the LIST command. The devicedependent commands associated with the commands will not be transmitted.
3. The programmed terminator and EOI command will be transmitted at the end of the complete LIST sequence.

| Programming |  | ! Dimension input string. |
| :---: | :---: | :---: |
| Eamples | 20 OUTPIT $715 ; 4$ ALIASSETUPI R1F1\%; | $!$ Define first word. |
|  | 30 DUTPUT 715; "ALIASSETUF2 RGT2\%;" | ! Define second word. |
|  | 40 OUTPUT 715 ; "ALIASSETUFS GESER: | ! Define third word. |
|  | 50 DUTPUT 715 ; "LIST" | ! Send LIST command. |
|  | 60 ENTER 715; A* | ! Get word list. |
|  | T6 IISF A ${ }^{\text {a }}$ | ! Display word list. |

### 4.10.6 Purging Translator Words (FORGET)

Purpose To erase previously defined user Translator words from memory.
Format FORGET
Parameters None
Description Translator words can be purged (erased) from memory by using the reserved word FORGET. Once this command is sent, there is no way to restore them other than by re-programming with the ALIAS command.

Programming The DCL and SDC commands will also erase Translator words from memory. Note

Programming 16 OUTFUT 715; "FOREET" ! Erase all user Translator words.
Example

### 4.10.7 Obtaining Translator Status (U27-U31)

Purpose To obtain user and factory Translator word lists, a list of reserved words, and to determine whether or not Translator is enabled.

## Format Un

Parameters U27 Send user name list (no DDCs).
U28 Not used
U29 Send list of reserved words.
U30 Indicate Translator state (NEW or OLD).
U31 Send user translation list, including DDCs.
Description The U27 through U31 commands allow you to obtain from the instrument certain information on various aspects of Translator programming. To obtain the desired status, simply send the command, address the instrument to talk, and input the status string as you would with normal data.

U27 will give you the user name list. Information associated with these commands includes the defined Translator words, but the associated device-dependent commands will not be sent. To obtain both the Translator word and the command string associated with it, send U31 for the user list:

U29 will give you a list of the reserved words such as ALIAS and NEW, while U30 will indicate whether the Translator is enabled (NEW) or disabled (OLD).

Table 4-18 summarizes Translator status words, and Figures 4-38 through 4-41 show the general formats for all the Translator status words.

Table 4-18. Translator Status Word Summary

| Command | Identifier | Description |
| :---: | :---: | :--- |
| U27 | UNL | User Name List (No DDCs) |
| U29 | RNL | Reserved Name List |
| U30 | AAA | NEW or OLD in AAA field <br> defines state |
| U31 | UTL | User Translation List (Includes <br> DDCs) |

Programming 1．A Translator status word will be sent only once per command．
Notes 2．Additional status words which detail other aspects of instrument op
3．The programmed terminator and EOI will be sent at the end of the status word string．
4．The U27 and LIST commands perform the same operation．
5．If no Translator words are defined，nothing except the terminator and EOI（if programmed）will be sent after programming U27．

## Programming

$1[\operatorname{IIIM} A \neq[206] \quad!$ Dimension input string．
29 GUTPUTT 715 ；＂リ27X＂；！Program for user name list．
SQ EHTER 715 ；A\＄！Get user name list．
40 IISF A 4 ，Display factory name list．
 69 EHTER 715；A青 Get reserved word list．
70 IIISP A 丰 ！Display reserved words．
E日 OUTPUT 715；＂UJ30\％＂！Program for Translator state．
90 EHTER 715： A 丰
100 IISF a⿻三 $^{\circ}$ ．－． Display NEW or OLD．


Figure 4－38．U27 Status Word Format（Translator User Name List）


Figure 4－39．U29 Status Word Format（Reserved Name List）


Figure 4－40．U30 Status Word Format（New／Old Status）


Figure 4-41. U31 Status Word Format (Translator User Translation List)

### 4.10.8 Translator Parameter Passing (\$)

Purpose To allow partial definition of Translator words with parameters later passed in devicedependent command options.

## Format ALIAS WORD Cmd\$(,\$)(,\$) ;

Parameters ALIAS: The reserved word that defines Translator words.
Cmd: A device-dependent command letter.
\$: A wildcard parameter used to mark a position where command options will later be inserted.
<space>: A space must-be included between elements of the string.
;: Semicolon is necessary to terminate the ALIAS string.
Description The $\$$ character is a wildcard that allows you to mark the position in a devicedependent command string where parameters will later be placed. With multiple option commands, you may substitute as few or as many options as desired. For example, to specify voltage parameters, you could define $\mathrm{V} \$, \$, \$, 5 \mathrm{X}$, or simply $\mathrm{V} \$, 10,0.5,5 \mathrm{X}$. In the first case, only the default bias (5) is specified when the Translator word is first-defined, while the remaining parameters (first, last, and step bias voltages) would be sent when the Translator word is transmitted to the instrument. In the second instance, only the first voltage would be left unspecified, while the remaining parameters would be permanently defined as attributes of the Translator word.

To pass parameters once a word is defined, you need only include the command options immediately following the Translator word in your command string. The word and each option must be separated with a space, and would normally be followed with the usual terminator sequence. For example, assume that $=$ you previously defined the word VOLTS as being associated with V $\$, \$, \$, 5 \mathrm{X}$. Options could then be passed by sending the following string:

## VOLTS 1100.5 <TERMINATOR>

In this case, the instrument would perform a command equivalent to $\mathrm{V} 1,10,0.5,5$, or first, last, step, and default voltages of $1 \mathrm{~V}, 10 \mathrm{~V}, 0.5 \mathrm{~V}$, and 5 V , respectively.
Programming 1. With multiple-option commands, each parameter, including wildcards, must be Notes separated by commas.
2. Parameters for all wildcards must be included with the Translator word when sent.
3. The execute character must be included as the device-dependent command string, if those commands are to be executed when that particular string is sent.
4. Parameters are passed in the order they appear in the definition and execution strings.

| Programming Examples |  | ! Define RANGE with R command. |
| :---: | :---: | :---: |
|  |  | $!$ Program autorange. |
|  | 30 OUTFUT 715 : "RAHEE 9 ", | ! Turn off autorange. |
|  | 46 OUTPUT 715: "RANGE 4" | ! Select-2nF range. |
|  | 50 OUTFUT 715: "ALIAS UOLTSU未 | ! Define VOLTS with V command only default voltage specified. |
|  |  | ! Send VOLTS with passed parameters first, last, and step. |
|  | 70 OUITPUT 715 : "ALIASEIASHI, <br>  | $!$ Define BIAS with $W$ command, all except step time specified. |
|  | E0 OLTPUT $715:$ "EIAS 10日E-3" | $!$ Program BIAS with 100 msec step time. |

### 4.10.9 Translator Error Handling

Purpose To flag Translator error conditions.
Format TRANSLATOR-ERR
Description If a Translator error occurs, the instrument will briefly display the following message on the front panel:

## TRANSLATOR-ERR

In addition, the Translator error bit in the U 1 status word will be set when an error condition occurs (paragraph 4.9.15). Since the setting of any bit in the U1 can generate an SRQ (Service Request), the unit can be programmed to request service from the controller should a Translator error occur. Refer to paragraph 4.9.16 for SRQ information.

Conditions that can cause a Translator error include:

1. No more memory available for additional Translator words. A total of $\mathbf{1 , 4 5 0}$ bytes (characters) are available for Translator words and the associated device-dependent command strings.
2. Use of more than one ALIAS in a definition. ALIAS can be used only once per definition.
3. Translator word exceeds the maximum allowed 31 characters.
4. Use of $X$ in a Translator word.
5. Attempting to define a Translator word that already exists.
6. Using a reserved character or word in a Translator word (\$ LIST FORGET ALIAS NEW OLD).

### 4.11 CABLE CORRECTION

The following paragraphs describe in detail the three available methods of cable correction. Correction methods are:

1. Driving point method (front panel and bus): The driving point admittance of an open-ended cable is measured and correction constants are calculated from the resulting measurements.
2. Matrix parameter method (bus only): Transmission line matrix parameters are sent to the instrument over the bus to derive the necessary correction constants. These matrix parameters are derived from two-port scattering parameters that must be measured with specialized test equipment.
3. Calibration capacitor method (bus only): Here, two precisely known capacitance sources are connected in place of the test fixture, and the Model 590 is programmed with the actual values over the bus.

The three available methods as well as certain facts and limitations are summarized in Table 4-19. Table 4-20 summarizes bus commands associated with cable correction. I0 performs driving point cable correction, while I2 and I3 send the transmission line matrix parameters for the OUTPUT and INPUT paths, respectively. I4, I5, and I6 are used to perform the calibration capacitor method in two steps. II is used to send internal cable correction coefficients to the instrument.

Two additional cable correction commands include the C command, which can be used to save and recall cable correction set ups, as well as the U26 command used to obtain cable correction constants from the instrument.

More information on cable correction principles may be found in Section 6 of this manual.

## NOTE

The dynamic range of the capacitance and conductance readings is reduced by using cable correction. The amount of reduction will depend on such factors as cable length and capacitance.

Table 4-19. Cable Correction Methods

| Method | Description | Typical <br> Accuracy* | Comments |
| :---: | :--- | :---: | :--- |
| 1 | Driving point <br> (Front panel or | $2 \%$ | Single cables <br> only |
| 2 | bus) <br> Matrix parameter <br> (Bus only) | $1.5 \%$ | Can be used <br> with complex <br> paths. |
| Calibration capa- <br> citor (bus only) | $0.5 \%$ | Can be used <br> with complex <br> paths. |  |

*Accuracy figures are only typical and are exclusive of other accuracy figures given at the front of this manual.

NOTE: Cable correction does not affect linearity specifications.

Table 4-20. Cable Correction Commands

| Command | Description |
| :---: | :---: |
| C0, n | Recall cable setup $\mathrm{n}(0 \leq \mathrm{n} \leq 7)$ * |
| CI, n | Save cable setup $\mathrm{n}(1 \leq \mathrm{n} \leq 7)$ |
| I0 | Perform driving point correction |
| I1,n1,n2,n3,n4 | Assign correction constants $K 0(n 1+j n 2), K 1(n 3+j n 4)$ |
| $\begin{aligned} & \mathrm{n} 2, \mathrm{n} 1, \mathrm{n} 2, \mathrm{n} 3, \mathrm{n} 4, \\ & \mathrm{n} 5, \mathrm{n} 6, \mathrm{n} 7, \mathrm{n} 8 \end{aligned}$ | Assign test OUTPUT matrix parameters: $A(n 1+j n 2), B(n 3+j n 4)$, $C(n 5+j n 6), D(n 7+j n 8)$ |
| 13,n1,n2,n3,n4, | Assign test INPUT matrix parameters: |
| n5,n6,n7,n8 | $\begin{aligned} & A(n 1+j n 2), B(n 3+j n 4), C(5 n+j n 6), \\ & D(n 7+j n 8) \end{aligned}$ |
| I4, C, G | Zero cable open |
| I5, Cr, G | Program $C$ and $G$ values, step 1 |
| I6, C, G | Program C and G values, step 2 |
| U26 | Obtain cable correction constants |

*To cancel cable correction, use $\mathrm{C} 0,0$

### 4.11.1 Driving Point Correction

## Description

To perform cable correction with this method, you need only connect your test cables to the test INPUT and OUTPUT jacks and send the appropriate command over the bus (cables must be unterminated when the command is sent). Note that this method can be used only with simple transmission paths. To properly correct for multiple-cable or switching matrix paths, you must use either the matrix parameter or standards method described below.

## Required Equipment

Other than the two coaxial cables used to connect the test fixture to the Model 590, no additional equipment is required.

## Procedure

1. Tuitn on the Model 590 and allow it to warm up for at least one hour before beginning the correction procedure.
2. Program the Model 590 for the desired frequency and 2 nF range. With an HP-85 computer, this command string can be sent with the following statement:

$$
\text { OUTFUT } 715 ; \text { "F1R4K': }
$$

In this instance, we have chosen 1 MHz .
3. Connect two RG-58 cables of identical length to the test INPUT and OUTPUT jacks of the instrument, but leave the opposite ends disconnected. Keep in mind that the maximum recommended cable length is five meters.
4. Send the command $10 X$ over the bus to perform correction. Again, with an HP-85, this command can be sent as follows:

$$
\text { OUTFUT } 715 \text {;" } \text { IQN" }
$$

5. The instrument will then perform the correction, a process that will take a few seconds to complete. The new cable correction constants will then be placed into effect immediately.
6. See paragraph 4.11.4 for methods to save the correction constants.
7. Connect the test fixture to the cables and make measurements in the usual manner.

## Limitations and Considerations

The driving point cable correction method assumes the following:

1. Only simple, single-cable transmission paths can be used.
2. The characteristic impedance of the cable is $50 \Omega$.
3. Cable loss is zero.
4. Both cables are of exactly the same length.

Any deviations from these ideal conditions will cause errors in the correction constants, resulting in inaccurate readings.

### 4.11.2 Matrix Parameter Correction

## Description

In order to use the matrix parameter method, each pathway must be characterized for its characteristics impedance (Zo) and scattering (S) parameters utilizing specialized test equipment. Once these values are known, the A, B, C and D transmission line parameters must be calculated and then sent to the instrument. Keep in mind, however, that each transmission path must be characterized separately.

## Required Equipment

Table 4-21 summarizes the equipment necessary to characterize the transmission paths. The 4275A LCR Meter is used to measure the short-circuit inductance and open-circuit capacitance of the path from which the characteristic impedance is calculated. The 3577A Network Analyzer and 35677A S-Parameter Test Set are used to measure the four scattering parameters of each transmission path.

## Table 4-21. Equipment Required for Matrix Parameter Correction

| Equipment | Use |
| :--- | :--- |
|  |  |
| Hewlett-Packard 4275A | Determine $Z_{0}$ of each |
| LCR Meter | pathway. |
| Hewlett-Packard 3577A | Measure scattering (S) |
| Network Analyzer | parameters. |
| Hewlett-Packard 35677A | Used with 3577A to |
| S-Parameter Test Set | measure S parameters. |

## Connections

Figure $4-42$ demonstrates the basic connecting methods for normal measurements as well as for the $Z_{0}$ and $S$ parameter characterization. In (a), a typical test setup using a relay matrix is shown, while (b) and (c) show test configurations for determining $Z_{0}$ and the $S$ parameter respectively

As shown, the test setup included a relay switching matrix, a very common situation. When using such a relay setup, you must make certain that the relay contact(s) associated with the transmission path are closed during the characterization. Also, you should characterize as much of each path as possible for most accurate results. Typically, the complete path from the test INPUT and OUTPUT jacks through to the test fixture itself will be included in the path. One final point-each path must be characterized separately unless you are absolutely certain that the paths are identical.

## Characteristic Impedance Determination

Characteristic impedance, $Z_{0}$, is determined by using the LCR meter to measure the short circuit inductance and open circuit capacitance, from which $\mathrm{Z}_{\mathrm{O}}$ can be calculated. In order to complete the following procedure, you must be thoroughly familiar with the operation of the 4275A LCR meter. Consult the operator's manual for complete information.

1. Turn on the 4275A and allow it to warm up for the required period for rated accuracy. Be sure to select the desired frequency ( 100 kHz or 1 MHz ).
2. Disconnect the test cables from the Model 590 and the test fixture.
3. Connect the end of the cable normally attached to the Model 590 to the LCR meter UNKNOWN terminals, but leave the other end of the cable open at this time.
4. If the transmission path goes through a relay matrix, make sure that any relay contacts are closed.
5. Measure the open-circuit capacitance, $\mathrm{C}_{\mathrm{Oc}}$, using the LCR meter.
6. Short the open end of the test path cable between the center conductor and shield.
7. Measure the short circuit inductance, $\mathrm{L}_{\mathrm{SC}}$, with the LCR meter.
8. Disconnect the cable from the LCR meter and connect the other cable in its place. Again, you should connect the pathway end normally attached to the Model 590.
9. Repeat steps 3 through 8 for the other pathway to determine its $L_{S C}$ and $C_{O C}$ values.
10. Calculate the characteristic impedance for each pathway from the $L_{S C}$ and $C_{O C}$ values as follows:

$$
Z_{\mathrm{o}}=\sqrt{\frac{L_{\mathrm{Sc}}}{\mathrm{C}_{\mathrm{oc}}}}
$$

Where: $Z_{0}=$ characteristic impedance
$\mathrm{L}_{\mathrm{SC}}=$ short circuit inductance
$\mathrm{C}_{\mathrm{OC}}=$ open circuit capacitance

These two characteristic impedance values will be used in calculating transmission line matrix parameters, as described below.

## Measuring S (Scattering) Parameters

Four $S$ parameters, as shown in Figure 4-43, can be used to characterize any two-port network including a complex transmission path. Two of these parameters ( $\mathrm{S}_{12}$ and $\mathrm{S}_{21}$ ) are concerned with transmission, while the remaining two ( $S_{11}$ and $S_{22}$ ) are associated with reflection.

Use the following procedure to measure the $S$ parameters for each transmission path. The basic connections for this procedure are outlined in Figure 4-42(C). Refer to the 3577A manual for complete details on connections and operation.

1. Connect the 35677A $50 \Omega \mathrm{~S}$ parameter test set to the network analyzer, as discussed in the manual provided with that equipment.
2. Turn on the 3577A power and allow the unit to warm up for the prescribed period.
3. Disconnect the test cables from the Model 590 and the test fixture.
4. Connect the pathway cable normally connected to the Model 590 to PORT 1 on the $S$ parameter test set.
5. Connect the pathway cable normally connected to the test fixture to PORT 2 on the test set.
6. Select analyzer start and stop frequencies that will cover the frequency of interest ( 100 kHz to 1 MHz ).
7. If your pathways include one or more relays, make sure any relay contacts are closed while making measurements.
8. Using the network analyzer, determine the real and imaginary components of each of the four $S$ parameters. at the frequency of interest ( 100 kHz or 1 MHz ).
9. Repeat-steps 4 through 8 for the other transmission paths.


Figure 4-42A. Connecting Methods


Figure 4-42B. Connecting Methods (Cont.)


Figure 4-42C. Connecting Methods (Cont.)


S-parameters are simply related to power gain and mismatch loss, quantities which are often of more interest than the corresponding voltage functions:

|  | POWER REFLECTED FROM THE NETWORK INPUT |
| :---: | :---: |
| $\left\|S_{11}\right\|^{2}=$ | POWER INCIDENT ON THE NETWORK INPUT |
| $\left\|S_{22}\right\|^{2}=$ | POWER REFLECTED FROM THE NETWORK OUTPUT |
|  | POWER INCIDENT ON THE NETWORK OUTPUT |
| $\left\|S_{21}\right\|^{2}=$ | POWER DELIVERED TO A Z. LOAD |
|  | POWER AVAILABLE FROM $Z$, SOURCE |
|  | $=\begin{aligned} & \text { TRANSDUCER POWER GAIN WITH Z。LOAD AND } \\ & \text { SOURCE }\end{aligned}$ |
| $\left[\mathrm{S}_{12}\right]^{2}=$ | = REVERSE TRANSDUCER POWER GAIN WITH Z。 LOAD AND SOURCE. |

Figure 4-43. Simplified Parameter Definition

## Calculating Matrix Parameters

Once the $Z_{0}$ and $S$ parameter values are known, the $\mathrm{A}, \mathrm{B}, \mathrm{C}$, and D transmission line matrix parameters can be calculated by using the appropriate formula, as summarized in Table 4-22. Each matrix parameter result will be a complex number of the form:

$$
a \div j b
$$

Where: $a$ is the real component
$b$ is the imaginary component

Note that, although it is possible to derive phase and magnitude equivalents, it is best to leave the results in rectangular form as the Model 590 requires that they be programmed in that manner.

## Programming Matrix Parameters

To program matrix parameters use the appropriate I command to send the eight parameters representing the real and imaginary components of the transmission matrix. For example, the command to program test OUTPUT pathway parameters is of the form:

$$
\mathrm{I} 2, \mathrm{n} 1, \mathrm{n} 2, \mathrm{n} 3, \mathrm{n} 4, \mathrm{n} 5, \mathrm{n} 6, \mathrm{n} 7, \mathrm{n} 8
$$

Where: $n \mathrm{I}=\mathrm{A}$ parameter, real component
$\mathrm{n} 2=$ A parameter, imaginary component
$\mathrm{n} 3=\mathrm{B}$ parameter, real component
$\mathrm{n} 4=\mathrm{B}$ parameter, imaginary component
n5 = C parameter, real component
n6 $=C$ parameter, imaginary component
$\mathrm{n} 7=\mathrm{D}$ parameter, real component n8 $=\mathrm{D}$ parameter, imaginary component

The basic command structure and parameter set for the INPUT cable is the same, except, of course, for the fact that I3 is used in place of 12 . In either case, the programmed correction values will be placed into effect immediately. If you wish to save the correction, use the C command, as described below.

The simple program below will allow you to program these parameters using an HP-85 computer.

Table 4-22. Matrix Parameter Calculation

| Matrix Parameter | I2 or I3 Command Parameters | Calculation |
| :---: | :---: | :---: |
|  |  | $\left(1+S_{11}\right)\left(1-S_{22}\right)+S_{12} S_{21}$ |
| A | n1(real), n2(imaginary) | $A=\frac{2 S_{21}}{}$ |
|  |  | $\left(1-S_{11}\right)\left(1-S_{22}\right)-S_{12} S_{21}$ |
| C | n5(real), n6(imaginary) | $C=\frac{2 S_{21} Z_{0}}{2}$ |
|  |  | - $\left(1+S_{22}\right)\left(1-S_{11}\right)+S_{12} S_{21}$ |
| D | n/(rea), n8(imaginary) | $2 S_{21}$ |
|  |  | $A D-\frac{S_{12}}{S_{21}}$ |
| B | n3(real), n4(imaginary) | $B=\frac{C}{C}$ |


| PROGRAM | COMMENTS |
| :---: | :---: |
| 10REMOTE 715 | $!$ Place unit in remote. |
| 20 CLEAR 7 | ! Send device clear. |
| 25 DUTPUT 715 : F1\%: | $!$ Program 1MHz. |
| EQLEAR | ! Clear CRT. |
| 40 IISF: FROGRAM TEST IHPUT OR OUTPUT: : | ! Prompt for path way. |
| 50 IISF |  |
| 6Q DISF: $1=$ TEST OUTPUT: |  |
| TEIISP: $2=$ TEST INPUT": |  |
| 8 E I HPUT A | ! Input selection. |
| 90 IF $\mathrm{A}=1$ THEN $\mathrm{C} \ddagger=6: 12, *$ ELSE [急=:"IZ": | ! Define programming command. |
| 100 IISP: APARAMETER REAL" | ! Prompt and input |
| 116 IHPUT H 1 | ! real and imaginary |
|  | $!$ components for all |
| ImGIVARY" | ! four matrix parameters. |
| 130 LHFIIT Hz |  |
| 140 DISP: E PARAMETER: | - . |
| EEAL" |  |
| 156IHPIT HE |  |
| 164 IISP: E FARAMETER: |  |
| IMACIHAEY's |  |
| 17 ESHFLT H 4 |  |
|  |  |
| REAL" |  |
| 190 INFUT H5 |  |
| 2GG IISP: $\times$ PARAMETEE: |  |
| IMAEINAFT** |  |
| 210 INFIIT AE |  |

```
229 DISP:INEARAMETEF
    REAL":
2SM INFUT HP
240 IISF: \I FARANETER;
    IMAGIHARY':
    250 IHFIIT HE
    269 OUTPUTT15; E*FHI; ! Program 590 with
```






```
    2TQ IISF:%REFEAT YESOR !Prompt to repeat
    HOy:"
    280 IHPUIT A$
    z90 IF A垁[1,1]=6"Y's THEN
        3E
    304 ENTI
```


## A Practical Example

As a practical example, assume that the Model 590 is to be used in conjunction with a Keithley Model 705 Scanner equipped with a Model 7062 RF Switch Card, as shown in Figure 4-44. This arrangement would allow the Model 590 to automatically test up to five wafers without operator intervention.

To demonstrate typical S parameters, one pathway for the setup in Figure $4-44$ was tested for the four S parameters in the frequency range of 100 kHz to 1 MHz . The resulting real and imaginary values were plotted using autoscaling; the results are shown in Figures 4-45 through 4-52.


Figure 4-44. Test Configuration for S Parameter Examples



Figure 4-45. $\mathrm{S}_{11}$ Real Component


Figure 4-46. $\mathrm{S}_{11}$ Imaginary Component

0
1
0
0
0
0
1


Figure 4-47. $\mathrm{S}_{12}$ Real Component

Figure 4-48. $\mathrm{S}_{12}$ Imaginary Component
REF LEVEL
950. DOE-3


Figure 4-49. $\mathrm{S}_{21}$ Real Component

Figure 4-50. $\mathbf{S}_{21}$ Imaginary Component
$\square$

$$
\begin{array}{|l|l|l|l|l|l|l|l|l|}
\hline & & \\
\hline
\end{array}
$$

$$
\begin{aligned}
& 1 \\
& 1 \\
& 0 \\
& 0 \\
& n \\
& n \\
& n \\
& \hline 1
\end{aligned}
$$


REAL (S22)

$$
15: 300 E
$$



Figure 4-52. $\mathbf{S}_{22}$ Imaginary Component

### 4.11.3 Calibration Capacitor Correction

## Description

The calibration capacitor method is a two-step process involving connecting two precisely known capacitors to the instrument in place of the DUT (device under test) and then programming the actual capacitance values over the bus. Of the three methods, this one is the most accurate, assuming that capacitance source used have been precisely characterized for both capacitance and conductance.

## NOTE

The method outlined here uses the Model 5907 and is performed on the 2 nF range, yielding very good accuracy on all three ranges. The other ranges can be corrected (and stored) separately if appropriate sources are available.

## Recommended Sources

Table 4-23 lists the recommended capacitance sources for cable correction. Note that the values listed are nominal, and you should use the actual 100 kHz or 1 MHz values marked on the sources when programming them over the bus.

If different capacitors are used, they must be of high-quality stable design and properly characterized at the frequency of interest with suitable laboratory standards equipment. Also, each capacitor should be mounted in a shielded enclosure to minimize noise effects.

## Table 4-23. Capacitance Sources Required for Cable Correction

| Value $^{*}$ | Keithley Model Number |
| :---: | :---: |
|  |  |
| 470 pF | $5907^{* *}$ |
| 1.8 nF | 5907 |

*Nominal values shown. 100 kHz or 1 MHz value marked on source should be used.
**Model 5907 includes adapters to connect source to cables.

## Connections

Figure 4-53 shows typical connections for this method of cable correction. Again, we have assumed that a relay matrix will be included in the test path. Of course, your par-
ticular test configuration will probably be different. In any case, you should include as much of the actual test path in the test pathways. Typically, the test fixture will be disconnected from the cables and the source capacitor connected in its place. A better solution would be to connect the source capacitor directly to the test fixture, if possible, since doing so would allow for correction of fixture capacitance.

## Procedure

1. Turn on the Model 590 and allow the instrument to warm up for at least one hour.
2. Select the 2 nF range by sending the command S3R4T2X over the bus.
3. Program the frequency ( 100 kHz or 1 MHz ).
4. Perform drift correction by sending the command Q0X.
5. Disconnect the cables normally connected to the test fixtures and leave the cable ends open. The opposite ends should remain connected to the test INPUT and OUTPUT jacks. Close any relays in the test paths.
6. Send the correction offset command, I4X. A typical $\mathrm{HP}-85$ statement is:

$$
\text { OUTPUT } 715 ;: \text { : I4X': }
$$

7. Connect the 1.8 nF capacitance source listed in Table $4-23$ in place of your test fixture as shown in Figure 4-53.
8. Program the capacitance value by using the $I 5$ command. A typical HP-85 statement is:

$$
\text { OUTPITT } 715 ;: \text { : } 5: 1.8 E-9, G x^{3}:
$$

Here, we have assumed a capacitance of 1.8 nF .
9. Disconnect the 1.8 nF source and connect the 470 pF source in its place (Table 4-23).
10. Program the actual source C value with the I 6 command, as in this HP-85 example:

$$
\text { OUTPUT } 715 ;: 16: 47 \mathrm{EE}-12,6 \mathrm{~S}^{3}
$$

11. After the last command is sent, the programmed cable correction factors will go into effect-immediately. If desired, you can store the correction by using the save command discussed in the following paragraph.
12. Disconnect the source from the test cables and connect the test fixture in its place. Measurements may now be taken as usual.


Figure 4-53. Connections for Calibration Capacitor Correction

### 4.11.4 Saving and Recalling Cable Setups

By using the $C$ command, you can save and recall up to seven cable setups in NVRAM. Cables setups stored in this manner will be retained for future use even if power is removed from the instrument.

## Saving Cable Setups

To save a cable setup, first perform the correction procedure with the desired method (see above) and then send the command C1,n over the bus. Here in represents the position number to save (1-7). For example, to save setup \#4, the following command would be sent:

$$
\text { OUTFUT } 715 ; \times C 1: 4 \mathrm{k})
$$

## Recalling Cable Setups

The C0,n command allows you to reverse the above procedure by allowing the recall of previously stored cable setups. To recall setups, simply include the appropriate cable position number in the command option. Note that numbers 1 through 7 are stored setups, while a parameter of 0 will disable user cable correction and restore factory defaults necessary to correct for internal cabling to the front panel test jacks. Note that the recalled position will go into effect immediately.

For example, to recall position 6 , the following command would be sent:

$$
\text { OUTPUT } 715 ; \text { "C0.6x" }
$$

Similarly, the following command would be used to disable user cable correction constants:
OUTFUT 715; "C0, 日N:

## NOTES:

1. Sending a DCL or SDC command will also disable user correction and restore correction to the front panel only.
2. Corrections saved and recalled at each given position must be at the same frequency, or inaccurate readings will result.

### 4.11.5 Internal Correction Constants

## Description

With all three cable correction methods, the instrument in-
ternally processes the resulting data into two correction constants, K 0 and K 1 . Each of these constants is a complex number of the form:

$$
a+j b
$$

where a is the real component, and b is the imaginary component.

By sending appropriate commands to the instrument, you can request the K 0 and K1 constants in effect at that particular time. A different command allows you to later send them back to the instrument. Thus, these two commands would allow you to save a virtually unlimited number of cable setups, instead of being restricted to the seven user setups that can be saved and recalled with the C command.

## Requesting Correction Constants

The U26 command can be used to request correction constants K0 and K1. The basic procedure below outlines this operation.

1. First make certain that the cable correction constants you wish to access are in effect. If you have just completed a correction and the resulting constants are now operational, you need do nothing further. However, if you are accessing a particular cable setup number, first use the $C 0, \mathrm{n}$ command with n representing the position number of the cable setup to be accessed.
2. Now send the command string U26X over the bus. For example, the correct HP-85 statement is:

$$
\text { OUTFUTT } 715: \text { " } \cup 2 E X:
$$

3. Request data from the instrument as you would normal data, placing instrument status (see Figure 4-54) in a string variable. For example, a typical HP-85 statement would be:

## EHTER 715; $\hat{9}$ 丰

In this instance, the U26 status word, which contains the four-cable correction parameters, would be placed in the $A \$$ variable ( $\mathrm{A} \$$ must be previously dimensioned, by the way, because the data string is longer than 18 characters).
4. The data string can be parsed and broken up into four discrete numeric variables, placed in computer memory, or placed on a mass storage medium, as desired. The example program on the next page demonstrates this process.


Figure 4－54．Status Word Showing K0，K1 Real and Imaginary Parameters

## Sending Correction Constants to the Instrument

Correction constants can be sent from the computer by using the I1 command，which is of the form：

$$
\mathrm{n} 1, \mathrm{n} 1, \mathrm{n} 2, \mathrm{n} 3, \mathrm{n} 4
$$

Where： $\mathrm{n} 1=\mathrm{K} 0$ ，real component
$\mathrm{n} 2=\mathrm{K} 0$ ，imaginary component
$\mathrm{n} 3=\mathrm{K} 1$ ，real component
$\mathrm{n} 4=\mathrm{K} 1$ ，imaginary component

To send these parameters，simply include them in the com－ mand string in the order indicated above．As always，the string must be terminated by the X character in order for the instrument to execute the string．Once executed，the constants will be placed into effect immediately．You can then save them in NVRAM by using the C1 command，if desired．

## Programming Example

The program below demonstrates the basic principles for reading or writing all seven cable setups stored in the in－ strument．The parameters are then stored on or retrieved from tape．

## NOTE

Selecting the write option in the following program will overwrite any presently stored cable setups．

## Program

## 

29 REMOTE 715
30 CLEAR
35 GUTFUT 715；＂FIM＂
40 DISF： $1=$ READ COH－ STANTS FROM $590^{\prime}$ ：

50 HISF： $2=$ HRITE COH－ STAHTS TO 590＇
60 IISF
70 IISF：＂SELECT 1 ORZ＂
80 IHFIIT A
90 IF $\mathrm{A}=2$ THE 296
100 IISF：＂FILEHAME：
110 IMFUT F丰
120 CREATEFF： 5
136 ASSIGN\＃ 1 TOF
$140 \mathrm{FOEN}=1 \mathrm{TOT}$
时：＂x，

170 EHTER 715：A末

$190 \mathrm{NE}=\mathrm{MAL}(\mathrm{A} ⿻ \mathrm{~F}[19,29])$


## Comments

！Dimension input string．
$!$ Place 590 in remote．
！Clear computer CRT．
$!$ Program $\mathbf{1 M H z}$ ．
！Prompt for read or write of instrument parameters．
！Assign filename for storage．
！Create fille for storage．
！Open file to tape．
！Loop for all seven setups．
！Recall cable \＃N．
！Request cable para－ meters．
！Input parameter string．
！Parse string for para－ meters．


### 4.12 PROGRAMMING EXAMPLES

The following paragraphs give some examples of how to program the instrument for typical measurements. As listed, the programs are not necessarily in the most-efficient form, but instead are written for maximum clarity in understanding program flow.

### 4.12.1 Programming for One-Point Measurements

Use the program below to take single-point measurements and display the results on the computer CRT. The program assumes that the instrument will be operated at 100 kHz , with autoranging, and at the 1 reading per second rate. Appropriate changes can be made for other parameters, if desired.

Figure 4 - 55 shows a general flowchart of the program below.

| Program | Comments |
| :---: | :---: |
|  | ! Dimension data input string. |
| 20 REMOTE 715 | $!$ Place unit in remote. |
| 34 ELEAR 7 | ! Send device clear. |
| 40 OUTFUT 715: "FGROX" | ! Program 100 kHz , autorange. |
|  | ! Select $1 /$ sec rate, current reading output. |
|  | ! Program GET, oneshot trigger. |
| 70 OUTPUT 715: "MEX' * | ! Program for SRQ on reading done. |
|  | ! Display prompt. |
| 90 PAUSE | ! Pause for operator input. |
| 1010 TRIGIGER 315 | ! Trigger a single reading. |
| 110 STATUS 7,2 : | ! Get interface status. |
| 120 IF HOT BIT (S. 5 ) THEN <br> 110 | ! Wait for SRQ to occur. |
| $1305=\mathrm{SFOLL}(715)$ | ! Serial poll unit to clear SRQ. |
| 146EHTER 715: ${ }^{\text {a }}$ | $!$ Get reading string from 590. |
| 150 TISF A | ! Display reading string. |
| $160 \mathrm{gatog} g$ 170 EHII | ! Repeat. |



Figure 4-55. Flowchart of One-Point Program

### 4.12.2 CV Plotter Programming

The program below will allow you to take a reading sweep and then graph the data on an intelligent plotter connected to the instrument through the IEEE-488 bus. This program assumes that the plotter primary address is 5 .

A flowchart of the program is shown in Figure 4-56.

| Program | Comments |
| :---: | :---: |
| 10 REMITE 715 | $!\mathrm{P}$ |
| 20 CLEAR 7 | S Send device clear |
| 30 DUTFUT 715; "FGR4X! | ! Select $100 \mathrm{kHz}, 2 \mathrm{nF}$ range. |
| 46 OUTPU T 715; | ! Program 100/sec rate filter off. |
|  | ! Select sweep on GET mode. |
|  | ! Select single staircase. |
| 70 OUTPUT 715: "6U-5,530.1, 04's | $\begin{aligned} & \text { Program }-5 \mathrm{~V} \text { first } \mathrm{V} \\ & +5 \mathrm{~V} \text { last } \mathrm{V}, 0.1 \mathrm{~V} \\ & \text { step V, } 0 \mathrm{~V} \text { default }=- \\ & \text { V. } \end{aligned}$ |
|  | ! Program for SRQ on sweep done. |
| SO IISF: AFRESS "COHT' TO | ! Prompt for measurement. |
| 1 an Pause | ! Pause for operator input. |
| 110 OUTFUT 715 : "Hix" | $!$ Turn on bias output. |
| 120 TRIGIGER 715 | ! Trigger reading sweep. |
| 130 IISF: $\operatorname{sHEEP}$ IN FROGRESS: | ! Display sweep message. |
| 1409TATIS 7:2:S | ! Check interface status. |
| 150 IF HOT EIT (S.5) THEN 140 | ! Wait for SRQ. |
| 160 S = SFOLL (ح15) | ! Serial poll to clear SRQ. |
| 176 OUTPUT 715: "E3\%" | ! Transfer data to plot buffer. |


| Program | Comments |
| :---: | :---: |
| 160 IISP: SHEEP IOUHELOAD FLOTTER MITH PAPER, PRESS 'COHT':" | $!$ Prompt for plotting. |
| 19001TFUT 715 : 5 HEx" | ! Turn off bias source. |
| 206 PAUSE | ! Wait for operator input. |
| 216 OUTPUT $715 ; \mathrm{M} 12 \mathrm{E}$ | ! SRQ when plotter done. |
|  | ! Select pen \#1. |
|  | ! Program solid line type. |
| 240 OUTFITT 715; : A7 | ! Select full labels. |
| 250 OUTPUT $715 ; \times$ A 2 : ${ }^{\text {c }}$ | ! Select C vs V plot type. |
| 26 | ! Select full grid type. |
| 276 OUTPUT 715; "A4, | ! Plot from plot buffer. |
|  | ! Execute plot. |
| 290. SEHIT 7 L UNT UHL TALK 15 LISTENS | ! Address 590 to talk, plotter to listen. |
| 300 RESUME? | ! Set ATN false. |
| 319 STATIS 7,2 | ! Get bus status. |
|  | ! Wait for plot to finish. |
| SSG SEEHI 7; UNT UHL | ! Untalk and unlisten the bus. |
| 346 S=SPOLL (715) | ! Serial poll to clear SRQ. |
| S50 OUTFUT 715: "A18" | ! Execute grid. |
| 360 SEMII 7: UHT UNL TALK 15LISTEN 5 | ! Address 590 to plotter to listen |
| 370 FESUME 7 | ! Set ATN false. |
| 380 STATUS $7,2,5$ | ! Get bus status. |
| 390 IF HOT EIT 8,5 ) THEH | ! Wait for grid to finish. |
| 406 SEHII 7: UNT UNL | ! Untalk and unlisten |
| $416 \mathrm{~S}=\mathrm{SFOLL}(715)$ | ! Serial poll to clear |
|  | SRQ |
| 429 EHI |  |



Figure 4-56. Flowchart of C vs V Plotting Example Program

### 4.12.3 C vs t Programming

The program below demonstrates the basic procedure for programming $C$ vs $t$ measurements over the bus. The program will prompt you to access information located at a specific location after the reading sweep has been completed.

As written, the program uses the $1000 / \mathrm{sec}$ rate, but other rates can be used as well. The computed time information assumes the $1000 / \mathrm{sec}$ rate and start, stop, and step times of 1 msec .

Figure $4-57$ shows a flowchart of the program.

| Program | Comments |
| :---: | :---: |
|  | ! Dimension input string. |
| 20 REMOTE 715 | $!$ Place 590 in remote. |
| 30 CLEAR 7 | $!$ Send device clear. |
| 40 CUTPUT 715: "FGR4\%" | ! Select 100 kHz , 2 nF range. |
| 50 OUTPUT 715; "SGPGX" | $!$ Select $1000 / \mathrm{sec}$ rate, filter off. |
| G0 OUTFUT P15; "T1:1\%" | ! Program sweep on GET mode. |
| $\begin{aligned} & 70 \text { OUTPUT } 715 ; \text { : } 40,1 \mathrm{E}-3, \\ & \text { 1E-Z:1E-3K; } \end{aligned}$ | ! Select DC bias waveform, start, stop, and step times of 1 msec . |
| SG OUTFUT 715; <br> "此: , : 180": | ! Program 5V first V, 100 count. | V, 100 count.

Program Comments
90 OUTFUT 715: "M4k": ! SRQ on sweep done.
100 IISP' afRESE 'COHT" TO MEASURE"
! Display prompt for measurement.
110 PAUSE
$!$ Pause for operator input.
120 OUTFUT 715; " H 1 M "
139 TRIGGER 715
140 STATUS 7:2:5
150 IF HOT EIT (8.5) THEN 140 ! Wait for SRQ to
$160 \mathrm{~S}=\mathrm{SPOLL}(715)$ - Serial poll to clear
17G OUTFUT 715: : EJK"
180 OUTPUT 715 : "NEX"
190 IISF: EUFFER LOCATIOH TOACCESS (1-100)"
200 IHFUTE
210 IFE < 1 ORE $>10 \mathrm{GTHEH}$ 190
220 OUTFUT 715; "EEs:";Bj. "4":
239 OUTPUT 715; "Q18"
240 ENTER 715; A $^{-}$
$250 \mathrm{~T}=.001+.062 * \mathrm{E}$
26日 IISF:"CAPACITAHCE: "; A
27G IISF:"TIME: "; T ! Display time.
280 EHI
occur. SRQ. source.
$!$ Trigger reading sweep.
! Check bus status.
! Transfer data to plot buffer.
! Turn off bias source.
! Prompt for buffer location.
! Input buffer location \#.
! Check for buffer limits.
! Select access from location B.
! Capacitance only.
$!$ Input data.
! Compute time.
$!$ Display data.


Figure 4-57. Flowchart of $C$ vs $t$ Program

### 4.12.4 Accessing Buffer Information

Very often, you will want to read out data from one of the buffers and place that information within a computer array for further analysis. The program below demonstrates the basic method for accessing buffer data and storing the information in a numeric array within the computer. In general, it's a good idea to transfer data to the plotter buffer immediately after the sweep is finished because sending many commands will automatically clear the A/D buffer of any relevant data.

In this instance, data is read into the computer in single reading units for convenience. An alternate method would be to operate the Model 590 in the G4 or G5 data format and output the entire buffer in one long string. Paragraph 4.13 discusses that method in more detail.

A general flowchart of the program is shown in Figure 4-58.

| Program | Comments |
| :---: | :---: |
| 10.0PTIONEASE 1 | ! Set array lower bound to 1. |
|  | $!$ Dimension input array. |
| 30 REMOTE 715 | ! Place unit in remote. |
| 46 CLEAR ? | ! Send device clear. |
| SG OUTPUT $715 ;$ "FGR4N", | $!100 \mathrm{kHz}, 2 \mathrm{nF}$ range. |
| G日GUTFUT 715; "SEFEX" | ! 18/sec reading rate, filter off. |
| 70 OUTFUT 715; "W1\%", | ! Single staircase waveform. |
|  | ! Sweep on GET mode. |
| 90 OUTPUT $715 ;: 40-5$ : 5.0.1.0.0. | ! First V, last V, step V, default.V. |
|  | ! SRQ on sweep done. |
| 11 IISP: FPRESS ©ONT: TO MEGGURE:" <br> 120 FAlse | ! Prompt to start measurement. |
| $150 \mathrm{OUTPUT} 715 ;: \mathrm{H} 1 \mathrm{~K}$ " | ! Turn on bias source. |
| 140 TRIGGER 715 | ! Trigger a reading sweep. |
| 15 DISP: SGLEEP IH PROGRESS: | ! Sweep is now active. |


| Program | Comments |
| :---: | :---: |
| 160 Status | $!$ |
| 179 IF HOT EIT 160 S. 5 ) THEH | ! Wait for SRQ. |
| 180 DISP: SAEEF IDAE <br> REALING BUFFER": | ! Sweep is over. |
| $1905=S P O L L C 715)$ | ! Serial poll to clear SRQ. |
|  | $!$ Transfer data to buffer B. |
| 210 OUTPUT 715; "HEX", | $!$ Turn off bias source. |
| 220 GUTFUT $715 ; ~ " G 1 \% "$ | ! No prefix on data format. |
|  | ! C only, parallel model. |
|  | ! Plotter buffer output, all points. |
| 256 FOR $\mathrm{I}=1$ TO 101 | $!$ Loop for all points. |
| 260 ENTER 715: ACI) | ! Put data point into array. |
| 276 HERT I | ! Next data point. |
| 280 IIISF' "IAATA FOINT TO | ! Prompt for data point. |
| 29011sP*(1-161) |  |
| 30 OL IHPUT $\mathrm{F}^{\circ}$ | ! Input point number. |
| $310 \operatorname{IFP}<1$ ORP $>101$ THEN | ! Check point limits. |
| $320115 F \mathrm{~A}$ (P) | ! Display the point. |
| 350 GOTO 280 | ! Repeat. |
| 340 Efili |  |

The above program can easily be modified to manipulate the data in just about any way you desire. For example, assume that you wish to take a simple average of all points in the data base. To do so, delete lines 280 through 340 above and add the lines below.
$280 \mathrm{~A}=\mathrm{G} \quad$ ! Sum variable $=0$.
$290 \mathrm{FORI}=1$ TO 101
$306 \mathrm{~A}=\mathrm{A}+\mathrm{A}$ (I)
316 HERT I
320 IIISF $\operatorname{A} 101$
350 END
! Loop for 101 points.
! Sum the data points.
! Loop back for next point.
! Display average of points.


Figure 4-58. Flowchart of Buffer Program

## 4．12．5 Obtaining Complete Instrument Status

Use the program below to obtain and display all status words associated with instrument operation．Status words are discussed in detail in paragraphs 4．9．15 and 4．10．

Figure $4-59$ shows a program flowchart．

| Program | Comments |
| :---: | :---: |
| 16 REMOTE P15 | $!$ Place 590 in remote． |
|  | ！Dimension input string． |
| Sarar $\mathrm{I}=0 \mathrm{TO} 1$ | $!$ Loop for all words． |
|  | $!$ Program for status． |
| 59 EHTER 715：As | ！Get status word． |
| 60 DISF Ho | ！Display status word． |
| 70 HEST I | ！Loop back and get next word． |



## 4．12．6 Using the Translator

The program below will demonstrate the basic process for defining Translator words and programming the instru－ ment using the defined words．As written，the program will prompt the operator to select such operating modes as range，frequency，reading rate，as well as voltages and times associated with the bias waveform．

The program also demonstrates methods for using end－ of－line branching to process a service request when an er－ ror condition occurs．An appropriate error message will be displayed on the computer CRT should such an error occur．

Figure 4－60 shows a programming flowchart．

Program
10 IIMAF［100］
15 OH IATR 7 GUTO 780
$20 \mathrm{~F}=715$
25 EHAELE INTE $7: 8$
30 REMOTE P
40 CLEAR 7
50 OUTPUTF；：＂ALIAS
RAHEERA；＂
6G OITPIITP；＂ALIAS FREQF制；＂：
70 GUTFUTF：：GLIAS RATE S积；：
gG DUTPITTF：：ALIAS TRIGGERT1：1䍚；＂

90 OUTPUTP：：ALIAS SRC＿DHALX；＂
100 OUTFUTF；：ALIAE SRC＿OFF HQA：＂
110 OUTFUTF：＂ALIAS

12 E OUTFUT F；＂ALIAS


130 OUTFUT F：：ALIAS TRAHSFER BSK：
140 OUTFUT F：＂ALIAS

156 OUTFIJTF：＂ALIAS SERUICE Mze\％；＂
160 CLEAR

Comments
！Dimension input string．
！Point where to jump on SRQ．
$!$ Primary address is 15.
！Enable bus interrupt on SRQ．
$!$ Put 590 in remote．
！Send device clear．
！Define range Trans－ lator word．
$!$ Define frequency word．
！Define rate Trans－ lator word．
！Define trigger Trans－ lator word（sweep， GET）．
！Define source on word．
！Define source off word．
！Define bias voltage Translator word．
$!$ Define waveform （staircase）and times Translator word．
！Define A＞B buffer transfer word．
！Setup buffer location word．
！SRQ on sweep done or error．
！Clear CRT．

Figure 4－59．Flowchart of Status Word Program

| Program | Comments | Program | Comments |
| :---: | :---: | :---: | :---: |
| 179 GUTPUTF：${ }^{\text {a }}$ TRIG－ | ！Program trigger source | 560 |  |
|  | and mode． | 576 DISP＊STEP TIME |  |
| 180 OUTFUTF：＂SER－ | $!$ Program SRQ mode． | （1mE T065S）＂ |  |
| UICE |  | 560 INFITT TS |  |
| 190IISF＇RAHES＂ | $!$ Prompt for range． | 590 DUTPUTF；‘TINE＂： | ！Program waveform |
|  |  | T1：T2：T3 | times． |
|  |  | 600 OUTPUT $F$ ；＇SRC＿ | ！Turn on bias source． |
| 230 IIISF： $3=241 \mathrm{FF}^{\prime \prime}$＂ |  | 610 TRIGGER 715 | ！Trigger sweep． |
| 240 HISF： $4=2 \mathrm{AF}$ ： |  | 615 COHTROL 7，1：0 | ！Turn off SRQ |
| 250 INFUT R | ！Input range selection． |  | interrupt． |
|  | ！Program range． | 620 status $7,2,8$ <br> 636 IF HOT EIT（6．5）THEN | ！Get bus status． <br> ！Wait for SRQ on |
| 270 CLEAR | ！Clear CRT． | E20 | sweep done． |
| 2SQ IIISP＂：FREQUEHET：${ }^{\text {a }}$ | ！Prompt for frequency． | E40 CLEAR |  |
|  |  | 6S0 OUTFUT F； | ！Transfer buffer A to B |
| 300 IISF： $1=1 \mathrm{NHZ}$＇ |  | ＂TRANSFER＂ |  |
| 316 IHPUT F | ！Input frequency selection． | 660 OUTFUTF；＂SRC | ！Turn off bias source． |
| 320 OUTFUT F：＂FREQ＂： F | ！Program frequency． | 670 DISF＂：FIRET EUAFER LOCATIOH＂： | ！Get first location to access． |
| 350 CLEAR |  | 680 INFIJT $F$ |  |
| 340 IISF： READING RATE： | ！Prompt for reading rate． | 696 IIGP：LAST BUFFER LOLATIOH： | ！Get last location to access． |
|  |  | 700 INFUTL |  |
| 560 IISF： $1=160 / 5 E C:$ |  | P100UTPUTP；：EUF－ | ！Program buffer |
| 370 IISF： $2=20 / \mathrm{SEC} *$ |  | FER＇：${ }^{\text {F }}$ ： 1 | locations． |
| Sea misfus $B=10 . \mathrm{SEC}$ ： |  | $720 \mathrm{~N}=\mathrm{L}-\mathrm{F}+1$ | ！Compute number of |
| 390 DISF ： $4=1, \mathrm{SEC}^{\prime \prime}$ |  |  | locations． |
| 406 IUPIIT 5 | ！Input reading rate selection． | 730 FORI $=1$ T0 N | ！Loop for desired locations． |
| 416 OUTPUT F；＂RATE＊； | ！Program reading | 740 EHTERP；${ }^{\text {a }}$ 全 | ！Input a reading． |
| 5 | rate． | 750 DISP 料 | $!$ Display the reading． |
| 4 CaCLEAR |  | 760 NEST I | ！Loop for next |
| 43 UIISP：‘FIRST BIAS （－zGu To zque＇ | ！Prompt for and input | 77060T0 980 | reading． |
| 446 IHPUTU1 |  | 780 STATUS 7：1：S1 | ！Subroutine to process |
| 450 DISF：LAST BIAS |  |  | SRQ． |
| （－20 T0 20u）＇ |  | $79682=S P O L L(P)$ | ！Serial poll 590. |
| 460 IHPUT UE |  | 806 IF HOTEIT（S2．5） | ！If no error，forget it． |
| 470 IISF＇sSTEP BIAS （－2G TO 2 UU）： |  | THEH 90 <br> B1区 OLITPITF：： 1 U1R： | ！Program for error |
| 4 Ca IHPUT UZ |  |  | Program for error status． |
| 490 IISP：DEFAULTEIAS |  | g2g Enterf ；At | ！Get error status． |
| （－20 To 290）＂ |  | SSORESTORE | $!$ Restore data pointer． |
| 506 INFUT U4 |  | 840 FORI $=5$ To 19 | ！Loop to test status |
| 510 OUTFUTF；＂UOLTS＂ | ！Program bias voltage |  |  |
| ju1；censuzac： | tage parameters | 850 REAITE＊ | ！Read error message． |
|  | （spaces to delimit parameters） | $860 \mathrm{IF} A \neq I, I]=: 1$ <br> THENIISF Eq； | ！Display the error． |
| 526 CLEAR |  | ＂ ERROR＇$^{\text {E EEEF }}$ |  |
| 530 DISP： 6 START TIHE | $!$ Prompt for and | 670 HEKT I | ！Loop for next error bit： |
| （14S T0 65s）＂ | input waveform | G80 IISP：PRESS |  |
| 546 IHPUT T1 | $!$ times． | ＂COHT＂： |  |
| 550 IISP： STOF $^{\text {PIME }}$ |  | 890 PALSE |  |

```
GM0 ENABLE IHTR7:E E
    GOT0 40
910 IHTA: TRIGGER
    DUERFUH:": "NEED
    18GK:
920
    :HOT ISEI":
GEU IATA & CAL LOCKED":
    :"GOHFLIET:
940 IATA:"TRAHSLATOR":
```

! Re-enable SRQ
interrupt.
! Data statements containing error messages.

```
    SGNORENUTE:*
G50 DATA: = IIIM:":
    " IHDLO":*
    "INUALID":
    96. DATA : xHOT IHSTALL-
    EI":, "FMOT ISEI|"
970 IMTA : <4OIMLE OUER-
    LOAD:": \FHT
    LSEI";
990 EHD
```



Figure 4-60. Translator Program Flow Chart

### 4.12.7 Using an External Bias Source

Some devices may require bias voltages greater than the nominal $\pm 20 \mathrm{~V}$ that the Model 590 can supply. The Keithley Model 230 Programmable Voltage source can be used with the Model 590 to supply bias voltages up to $\pm$ 101V DC. The following paragraphs discuss equipment connections and programming notes for using the Model 230 in conjunction with the Model 590 to supply higher bias voltages.

A sample program is also included to help clarify programming techniques. This program will allow you to setup the Model 230 for the desired voltage parameters, generate a sweep, and then plot the data on a digital plotter.

## Instrument Connections

In order to use the program below, instrument connections must be made as outlined below. Figure 3-19 in Section 3 details 230/590 connections, while Figure 3-2 shows device connections in detail. Use suitable coaxial cable for all connections.

1. Connect the Model 230 EXTERNAL TRIGGER OUTPUT to the Model 590 EXTERNAL TRIGGER INPUT.
2. Connect the Model 230 source output to the Model 590 BIAS VOLTAGE INPUT jack.
3. Connect the device being measured to the Model 590 front panel test jacks in the usual manner.
4. The instruments and plotter must be connected to the controller using suitable IEEE-488 cables. See paragraph 3.16 for more information on the types of plotters that can be used.

## Programming Considerations

At the start of the program, you will be prompted to enter first, last, and step bias voltages, which are used to program the Model 230. These voltages are analogous to those used when programming the Model 590 voltage source, except, of course, for the fact that the Model 230 is programmed instead of the Model 590.

The Model 230 dwell time is used as a step duration and can be considered as the time duration for the individual steps in the bias waveform. Care must be taken not to select too short a dwell time or you will cause a Model 590 trigger overrun condition. For example, with a $75 / \mathrm{sec}$ rate, you should be able to use dwell times as short as 30 msec .

In order to synchronize the two instruments, the Model 590 is set up for the one-shot, external trigger mode. With this arrangement, the Model 230 trigger pulse (which occurs at the end of each dwell time) is used to trigger each model 590 reading.

It is important that each reading be allowed sufficient settling time after the Model 590 is triggered. For that reason, the CV analyzer is programmed for a step time equal to $40 \%$ of the entered Model 230 dwell time. In some cases, it may be necessary to change this value for best results.

The Model 230 advances to memory location 2 when first triggered by the controller. Also, since the trigger output pulse does not occur until after the second memory location dwell time, memory location 3 is the first one used.

Other aspects of the program include user-defined frequency, reading rate, and a choice between C vs V and C vs $t$ plot types. Keep in mind that $C$ vs $t$ indicates the buffer index along the $X$ axis, from which you can compute the actual time at each location.

| Program |  | Comments |
| :---: | :---: | :---: |
| 10 | $\mathrm{P} 1=713$ | ! 230 primary address is 13. |
| 20 | $\mathrm{P} 2=715$ | ! 590 primary address is 15 |
| 30 | IIMA*[19日] | $!$ Dimension input string. |
| 46 | CLEAR: | $!$ Clear CRT. |
| 50 | REMOTE P1sFE | ! Put instruments in remote. |
| 68 | CLEAR 7 | ! Send device clear. |
| 76 | DISF: THIS PROGRAM COHTROLSA, |  |
| 80 | IISF: © 250 yOLTAGE SOURCE AHD": | - .... |
| 98 | IISF essacu |  |
|  | AHAL'YZER.' |  |
| 10 C | IISP |  |
| 110 | IISP *PRESS "COHT" |  |
| 124 | False |  |
| 130 | DUTFUTF1; "FQTEX' | ! 230 step, start on GET. |
| 146 | OUTFUT FE: "TEsGR" | ! One-shot external trigger. |
| 150 | CLEAR | ! Clear CRT. |


| Program |  | Comments | 550 | $\omega 1=0.4 \% \mathrm{LH}$ | ！Compute step |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 16.5 |  | ！Prompt for test frequency． | 560 | CLEAR |  |
| 16. | FRERUENC：＂ |  | 570 | IISP ：SELECT FLOT | ！Choose C vs V or |
| 170 | IIISP |  |  | TYPE＇ |  |
| 180 | DISF＊ag＝10GKHZ＂ |  | 580 | IISP |  |
| 190 | DIEP ： $1=14 \mathrm{~Hz}^{\prime \prime}$ |  | 590 | IIISP＂1＝CUSU： |  |
| 296 | INPUT F | ！Input test frequency． | 6610 | IHFUIT $P$ |  |
| 216 | IF F $<0 \mathrm{ORF} \times 1$ THEH 160 |  | 620 | IF $\mathrm{P}<1$ ORF $\mathrm{P} \times 2$ THEN 570 |  |
| 220 | OUTFUT FZ：AFF：＂F： ： $\mathrm{CX}^{\prime}$＂ | ！Program fre－ quency． | 630 | IF $F=1$ THEH $P=0$ ELSE $\mathrm{F}=4$ | ！Convert to plot type parameter． |
| 230 | CLEAR |  | 646 |  |  |
| 240 | DISF：＂SELECT 59日 RAHGE： | ！Range prompt． | 64.5 | OUTFUTPE；＂U，，：＂：＇； | ！Program COUNT． |
| 256 | IISP |  |  |  |  |
| 266 | IIISP： a $^{\text {a AUTORAHESE }}$ |  | 650 |  | ！ 590 external wave－ form delay time |
| 270 | IISP：${ }^{\text {a }}$＝2PF： |  |  | W1：＊8＇， | form，delay time after step change． |
| 280 |  |  | 660 | FOR I $=1 . \mathrm{TOH}+2$ | ！Loop for all vol－ |
| 300 | DISF：＂4＝2NF： |  |  |  | tage bias points． |
| 310 | IHPITR |  | 670 | 解： | ！Select 230 buffer location． |
| 320 | IF E ＜O ORE $>4$ THEA 179 | selection． <br> ！Check range limits． | 680 | OUTFITFF1：＂ 4 ＂；；$W$ ； 68： | ！Program 230 dwell time． |
| 350 | DUTFUTFE：‘R＇s； ＂X＇： | 1 Program 590range． range． | 690 | IF I＜E THEH 720 | ！First two 230 loca－ tions not used． |
| 346 | clear |  | 760 |  | ！Program 230 |
| 356 | DISP：＂SELECT READIHG RATE＂ | ！Prompt for rate． | 710 | F $=\mathrm{F}+51$ | voltage． <br> ！Compute next bias |
| 360 | IIISP |  |  |  |  |
| 380 | IISP： $1=75$ SEC： |  |  |  | Loop for |
| 396 | HISF：2 $=18 . \mathrm{SEC}^{\prime}$ ， |  |  |  |  |
| 409 | DISF： 3 ＝ $10 / \mathrm{SEC}$ ： |  | 736 | clear | ！Clear CRT． |
| 416 | DISF：4 $=1 /$ SEC ${ }^{\text {a }}$ |  | 746 | DISP ：CHECK COHHEC－ |  |
| 420 | IHPUTS 5 | ！Input rate selection． | 750 | TIOHS THEH： <br> IISF＂＂PRESS＂COHT＂TI |  |
| 436 | IF $\mathrm{S}<1 \mathrm{OR} \mathrm{S}$ ¢ 4 THEN 550 |  |  |  |  |
| 435 | IF $S=1$ THEH DITTPIT PS； ＂ POX ＂ | ！If $75 / \mathrm{sec}$ rate， turn off filter． | 760 | OUTPLIT P1；＂M48＂， | $!$ Program 230 to SRQ when sweep |
| 446 |  ses： | $!$ Program reading rate． | 770 | $\mathrm{S} 1=\mathrm{SPOLL}(\mathrm{Pl} 1)$ | done．${ }_{\text {！}}$ Serial poll 230 to |
| 456 | IISF：AFIRSTEIAS＂ | ！Get first bias． |  |  | make sure SRQ is |
| 46 B | IHFIIT F |  |  |  |  |
| 478 | IISFF＂LAET BIAS＂ | ！Get last bias． | 380 | Phose | ！Wait for operator input． |
| 480 | IHPUTL | ！Get step bias． | 790 | OUTFUTFE；＂ATE＇ | ！Turn on 590 bias． |
| 5 Ca | IHPUT S1 |  | 800 | OUTPUTF1；＂F1：${ }^{\text {a }}$＂ | ！Turn on 230 |
| 516 | $\mathrm{H}=\mathrm{ABS}(\mathrm{CL}-\mathrm{F}) \cdot \mathrm{Si} 1+1)$ | ！Compute number readings in sweep． | 816 | TRIGIER P1 | ！Trigger 230 to start sweep． |
| 520 | IF $\mathrm{H}>9 \mathrm{STHEN}$ IISF <br> ： 23 G MEMORY LOCATIOH | ！Check for 230 memory limits． | 820 | STATUS 7， $2: 5$ | ！Check interface status． |
|  | LIMITEXCEEDED＂？ GOTO27日 |  | 880 | IF WOT BIT（ 6,5 ）THEN 820 | ！Wait for SRQ to occur when |
| 536 | IISP：230 IHELL <br> TIHE： | ！Get bias step duration | 846 | S1＝SFOLL ${ }^{\text {P1 }}$ ） | sweep is done． <br> ！Serial poll 230 to |
| 546 | INFUT W |  |  |  | clear SRQ． |


| Program |  | Comments |
| :---: | :---: | :---: |
| 850 | OUTPUT P1: "FEES" | ! Turn off 230 output. |
| 860 | OUTPUTFE; "EESK" | ! Transfer 590 data to buffer B. |
| 876 | OUTFUT Fi; "MEX" | ! Turn off 230 SRQ . |
| 880 | GUTFUT FE; " M1288" | ! 590 SRQ on plotter done. |
| 890 |  :sx" | ! Program plot type. |
| 900 | OUTPIT FE; "A4s, 18" | ! Plot buffer B. |
| 916 | OUTPUT P2: "ARX: | ! Tell 590 to plot. |
| 920 | SEHD 7 ; UHT UNLL TALK 15 LISTEN 5 | ! Address 590 to talk, plotter to listen. |
| 930 | EESUME 7 | $!$ Set ATN false. |
| 946 | STATUS 7,2;S | ! Get bus status. |
| 950 | IF HOT EITCS:5; THEN 940 | ! Wait for SRQ on plotter done. |
| 960 | $8=9 \mathrm{FOLL}(\mathrm{P} 2)$ | ! Serial poll 590 to clear SRQ. |
| 970 | SEHD 7 I UNT UHL | ! Untalk and unlisten the bus. |
| 980 | CIUTPUTFE; : A18: | ! Generate the grid. |
| 990 | SEHD 7: UHT UHAL TALK 15 LISTEH 15 | ! Address 590 to talk, plotter to listen. |
| 16040 | RESUME ? | ! Set ATN false. |
| 1616 | STATUS $7: 2,8$ | $!$ Get bus status. |
| 1829 | IF HOT BITCS:5) THEH 1010 | ! Wait for SRQ on plotter done. |
| 1036 | SEHII 7 U UHT UHL | $!$ Untalk and unlisten the bus. |
| 1049 | $\mathrm{S}=\mathrm{SFOLL}(\mathrm{FE})$ | ! Serial poll 590 to clear SRQ. |
| 1050 | ENIT |  |

### 4.13 BUS TRANSMISSION TIMES

How rapidly the instrument transmits data over the bus is a function of a variety of factors, including selected reading rate and the number of programmed bias steps. The following paragraphs discuss the factors that affect transmission times and give a typical example for a 200 step measurement.

### 4.13.1 Factors Affecting Bus Times

Basically, there are four phases to programming the instru-
ment, performing a sweep, and transmitting the data over the bus as follows:

1. Programming phase: Here, all the necessary operating modes are programmed by sending appropriate commands over the bus. Typically, you will select the range, frequency, reading rate, trigger mode and source, and bias waveform.
2. Trigger phase: In order to perform a sweep, the unit must be triggered in some fashion; that trigger will, of course, depend on the programmed trigger source. If the instrument is to be synchronized with external equipment, an external trigger source should be selected. If you intend to trigger the unit from a controller, use one of the IEEE trigger sources ( $X$, GET, or talk). The best one to use in many situations may be GET for two reasons: (1) with trigger on $X$, the unit will be re-triggered when sending commands, and (2) with trigger on talk, the instrument will be re-triggered when requesting data. In either case, a trigger overrun situation will occur.
3. Sweep phase: During this phase, the instrument cycles through the steps of the bias waveform and takes readings. For the staircase and pulse waveforms, the number of readings depends on the first, last, and step bias voltage values. The number of readings for the $D C$ and external waveforms can be separately programmed, by the count parameter.
4. Data transmission phase: Once the sweep is completed and data is stored in the Model 590 buffer, data must be transmitted to the computer. Basically, there are two general method that can be used: complete sweep data transmission and single point transmission. If your computer can handle a long string of bytes, program the Model 590 to dump its entire buffer in one block. Alternately, a single point-at-a time can be transmitted, if desired.

Keeping these points in mind, the total transmission time from trigger is the sum of the following:

1. Trigger response time: This time period is the interval from the time the unit receives a trigger to the time that is begins the sweep. In most situations, this interval is so small that it can be ignored.
2. Sweep interval: The length of time it takes to complete a sweep depends on the number of data points, reading rate, and programmed start, stop, and step times.
3. Transmission time: The length of time for transmission depends on such factors as the number of bytes of data, as well as the speed of the controller.

## 4．13．2 Optimizing Measurement Speed

The exact steps necessary to optimize measurement speed will depend somewhat on your particular test configura－ tion and requirements．However，there are a few simple rules that will apply in most cases，including：

1．Select the fastest reading rate possible．If you require only capacitance data and can use a DC or external waveform，use the $1000 / \mathrm{sec}$ reading rate．However，if you require C，G，and V data，or must use a staircase or pulse waveform，the fastest rate available is 100 readings per second．In either case，some compromises such as display resolution and reading noise must be taken into account．
2．Program the minimum possible start，stop，and step times for the particular test configuration．Here，some experimentation may be required to determine optimum times based on such factors as settling time of the device under test．Also，you should turn off the analog filter when using short intervals because of the 25 msec settl－ ing time of that filter．
3．Use SRQ to detect end of sweep．Generally，the Model 590 can be＂untouched＂over the bus while it is pro－ cessing a sweep．Thus，the best way to detect the end of a sweep is to program an SRQ on sweep done condi－ tion（M4）and then use the controller to detect when the SRQ occurs．For simpler control situations，a polling method can be used．In other cases，it may be necessary to use interrupt processing to detect the SRQ．
4．Transfer buffer data and turn off the A／D converter when the sweep is finished．The first thing that should be done once the sweep is completed is to transfer the data to buffer $B$ for safekeeping（sending many com－ mands will clear buffer A，destroying your data）．Next， send a command that will turn off the $A / D$ converter （for example，N0）to maximize transmission speed．
5．Select the most compact data format．If your computer can handle long strings in one continuous block，use the G4 data format，which will eliminate reading prefixes and suffixes and dump the entire buffer in one long block．Also，if you are interested only in one type of data （for example only capacitance or conductance），use the O command to select the type of data output（for exam－ ple，send $O 1$ for capacitance only）．Both these steps will minimize the number of bytes that must be transmitted over the bus．
6．Use the fastest controller data transmission mode．Some controllers have more than one transmission mode such as DMA or fast handshake methods．Use the fastest mode to minimize transmission time．

## 4．13．3 Programming Example

The program below was used to determine the time period
from the initial trigger until all data is transferred to the computer．In order to minimize the total time necessary for the complete process，the instrument and computer are set up as follows：

1．The instrument is programmed for the $1000 / \mathrm{sec}$ rate using a DC bias waveform and is externally triggered． A total of 200 points are taken at the minimum start， stop，and step times possible（ 1 msec ）．
2．The instrument data format is programmed to eliminate prefixes and suffixes and to allow a complete buffer dump（G4）．This arrangement minimizes the number of bytes requiring transfer and maximizes efficiency．
3．The HP－85 computer is operated in the fast handshake mode for most rapid data transfer．

Using the program below to take 200 points of capacitance only information，a total interval of 14 seconds from trig－ ger was achieved．

Program Comments

| IIIMA丰［4096］： E丰［40610］ | ！Dimension strings． |
| :---: | :---: |
| 20 IDEUFFER E | ！Define I／O buffer． |
| 308 REMOTE 715 | $!$ Place unit in remote． |
|  | ！DC waveform， 1 msec start stop，step times． |
| 50 OUTPUT 715 ； <br>  | $!10 \mathrm{~V}$ bias， 200 count． |
| 6G OUTPITT 715 ； <br> ＂TS：1世＂： | ！Sweep on external trigger mode． |
| G OUTPUT 715 ； | ！SRQ on sweep done． |
| SQ IUTFUT $715:$＇SEX＇ | $!1000 / \mathrm{sec}$ reading rate． |
| 90 OUTFUT $715:$ <br> ＂ 1 ［184： | ！C only，no prefix or suffix． |
| 106 DUTPUT $715 ;$ ：FGX： | Turn off filter． |
|  | ！Turn on bias source． |
| 120 IISP：AFFL＇TRIG－ GER TO EXTERHAL JACK！ | ！Prompt for trigger． |
| 136 STATHS7，2：S | ！Get bus status． |
| 146 IF HOT EITCS，5） THEH 136 | ！Wait for SRQ． |
|  | ！Transfer data to buffer B． |
|  | Turn off bias source． |
|  | ！Access buffer B readings 1－200． |
| 189 TRAHSFER 715 T0 B伟 | ！Get buffer data from |
| FHS：EOI | 590. |
|  | ！Transfer it to usable string． |
| 260 DISP A＊ | ！Display data． |
| 210 EHI |  |

## SECTION 5 PERFORMANCE VERIFICATION

### 5.1 INTRODUCTION

The procedures outlined in this section may be used to verify that Model 590 accuracy is within the limits stated in the specifications at the front of this manual. Performance verification may be performed when the instrument is first received to ensure that no damage or misadjustment has occurred during shipment, or following calibration, if desired.

If the instrument is found to be in need of calibration, refer to Section 7 of this manual for the correct calibration procedures.

## NOTE

If the instrument is still under warranty (less than one year since the date of shipment), and its performance falls outside the specified range, contact your Keithley representative or the factory to determine the correct course of action.

Information in this section is arranged as follows:
5.2 Environmental Conditions: Gives the temperature and humidity limits for the verification procedure.
5.3 Initial Conditions: Details the warm-up procedure and what to do if the instrument has been stored in environmental extremes.
5.4 Recommended Test Equipment and Sources: Lists equipment necessary for capacitance, conductance, and bias source accuracy verification.
5.5 Verification Limit Calculations: Discusses how to calculate allowed reading limits for the various verification procedures.
5.6 Verification Procedures: Details procedures for verifying both 100 kHz and 1 MHz conductance and capacitance accuracy of the complete instrument, as well as the analog outputs separately. Accuracy checks for the vol-
tage display and internal bias source are also included.

### 5.2 ENVIRONMENTAL CONDITIONS

All measurements should be made at an ambient temperature between $18-28^{\circ} \mathrm{C}\left(65-82^{\circ} \mathrm{F}\right)$ and at less than $70 \%$ relative humidity unless otherwise noted.

NOTE
The ambient temperature must not change more than $\pm 2^{\circ} \mathrm{C}$ from the time the CAL button is pressed until each reading is made.

### 5.3 INITIAL CONDITIONS

Before beginning the verification procedure, turn the Model 590 on and allow it to warm up for at least one hour. If the instrument has been subjected to temperatures outside the range given in paragraph 5.2, additional time must be allowed for internal temperatures to stabilize. Typically, it takes one additional hour to stabilize an instrument that is $10^{\circ} \mathrm{C}\left(18^{\circ} \mathrm{F}\right)$ outside the normal temperature range.

### 5.4 RECOMMENDED TEST EQUIPMENT AND SOURCES

Table 5-1 lists all test equipment and sources required for the verification procedures. Alternate equipment may be used as long as that equipment has specifications at least as good as those listed in the table.

NOTE
Accuracy of conductance and capacitance sources used for the verification procedures must be traceable to recognized standards. For that reason, it is recommended that only the sources listed in Table 5-1 be used for the verification procedures. Accuracy of the procedures with different sources cannot be guaranteed.

Table 5-1. Equipment and Sources Required for Verification

| Description | Specifications | Manufacturer and Model | Use |
| :---: | :---: | :---: | :---: |
| 1.5pF, 18pF, 180pF, 1.8nF, 18nF | * | Keithley 5905, 5906 | Check capacitance accuracy. |
| Source capacitors <br> $1.8 \mu \mathrm{~S}, 18 \mu \mathrm{~S}, 180 \mu \mathrm{~S}, 1.8 \mathrm{mS}$, | * | Keithley 5905,5906 | Check conductance |
| 18 mS Conductance sources |  |  | accuracy. |
| DC Calibrator | 0 to $\pm 200 \mathrm{~V}, \pm 0.002 \%$ | Fluke 343A | Check voltage read-back accuracy. |
| DMM | $\begin{aligned} & 0 \text { to } \pm 20 \mathrm{~V}, \pm 0.009 \% \\ & \geq 10 \mathrm{M} \Omega \text { Input resistance } \end{aligned}$ | Keithley 196 | Check analog outputs and bias source. |

*These values must be characterized and traceable to recognize standards.

### 5.5 VERIFICATION LIMIT CALCULATIONS

Each capacitance source has actual characterized values for the frequencies of interest marked on it. This value will probably differ somewhat from the nominal value. For that reason, it is not possible to provide actual verification limits in this manual. Instead, it will be necessary for you to calculate the limits based on instrument accuracy specifications and the displayed reading.

Calculations for conductance verification limits are not necessary as these limits have been provided in this section.

### 5.5.1 Specification Format

Instrument accuracy is generally specified as a percent of reading value plus so many counts, including a spillover component in counts. For example, the capacitance accuracy of the 2 nF range might be specified as:
$0.25 \%$ of reading $+(200 \mathrm{G} / \mathrm{GFS}+5)$ counts

Here, the $0.25 \%$ value is a percent of reading specification, while the G/GFS term computes the deviation from accuracy due to spillover of conductance into the capacitance reading. The final count value (5) is a fixed number that must also be taken into account when calculating verfication limits.

### 5.5.2 Full Scale Accuracy

For full scale accuracy checks, the limits can be computed from the percent of reading and fixed count specifications
alone. For example, assume the $0.25 \%$ specification applies to the 2 nF range with an actual reading of 1.802 nF . The allowed increment of the reading, $\Delta \mathrm{R}$, would be simply:
$\Delta R=1.802 \times 0.0025+5 / 10,000$
$\Delta R=0.0045+0.0005=0.005$

Note that it is necessary in this case to divide the count value by 10,000 to properly scale units. This scaling factor will, of course, depend on the range.

The reading limits can then be calculated simply by adding and subtracting this value from the actual displayed value. If the lower and higher limits are $R_{L}$ and $R_{H}$, we have:
$\mathrm{R}_{\mathrm{L}}=1.802-0.005=1.797 \mathrm{nF}$
and,
$\mathrm{R}_{H}=1.802+0.005=1.807 \mathrm{nF}$

Thus, the allowable reading range for rated accuracy would be between 1.797 nF and 1.807 nF .

### 5.5.3 Spillover Calculations

The spillover calculations use the actual marked values along with the spillover component in the specifications. For capacitance sources, you can assume a conductance of zero, and the spillover into the conductance reading can be calculated from the spillover factor alone. For example, assume that you are verifying the 2 nF range with an actual capacitance source value of 1.8 nF . The conductance reading limits on the 2 mS range can be calculated as follows:

$$
R=0 \pm(22 \times C / C F S+5) / 10,000
$$

Where: $\mathrm{R}=$ conductance reading limits
$C=$ capacitance source value
CFS = full scale capacitance for selected range $10,000=$ factor to convert from counts to reading units (depends on range)

In our current example, the conductance reading limits would be:

$$
\begin{gathered}
R=0 \pm(22 \times 1.8 / 2+5) / 10,000 \\
R=0 \pm 0.0025 \mu \mathrm{~S}
\end{gathered}
$$

Since $0.1 \%$ tolerance resistors are used for the conductance sources, conductance spillover limits have been provided. Table 5-2 summarizes nominal conductance source values, actual resistances used, along with stray capacitances for each conductances source. Note that these stray capacitance values are factored into the verification limits given in this section.

### 5.5.4 Conductance Specification Considerations

Model 590 accuracy for a $Q$ of less than 20 is specified as typical. Because the conductance verification procedures in this section are performed with a conductance of approximately $90 \%$ of fuil scale, all the conductance limits calculated in this section are based on typical specifications.

### 5.5.5 Analog Output Calculations

Calculations for the analog output tests are done in a similar manner, except that values are in volts and millivolts instead of capacitance, conductance, or counts.

### 5.5.6 Absolute Values

In some cases, the connected source may yield a negative reading on the display. For example, stray inductance for a high value conductance source might result in a negative capacitance display value. In all cases, the absolute value of the displayed reading should be used for the calculations.

Table 5-2. Model 5905 and 5906 Conductance Source Parameters

| Nominal <br> Conductance | DC <br> Resistance* | Actual <br> Conductance* | Stray <br> Capacitance** |
| :---: | :---: | :---: | :---: |
| $1.8 \mu \mathrm{~S}$ | $562 \mathrm{k} \Omega$ | $1.7794 \mu \mathrm{~S}$ | +0.16 pF |
| $18 \mu \mathrm{~S}$ | $56.2 \mathrm{k} \Omega$ | $17.794 \mu \mathrm{~S}$ | +0.16 pF |
| $180 \mu \mathrm{~S}$ | $5.62 \mathrm{k} \Omega$ | $177.94 \mu \mathrm{~S}$ | +0.158 pF |
| 1.8 mS | $562 \Omega$ | 1.7794 mS | +0.004 pF |
| 18 mS | $56.2 \Omega$ | 17.794 mS | -15.42 pF |

* $\pm 0.1 \%$ tolerance.
$* * \pm(10 \%+0.02 \mathrm{pF})$ tolerance


### 5.6 VERIFICATION PROCEDURES

The following paragraphs contain procedures for verifying capacitance and conductance accuracy. In addition, a procedure to verify accuracy of the internal bias source is also included.

The procedures in this section are intended for use only by qualified personnel using accurate and reliable test equipment. If the instrument is out of specifications, refer to Section 7 for calibration procedures.

WARNING
The maximum common-mode voltage (voltage between analog common and chassis ground) is 30V RMS. Exceeding this value may create a shock hazard. Some of the procedures in this section may expose you to dangerous voltages. Use standard safety precautions when such dangerous voltages are encountered.

### 5.6.1 Front Panel Verification

The procedures below outline verification of front panel capacitance and conductance accuracy. For separate verification of the analog outputs, refer to paragraph 5.7.2. Keep in mind that conductance accuracy specifications for $Q<20$ are typical.

To verify each range, you will be required to connect the capacitance or conductance sources to the instrument. In all cases the source must be connected to the instrument directly at the front.panel test INPUT and OUTPUT jacks as shown in Figure 5-1. Under no circumstances are cables to be used, as these will affect the accuracy of the procedures. Figure $5-2$ is a general flowchart for the verification procedures.


Figure 5-1. Mounting Source on Instrument

## 100 kFFz Capacitance Verification

1. Turn on instrument power and allow it to warm up for at least one hour.
2. Initially set up the instrument as follows:

Frequency: 100 kHz
Model : parallel
Filter: on
Reading rate: 10 per second
Zero: off
Trigger mode: sweep
Trigger source: front panel
Bias: off
3. Select the 2 pF range with the RANGE key.
4. Press the CAL button and allow sufficient time for the instrument to complete the calibration cycle. During the cycle, the unit will display the BUSY message.
5. With nothing connected to the test INPUT and OUTPUT jacks press ZERO to enable that mode. Leave zero enabled while taking measurements.
6. Trigger the instrument by pressing the MANUAL button.
7. Connect the 1.5 pF capacitance source to the test IN PUT and OUTPUT jacks.
8. Compute the allowed reading limits from instrument specifications (see front of manual) and the displayed capacitance value by using the appropriate formula at the bottom of Table 5-3. Space has been provided for you to record the limits in the capacitance only column. After computation, verify that the displayed reading is within calculated limits.
9. Calculate the allowed spillover limits by using the formula including the spillover component at the bottom of Table 5-3. Record the reading limits in the table, if desired.
10. Verify that the displayed conductance reading is within the limits calculated above.
11. Repeat steps 4 through 10 for the 20 pF through 2 nF ranges by using the appropriate capacitance sources listed in Table 5-3. Be sure to calibrate and zero the instrument properly for each range as outlined in the appropriate steps above.
12. If you normally use a 5904 input adapter, and wish to verify its performance, connect the 5904 to the 590 test INPUT and OUTPUT jacks and repeat steps 4 through 10 using the correct sources. The range of interest here is 20 nF . Be sure to place the instrument on the proper range by enabling the X10 attenuator (press SHIFT RANGE).

Figure 5-2. General Flowchart of instrument Verification

Table 5-3. Instrument 100 kHz Capacitance Verification

| Range | Nominal Capacitance | Capacitance Accuracy Limits* | Conductance Spillover Limits** |
| :---: | :---: | :---: | :---: |
| $2 \mathrm{pF} / 2 \mu \mathrm{~S}$ | 1.5pF | to | to _- SS |
| $20 \mathrm{pF} / 20 \mu \mathrm{~S}$ | 18 pF | to | _ to _ $\mu$ S |
| $200 \mathrm{pF} / 200 \mu \mathrm{~S}$ | 180 pF | to - pF | _ to _ $\quad \mu \mathrm{S}$ |
| $2 \mathrm{nF} / 2 \mathrm{mS}$ | 1.8 nF | to | to _mms |
| $20 \mathrm{nF} / 20 \mathrm{mSt}$ | 18 nF | to | _ to __ms |

*Calculated as follows:

$$
R=C_{ \pm}[(P \times C) / 100+C 0 / D]
$$

where: $\mathrm{R}=$ Reading limits ( pF or nF )
$C=$ Capacitance source value ( pF or nF )
$P=$ Percent of reading value from specifications (percent)
$\mathrm{C} 0=$ Fixed count-value from specifications
$\mathrm{D}=$ Divisor to adjust count units: $\mathrm{D}=10,000$ $(2 \mathrm{pF}, 2 \mathrm{nF}) ; 1,000(20 \mathrm{pF}, 20 \mathrm{nF}) ; 100(200 \mathrm{pF})$
**Calculated as follows:

$$
\mathrm{R}=0 \pm(\mathrm{M}(\mathrm{C} / \mathrm{CFS})+\mathrm{G} 0) / \mathrm{D}
$$

where: $\mathrm{R}=$ Reading limits ( $\mu \mathrm{S}$ or mS )
$\mathrm{G}=$ Displayed conductance ( $\mu \mathrm{S}$ or mS )
G0 = Fixed count value from specifications
$\mathrm{C}=$ Capacitance source value ( pF or nF )
CFS $=$ Full scale capacitance for selected range ( pF or nF )
$\mathrm{M}=\mathrm{C} / \mathrm{CFS}$ multiplier from specifications
$\mathrm{D}=$ Divisor (see above).
†This range applicable only to Model 5904 Input Adapter.
NOTE: Use absolute $C$ and $G$ values.

## 100 kHz Conductance Verification

1. Turn on instrument power and allow the unit to warm up for at least one hour.
2. Initially set up the Model 590 as follows.

Frequency: 100 kHz
Model: parallel
Filter: on
Reading rate: 10 per second
Zero: off
Trigger mode: sweep
Trigger source: front panel
Bias: off
3. Select the $2 \mu \mathrm{~S}$ range with the RANGE key.
4. Press the CAL button and allow sufficient time for the instrument to complete calibration. BUSY will be displayed while correction is being performed.
5. With nothing connected to the test INPUT and OUTPUT jacks, enable zero. Leave zero enabled while making measurements.
6. Press MANUAL to trigger the unit.
7. Connect the $1.8 \mu \mathrm{~S}$ source to the test INPUT and OUTPUT jacks.
8. Verify that the conductance and capacitance readings are within the limits shown in Table 5-4.
9. Repeat steps 4 through 8 to verify the 20 pF through 2 nF ranges by using the appropriate sources. Be sure to calibrate and zero the instrument properly after selecting each range.
10. If using a 5904 input adapter, connect the 5904 to the instrument test INPUT and OUTPUT terminals and repeat steps 4 through 13. The range of interest is 20 mS . To place the instrument on the proper range, select the X10 attenuator by pressing SHIFI RANGE.

Table 5-4. Instrument 100kHz Conductance

| Range | Nominal <br> Conductance | Conductance <br> Reading Limits** |
| :---: | :---: | :---: |
| $2 \mathrm{pF} / 2 \mu \mathrm{~S}$ | $1.8 \mu \mathrm{~S}$ | 1.7569 to $1.8021 \mu \mathrm{~S}$ |
| $20 \mathrm{pF} / 20 \mu \mathrm{~S}$ | $18 \mu \mathrm{~S}$ | 17.784 to $17.804 \mu \mathrm{~S}$ |
| $200 \mathrm{pF} / 200 \mu \mathrm{~S}$ | $180 \mu \mathrm{~S}$ | 177.68 to $178.20 \mu \mathrm{~S}$ |
| $2 \mathrm{nF} / 2 \mathrm{mS}$ | 1.8 mS | 1.7768 to $1.7820 \mu \mathrm{~S}$ |
| $20 \mathrm{nF} / 20 \mathrm{mS}^{*}$ | 18 mS | 17.745 to $17.843 \mu \mathrm{~S}$ |

[^1]
## 1MHz Capacitance Verification

1. Turn on the Model 590 and allow it to warm up for one hour.
2. Set up the instrument as follows.

Frequency: 1 MHz
Model: parallel
Filter: on
Reading rate: 10 per second
Zero: off
Trigger mode: sweep
Trigger source: front panel
Bias: off
3. Select the 20 pF range with the RANGE button.
4. Press the CAL key and allow sufficient time for the instrument to perform internal calibration. The Model 590 will display the BUSY message during correction.
5. With nothing connected to the test INPUT and OUTPUT jacks, enable zero. Leave zero enabled while taking measurements.
6. Press MANUAL to trigger the unit.
7. Connect the 18 pF capacitor directly to the test INPUT and OUTPUT jacks.
8. Calculate the allowed accuracy reading limits for the selected range from instrument specifications and the displayed capacitance value. Use the correct formula from the bottom of Table 5-5. Record the limits in Table $5-5$, if desired.
9. Verify that the instrument reading is within the limits calculated in step 8 above.
10. Compute the allowed reading limits for conductance spillover with the appropriate formula from Table 5-5. Record the limits, if desired.
11. Verify that the displayed reading is within the limits calculated in step 11.
12. Repeat steps $4^{-}$through 11 for the 200 pF and 2 nF ranges by using the appropriate source values. Be sure to properly calibrate and zero the unit after selecting each range.

## 1MHz Conductance Verification

1. Turn on the instrument and allow it to warm up for one hour.
2. Intitially configure the instrument as follows:

Frequency: 1 MHz
Model: parallel
Filter: on
Reading rate: 10 per second
Zero: off
Trigger mode: sweep
Trigger source: front panel
Bias: off
3. Select the $200 \mu \mathrm{~S}$ range with the RANGE key.
4. Press MANUAL to trigger the sweep.
5. Press CAL and allow sufficient time for the instrument to complete the calibration cycle. BUSY will be displayed during correction.
6. With nothing connected to the test INPUT and OUTPUT jacks, enable zero. Leave zero enabled while making measurements. Press MANUAL.
7. Connect the $180 \mu \mathrm{~S}$ source to the instrument.
8. Verify that the displayed capacitance and conductance readings are within limits (see Table 5-6).
9. Repeat steps 3 through 8 for the 2 mS and 20 mS ranges by using the appropriate sources, as listed in the table. Be sure to properly calibrate and zero the instrument after selecting each range.

Table 5-5. Instrument 1MHz Capacitance Verification

| Range | Nominal Capacitance | Capacitance Reading Limits* | Conductance Spillover Limits** |
| :---: | :---: | :---: | :---: |
| $\begin{gathered} 20 \mathrm{pF} / 200 \mu \mathrm{~S} \\ 200 \mathrm{pF} / 2 \mathrm{mS} \\ 2 \mathrm{nF} / 20 \mathrm{mS} \end{gathered}$ | $\begin{array}{r} 18 \mathrm{pF} \\ 180 \mathrm{pF} \\ 1.8 \mathrm{nF} \end{array}$ | $\begin{array}{lll} - & \text { to } & \mathrm{pF} \\ - & \text { to } & \mathrm{pF} \\ - & \text { to } & \mathrm{nF} \end{array}$ | $\begin{array}{lll}\text { _ } & \text { to } & \mu \mathrm{S} \\ \ldots & \text { to } & \mathrm{mS} \\ \ldots & \text { to__ } & \mathrm{mS}\end{array}$ |

*Calculated as follows:

$$
R=C \pm-[(P \times C) / 100+C 0 / D]
$$

where: $R=$ Reading limits ( $\mathrm{pF} \overline{\text { or }} \mathrm{nF}$ )
$C=$ Capacitance source value ( pF or nF )
$P=$ Percent of reading value from specifications (percent)
$\mathrm{CO}=$ Fixed count value from specifications
$\mathrm{D}=$ Divisor to adjust count units: $\mathrm{D}=1,000(20 \mathrm{pF})$; $100(200 \mathrm{pF})$; $10,000(2 \mathrm{nF})$
**Calculated as follows:

$$
R=0 \pm(M(C / C F S)+G 0) / D
$$

where: $\mathrm{R}=$ Reading limits ( pF or nF )
$\mathrm{G0}=$ Fixed count value from specifications
$\mathrm{C}=$ Capacitance source value ( pF or nF )
CFS $=$ Full scale capacitance for selected range ( pF or nF )
$\mathrm{M}=\mathrm{C} / \mathrm{CFS}$ multiplier from specifications
$\mathrm{D}=$ Divisor: $\mathrm{D}=100(200 \mu \mathrm{~S}) ; 10,000(2 \mathrm{mS})$; $1,000(20 \mathrm{mS})$

NOTE: Use absolute $C$ and $G$ values.

## Table 5-6. Instrument 1MHz Conductance Verification

| Range | Nominal <br> Conductance | Conductance <br> Reading Limits* |
| :---: | :---: | :---: |
| $20 \mathrm{pF} / 200 \mu \mathrm{~S}$ | $180 \mathrm{\mu S}$ | 177.31 to $178.57 \mu \mathrm{~S}$ |
| $200 \mathrm{pF} / 2 \mathrm{mS}$ | 1.8 mS | 1.7737 to 1.7851 mS |
| $2 \mathrm{nF} / 20 \mathrm{mS}$ | 18 mS | 17.736 to 17.852 mS |

*Using Keithley Model 5905 or 5906 sources.

### 5.6.2 Analog Output Verification

Analog output verification procedures are very similar to those used for normal reading verification. The main difference is that you will be measuring an analog output voltage on the rear panel using a DMM. Instead of a capacitance reading, the signal will be a scaled $0-2 \mathrm{~V}$ value. Also, since software accuracy compensation is not applied to these signals, the allowable tolerances are substantially larger than for front panel readings.

The same sources are to be used for these tests; refer to Figure 5-1 for connections. Figure 5-3 shows a general flowchart of the analog output verification procedures.

## 100 kHz Capacitance Verification

1. Turn on instrument power and allow it to warm up for at least one hour.
2. Initially set up the instrument as follows:

Frequency: 100 kHz
Filter: on
Bias: off
3. Connect the DMM to the CAPACITANCE ANALOG OUTPUT jack on the rear panel, as shown in Figure 5-4. The DMM high terminal should be connected to
the center conductor, and the low terminal should be connected to the cable shield. Select the DCV function and autoranging.
4. Select the 20 pF range with the RANGE key, then zero the DMM.
5. Connect the 18 pF capacitance source to the test INPUT and OUTPUT jacks.
6. Compute the allowed voltage limits from instrument specifications (see front of manual) and the DMM reading by using the appropriate formula at the bottom of Table 5-7. Space has been provided for you to record the limits in the capacitance only column. After computation, verify that the measured voltage is within calculated limits.
7. Calculate the allowed limits by using the formula including the spillover component at the bottom of Table $5-7$. Record the voltage limits in the table, if desired.
8. Verify that the measured voltage is within the limits calculated above.
9. Repeat steps 4 through 8 for the 200 pF and 2 nF ranges by using the appropriate capacitance and conductance sources listed in Table 5-7.
10. If you normally use a 5904 input adapter, and wish to verify 20 nF range performance, connect the 5904 to the 590 test INPUT and OUTPUT jacks and repeat steps 4 through 8 using the correct sources. Be sure to place the instrument on the proper range by enabling the X10 attenuator (press SHIFT RANGE).


Figure 5-3. General Flowchart of Analog Output Verification

Table 5-7. Analog Output 100kHz Capacitance Verification

| Range | Nominal <br> Capacitance | Nominal <br> Output | Capacitance <br> Output Limits* | Conductance Output <br> Spillover Limits** |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| $20 \mathrm{pF} / 20 \mu \mathrm{~S}$ | 18 pF | 1.8 V | - to -V | $-\mathrm{to}-\mathrm{V}$ |
| $200 \mathrm{pF} / 200 \mu \mathrm{~S}$ | 180 pF | 1.8 V | - to -V | - to -V |
| $2 \mathrm{nF} / 2 \mathrm{mS}$ | 1.8 nF | 1.8 V | - to -V | - to -V |
| $20 \mathrm{nF} / 20 \mathrm{mSt}$ | 18 nF | 1.8 V | to -V | - to -V |

*Calculated as follows:

$$
\mathrm{O}=\mathrm{C} \pm[(\mathrm{P} \times \mathrm{C}) / 100+\mathrm{V} / 1,000]
$$

where: $\mathrm{O}=$ Analog output voltage limits in volts
$\mathrm{C}=$ Displayed capacitance (converted to volts)
$P=$ Percent of reading value from specifications (percent)
$\mathrm{V}=$ Fixed offset value from specifications (mV)
**Calculated as follows:

$$
\mathrm{O}=0 \pm[(\mathrm{M}(\mathrm{C} / \mathrm{CFS})+\mathrm{V}) / 1,000]
$$

where: $\mathrm{O}=$ Conductance analog output voltage limits in volts
$\mathrm{M}=\mathrm{C} / C F S$ multiplier
$\mathrm{C}=$ Capacitance source
CFS $=$ Full scale capacitance
$\mathrm{V}=$ Fixed offset value (mV)
tThis range applicable only to Model 5904 Input Adapter.
NOTE: Use absolute values for $C$ and $G$ readings.


Figure 5-4. Connecting for Analog Output Capacitance Verification

## 100 kHz Conductance Verification

1. Turn on instrument power and allow the unit to warm up for at least one hour.
2. Initially set up the instrument as follows:

Frequency: 100 kHz
Filter: on
Bias: off
3. Connect the DMM to the CONDUCTANCE ANALOG OUTPUT jack on the rear panel, as shown in Figure 5-5. The DMM high terminal should be connected to the center conductor, and the low terminal should be connected to the cable shield. Select the DCV function and autoranging.
4. Select the $20 \mu \mathrm{~S}$ range with the RANGE key, then zero the DMM.
5. Connect the $18 \mu \mathrm{~S}$ source to the test INPUT and OUTPUT jacks.
6. Verify that the measured voltages are within the limits shown in Table 5-8.
7. Repeat steps 4 through 6 to verify the $200 \mu \mathrm{~S}$ and 2 mS ranges by using the appropriate sources.
8. If using a 5904 input adapter, verify the 20 mS range. To do so, connect the 5904 to the instrument test INPUT and OUTPUT terminals and repeat steps 4 through 6. To place the instrument on the proper range, enable the X10 attenuator by pressing SHIFT RANGE.

## 1MHz Capacitance Verification

1. Turn on instrument power and allow it to warm up for at least one hour.
2. Initially set up the instrument as follows:

Frequency: 1 MHz
Filter: on
Bias: off
3. Connect the DMM to the CAPACITANCE ANALOG OUTPUT jack on the rear panel, as shown in Figure 5-4. The DMM high terminal should be connected to the center conductor, and the low terminal should be connected to the cable shield. Select the DCV function and autoranging
4. Select the 20 pF range with the RANGE key, then zero the DMM.
5. Connect the 18 pF capacitance source to the test INPUT and OUTPUT jacks.
6. Compute the allowed voltage limits from instrument specifications (see front of manual) and the displayed DMM reading by using the appropriate formula at the bottom of Table 5-9. Space has been provided for you to record the limits in the capacitance only column. After computation, verify that the measured voltage is within calculated limits.
7. Calculate the allowed voltage limits by using the formula including the spillover component at the bottom of Table 5-9. Record the voltage limits in the table, if desired.
8. Verify that the measured voltage is within the limits calculated above.
9. Repeat steps 4 through 8 for the 200 pF and 2 nF ranges by using the appropriate capacitance and conductance sources listed in Table 5-9.

Table 5-8. Analog Output 100kHz Conductance Verification

| Range | Nominal <br> Conductance | Nominal <br> Output | Conductance <br> Output Limits* |
| :---: | :---: | :---: | :---: |
| $20 \mathrm{pF} / 20 \mu \mathrm{~S}$ | 18 | $\mu \mathrm{~S}$ | 1.8 V |
| $200 \mathrm{pF} / 200 \mu \mathrm{~S}$ | 180 SS | 1.7616 to 1.797 V |  |
| $2 \mathrm{nF} / 2 \mathrm{mS}$ | 1.7616 to 1.797 V |  |  |
| $20 \mathrm{nF} / 20 \mathrm{mSt}$ | 18 mS | 1.8 V | 1.7438 to 1.815 V |
| 18 | 1.8 V | 1.726 to 1.833 V |  |

tThis range applicable only to Model 5904 Input Adapter *Using Keithley Model 5905 or 5906 sources.

## 1MHz Conductance Verification

1. Turn on instrument power and allow the unit to warm up for at least one hour.
2. Initially set up the instrument as follows:

Frequency: 1 MHz
Filter: on
Bias: off
3. Connect the DMM to the CONDUCTANCE ANALOG OUTPUT jack on the rear panel, as shown in Figure 5-5. The DMM high terminal should be connected to the
center conductor, and the low terminal should be connected to the cable shield. Select the DCV function and autoranging.
4. Select the $200 \mu \mathrm{~S}$ range with the RANGE key and zero the DMM.
5. Connect the $180 \mu \mathrm{~S}$ source to the test INPUT and OUTPUT jacks.
6. Verify that the measured voltages are within the limits shown in Table 5-10.
7. Repeat steps 4 through 6 to verify the 2 mS and 20 mS ranges by using the appropriate sources.

Table 5-9. Analog Output 1MHz Capacitance Verification

| Range | Nominal Capacitance | Nominal Output | Capacitance Output Limits* | Conductance Output Spillover Limits** |
| :---: | :---: | :---: | :---: | :---: |
| $20 \mathrm{pF} / 200 \mu \mathrm{~S}$ | 18 pF | 1.8 V | V | V |
| $200 \mathrm{pF} / 2 \mathrm{mS}$ | 180 pF | 1.8 V |  | to _- V |
| $2 \mathrm{nF} / 20 \mathrm{mS}$ | 1.8 nF | 1.8 V | to | to |

*Calculated as follows:

$$
\mathrm{O}=\mathrm{C} \pm[(\mathrm{P} \times \mathrm{C}) / 100+\mathrm{V} / 1,000]
$$

where: $\mathrm{O}=$ Analog output voltage limits in volts
$\mathrm{C}=$ Displayed capacitance (volts)
$\mathrm{P}=$ Percent of reading value from specifications (percent)
$\mathrm{V}=$ Fixed offset value from specifications (mV)
**Calculated as follows:

$$
\mathrm{O}=0 \pm[(\mathrm{M}(\mathrm{C} / \mathrm{CFS})+\mathrm{V}) / 1,000]
$$

where: $\mathrm{O}=$ Analog output voltage limits in volts
$\mathrm{C}=$ Capacitance source value
$\mathrm{M}=\mathrm{C} / \mathrm{CFS}$ multiplier
CFS $=$ Full scale capacitance
$\mathrm{V}=$ Fixed offset value (mV)
NOTE: Use absolute values for $C$ and $G$ readings.


Figure 5-5. Connections for Analog Output Conductance Verification

## Table 5-10. Analog Output 1MHz Conductance Verification

| Range | Nominal <br> Conductance | Nominal <br> Output | Conductance <br> Output Limits* | Capacitance Output <br> Spillover Limits* |
| :---: | :---: | :---: | :---: | :---: |
| $20 \mathrm{pF} / 20 \mu \mathrm{~S}$ | $180 \mu \mathrm{~S}$ | 1.8 V | 1.744 to 1.81 .5 V | -0.068 to +0.068 V |
| $200 \mathrm{pF} / 2 \mathrm{mS}$ | 1.8 mS | 1.8 V | 1.725 to 1.833 V | -0.067 to +0.067 V |
| $2 \mathrm{nF} / 20 \mathrm{mS}$ | 18 mS | 1.8 V | 1.654 to 1.904 V | -0.268 to -0.268 V |

*Using Keithley Model 5905 or 5906 sources.

### 5.6.3 Complete Model 5904 Verification

From the factory, the Model 590 is calibrated to use the 5904 input adapter only on the $20 \mathrm{nF} / 20 \mathrm{mS}$ range. However, if you have field calibrated the instrument for use with the 20 pF through 2 nF ranges (see paragraph 7.3), you can verify accuracy of that calibration by repeating the procedures from paragraph 5.7.1 and 5.7.2 using the appropriate sources, as indicated below:
$20 \mathrm{pF} / 20 \mu \mathrm{~S}: 18 \mathrm{pF} / 18 \mu \mathrm{~S}$
$200 \mathrm{pF} / 200 \mu \mathrm{~S}: 180 \mathrm{pF} / 180 \mu \mathrm{~S}$
$2 \mathrm{nF} / 2 \mathrm{mS}: 1.8 \mathrm{nF} / 1.8 \mathrm{mS}$

### 5.6.4 Voltage Verification

The following procedures are intended to verify the accuracy of the internal bias source as well as the read-back accuracy of the voltage display. Figure $5-6$ shows a general flowchart of the voltage verification procedures.

## Internal Bias Source and 20V Range Read-Back Accuracy

1. Turn on the Model 590 and allow it to warm up for one hour.
2. Connect the DMM to the VOLTAGE BLAS MONITOR
jack, as shown in Figure 5-7. Select the DCV function and autoranging on the DMM.
3. Set up the instrument as follows:

Waveform: DC
Trigger source: front panel
Trigger mode: one-shot
Bias: on
4. Use the PARAMETER key to program a first bias voltage value of exactly 19.000 V .
5. Press the MANUAL key to trigger a reading.
6. Note the reading on the DMM and record its value (the actual measured values will be required for the 20 V range read back check outlined below). Check to see that the reading is within the limits stated in Table 5-11.
7. Calculate the allowable range of the Model 590 voltage display reading using the measured value obtained in step 6 and the formula at the bottom of Table 5-11.
8. Note the reading on the Model 590 voltage display. Check to see that displayed reading is within the limits calculated in step 7.
9. Repeat steps 4 through 8 for the remaining voltages listed in Table 5-11. For each programmed step, measure the voltage and verify that the value is within prescribed limits. Then use the measured voltage value to calculate the allowed limits of the Model 590 voltage display, and compare the actual display to calculated limits.


Figure 5-6. Voltage Verification Flowchart

Table 5-11. Internal Bias Source and 20V Range Read-Back Accuracy

| Programmed Voltage |  |  |
| :---: | :---: | :---: |
| -19.000V | -19.02 to -18.98 V | V |
| $-15.000 \mathrm{~V}$ | -15.0175 to -14.9825 V |  |
| -10.000V | -10.015 to -9.985 V |  |
| - 5.000 V | - 5.0125 to -4.9875 V |  |
| 0.000 V | -0.01 to +0.01 V |  |
| $+5.000 \mathrm{~V}$ | +4.9875 to +-5.0125 V |  |
| $+10.000 \mathrm{~V}$ | +9.985 to +10.015 V |  |
| $+15.000 \mathrm{~V}$ | +14.9825 to +15.0175 V |  |
| $+19.000 \mathrm{~V}$ | +18.98 to +19.02 V |  |

*Calculated as follows:

$$
V=M \pm(0.0005 \mathrm{M}+0.005)
$$

where: $V=$ Read-back voltage limits
$\mathrm{M}=$ Actual measured internal bias source value


Figure 5-7. Connections for Voltage Verification

## 200V Range Read-Back Accuracy Check

The internal bias voltage read back circuits are set to the 200 V range whenever the external bias source is selected. The procedure below will allow you to check the accuracy of the voltage display when reading external bias source.

## WARNING

Hazardous voltages are used in many of the following steps. Take care not to contact these voltages, which could cause personal injury or death.

## CAUTION

Do not place the DC calibrator used in this procedure to standby with the Model 590 bias on. Doing so may blow the bias fuse. Always turn off the Model 590 bias before placing the calibrator in standby.

1. Connect the external DC calibrator to the VOLTAGE BIAS INPUT jack, as shown in Figure 5-8. Initially set the calibrator to 0.0000 V and place the unit in operate.
2. Tum on the Model 590 and allow it to warm up for one hour.
3. Turn on the DC calibrator and allow it to warm up for the prescribed period.
4. Set up the Model 590 as follows:

Waveform: external
Trigger source: front panel
Trigger mode: one-shot
Bias: on
5. Set the DC calibrator to exactly -190.000 V .
6. Trigger a reading by pressing MANUAL.
7. Note the reading on the Model 590 voltage display, and compare it to the limits in the first line of Table 5-12.
8. Repeat steps 5 through 7 for each voltage listed in Table 5-12. At each voltage step, compare the displayed Model 590 reading with the limits listed in the table.
9. Turn off the Model 590 bias source (BIAS ON LED off) and then place the DC calibrator in standby.

Table 5-12. Limits for 200V Read-Back Range

| Applied Voltage | Read-Back Limits |
| :--- | :--- |
| -190.000 V | -190.15 to -189.85 V |
| -175.000 V | -175.14 to -174.86 V |
| -150.000 V | -150.13 to -149.87 V |
| -125.000 V | -125.11 to -124.89 V |
| -100.000 V | -100.10 to -99.90 V |
| -75.000 V | -75.09 to -74.91 V |
| -50.000 V | -50.08 to -49.92 V |
| -25.000 V | -25.06 to -24.94 V |
| 0.000 V | -0.05 to +0.05 V |
| +25.000 V | +24.94 to +25.06 V |
| +50.000 V | +49.92 to +50.08 V |
| +75.000 V | +74.91 to +75.09 V |
| +100.000 V | +99.90 to +100.10 V |
| +125.000 V | +124.89 to +125.11 V |
| +150.000 V | +149.87 to +150.13 V |
| +175.000 V | +174.86 to +175.14 V |
| +190.000 V | +189.85 to +190.15 V |



Figure 5-8. Connections for 200V Read-Back Verification

## SECTION 6 PRINCIPLES OF OPERATION

### 6.1 INTRODUCTION

This section contains an overall functional description of the Model 590 as well as detailed operating principles for various circuits within the instrument. Some descriptions include simplified block diagrams or schematics as an aid to understanding. Detailed schematic diagrams and component layout drawings for the various circuit boards are located in Section 8.

Section 6 is arranged as follows:
6.2 Functional Description: Presents Model 590 circuitry in block diagram form and gives an overview of circuit operation.
6.3 Digital Circuits: Outlines the operation of digital circuits such as the hardware multiplier and microcomputer.
6.4 Analog Circuitry: Describes operation of the analog circuitry including the A/D converter.
6.5 100kHz Capacitance Module: Details operation of the 100 kHz capacitance module including measurement principles.
6.6 1MHz Capacitance Module: Gives a detailed description of the 1 MHz capacitance module and its operating principles.
6.7 Power Supplies: Discusses the power supplies that feed the various circuits within the instrument.
6.8 Display Board: Covers operation of the display and keyboard circuits.
6.9 Cable Correction: Outlines the basic principles of cable correction used by the instrument to compensate for transmission line effects.

### 6.2 FUNCTIONAL DESCRIPTION

A simplified block diagram of the instrument is shown in Figure 6-1. The unit is essentially divided into two sections, analog and digital. These two sections are electrically isolated to allow analog common to be floated while maintaining digital common at chassis ground potential.

Key analog circuits include switching and control circuits, the 100 kHz and 1 MHz capacitance modules, the A/D converter, and the internal bias voltage source. Important digital circuits include the microcomputer, keyboard, display, and IEEE-488 interface circuits. Separate power supplies are included for the analog and digital sections in order to maintain isolation.

The device under test is connected to the selected 100 kHz or 1 MHz module. The module applies a composite of the nominal 15 mV test frequency ( 100 kHz and 1 MHz ) and the programmed bias voltage to the device under test, and it then measures the resulting 100 kHz or 1 MHz current through that device. The module then converts-the resulting capacitance and conductance signals into a scaled $0-2 \mathrm{~V}$ signal usable by the A/D converter.

The A/D converter digitizes the capacitance, conductance, and bias voltage signals for transmission to the microcomputer. The transmission process is done in serial form via an opto-isolator in order to maintain the necessary electrical isolation mentioned previously.

An internal voltage source supplies up to $\pm 20 \mathrm{~V}$ of bias that can be applied to the circuit under test. Like the remaining analog circuits, this supply is controlled by signals from the microcomputer.

The clock circuits generate the necessary signals to synchronize both analog and digital circuits. An 8 MHHz signal is used both for the 1 MHz module (if present) and the microcomputer. In this case, isolation is maintained by sending the clock signal through a pulse transformer instead of an opto-isolator because of the high frequency involved. The 8 MHz signal is divided down to 4 MHz for the A/D converter and 800 kHz for the 100 kHz capacitance module.

The 6809 -based microcomputer supervises virtually all operating aspects of the instrument, including control of the $A / D$ converter, voltage source, and capacitance modules. Control information from the microcomputer to these circuits is transmitted in isolated form through optoisolators. Additional circuits controlled by the microcomputer include the display, keyboard, and the IEEE-488 interface.


Figure 6-1. Block Diagram

The power supply circuits convert the applied AC power line voltage into various DC voltages used by the instrument. Fundamentally, the power supply is divided into analog and digital sections. Analog supplies include $\pm 5$, $\pm 15$, and $\pm 30 \mathrm{~V}$ sections, while a single +5 V supply powers the digital circuits.

### 6.3 DIGITAL CIRCUITRY

The paragraphs below discuss the various digital circuits used in the Model 590 . Figure 6-2 shows a simplified block diagram of the digital circuits, and a complete schematic is located on drawing number 590-126 located at the end of Section 8.

### 6.3.1 Microprocessor

The 68809 processor provides the intelligence to control the instrument. The B designation indicates that the processor is a 2 MHz unit, which is the frequency of operation for the MPU bus. As shown in the programming model of Figure 6-3, the 6809 has two 16-bit index registers ( X and Y ), two 16 -bit stack pointers ( U and S), a 16 -bit program counter, and two eight-bit accumulators, A and B. The direct page and condition code registers round out the register complement.

Key 6809 signal lines include:
Data lines (D7-D0): The MPU has an eight-bit data bus use to read and write information to external devices.

Address lines (A15-A0): The sixteen address lines give the 6809 a 64 K byte addressing capability.

Read/write $(\mathrm{R} / \overline{\mathrm{W}}$ ): The state of the read/write line determines whether data is being read from or transferred to external devices. A read occurs when this line is high, while a write takes place when the line is low.

Bus clock ( E and Q ): Quadrature 2 MHz bus clock signals are provided by these two lines.

Reset ( $\overline{\text { RESET }})$. This terminal is held low for 690 msec upon power up to generate a system reset. The reset signal is generated by U302 and associated components.

Interrupt request $(\overline{\mathrm{RQ}})$ : The 1.024 msec system clock is connected to this terminal to cause system interrupt timing at that interval. This interrupt-generated timing controls such operating aspects as A/D conversion. The interrupt signal is derived by dividing the 2 MHz E clock by 2048 , a function performed by U342.

Fast interrupt request ( $\overline{\text { FIRQ }}$ ): Pulling this line low causes a fast interrupt sequence, in which case the 6809 stacks only the condition code register and program counter, in contrast to a full interrupt, which causes all registers to be stacked. In the Model 590, FIRQ is connected to the IEEE-488 GPIA chip $\bar{R} Q$ terminal, which means that IEEE bus interrupts are processed on a fast interrupt basis.

Non-maskable interrupt (NMI): As the name implies, a low signal on this terminal causes an interrupt that cannot be disabled (masked) by setting the IRQ flag in the condition code register. This terminal is connected to the VIA IRQ pin, meaning that interrupts associated with I/O operations are processed on an NMI basis.

MPU clock (EXTAL): An 8 MHz clock, which originates on the mother board, is applied to this terminal. The clock passes through T301 for isolation and is re-shaped by U331A before being applied to the MPU. The 6809 internally divides this signal by four to generate the 2 MHz E and $Q$ bus clock signals.


Figure 6-2. Digital Circuit Block Diagram


Figure 6-3. 6809 Microprocessor Programming Mode

### 6.3.2 Memory Circuits

## ROM Memory

A total of 32 K bytes of program coding is stored in two ROMS, U306 and U307. Each of these devices is a 27128 ROM IC capable of storing 16 K bytes.

## RAM Memory

U308 and U309 provide 16K bytes of working storage for the operating system. Each device is an 8 K byte static RAM (6264), which, unlike dynamic RAM, requires no refreshing circuitry. Among other things, the RAM ICs are used to store data taken as part of a reading sweep. This form of RAM storage is volatile, meaning that data is lost when power is removed.

## NVRAM

Non-volatile memory storage is provided by U310, which is a 2 K byte storage device. This IC stores such data as calibration and setup configuration constants that must be retained when power is removed.

## Address Decoding

Because none of the memory ICs is capable of completely decoding the entire 64 K address space, additional decoding is necessary. U303 decodes for the memory circuits, as well as for the VIA and IEEE chips. U305 decodes for the display
latches and hardware multiplier, while U328 provides additional decoding for the hardware multiplier and associated latches.

## Memory Mapping

Table 6-1 summarizes the address locations for the various memory ICs. In addition, locations for various chips such as the VIA and GPIA are also included.

Table 6-1. Memory Map

| Address |  |  |
| :--- | :--- | :--- |
| Hexadecimal | Decimal | Description |
| $\$ 0000$ | 0 |  |
|  |  | Write X register, read <br> high-order multiplier |
| $\$ 0002$ | 2 | Write Y register, read |
|  |  | low-order multiplier |
| $\$ 1000-\$ 1001$ | $4,096-4,097$ | Display latches |
| $\$ 1040-\$ 1041$ | $4,160-4,161$ | Display latches |
| $\$ 1080$ | 4,224 | Register C, multiplier |
| $\$ 101$ | 4,25 | IRQ counter clear |
| $\$ 1100-\$ 1107$ | $4,352-4,359$ | 9914A GPIA |
| $\$ 1200-\$ 120 \mathrm{~F}$ | $4,608-4,623$ | 6522A VIA |
| $\$ 1400-\$ 17 \mathrm{FF}$ | $5,120-6,143$ | NVRAM |
| $\$ 2000-\$ 3 F F$ | $8,192-16,383$ | RAM \#1 |
| $\$ 4000-\$ 5 F F F$ | $16,384-24,575$ | RAM \#2 |
| $\$ 6000-\$ F F F$ | $24,576-65,535$ | Program ROMs |

### 6.3.3 Hardware Multiplier

U333 is the hardware multiplier (7216) used in the Model 590 in order to achieve fast, real-time digital processing at speeds that would otherwise be impossible using software. This versatile IC can multiply two 16-bit numbers and provide a 32 -bit, double-precision product in only 75 nsec . This speed and versatility allow the Model 590 to perform array processing on buffer data with greater efficiency.

## Multiplier IC Connections

Multiplicand data inputs ( $\mathrm{X} 15-\mathrm{X} 0$ ): These terminals provide 16-bit input for the multiplicand.

Multiplier data inputs ( $\mathrm{Y} 15-\mathrm{Y} 0$ ): The 16 -bit value of the multiplier is applied to these inputs.

Product outputs ( $\mathrm{P} 15-\mathrm{P} 0$ ): The most significant or least significant word of the product are made available at this port, depending on the state of MSPSEL (see below).

Product select (MSPSEL): The state of this line determines whether the product port assumes the value of the low or high-ordered bits of the 32 -bit product. When set low, the most significant product (MSP) will be selected, while the least significant product (LSP) will appear on the lines when MSPSEL is high.

Output port enable ( $\overline{\mathrm{OEP}}$ ): A low logic level on this terminal is necessary to enable the product port, which has tri-state outputs.

Clock terminals (CLKX, CLKY, CLKM, CLKL): Clock signals for the X, Y, MSP, and LSP registers are applied to these terminals.

## Multiplier/MPU Interfacing

Since the multiplier operates on 16-bits words and the MPU has an eight-bit data bus, additional support ICs are necessary to interface the multiplier to the MPU. U318 acts as a data latch for the low ordered eight bits of the product, while U323 performs a similar function when writing to the highest ordered eight bits of the X or Y registers. Additional decoding is provided by U328, which generates the necessary clock or enable signals for the data latches and hardware multiplier itself.

## Typical Calculation Sequence

A typical multiplication sequence is as follows:

1. The high-ordered byte (X15-X8) of the multiplicand is written to the input data latch (U323).
2. The low-ordered byte $(\mathrm{X} 7-\mathrm{X} 0)$ is then written to the multiplier. This action automatically latches the complete 16 -bit multiplicand into the X register.
3. The process is then repeated for the multiplier, with the 16 -bit word latched into the $Y$ register, using the twostep process above.
4. The CLKM and CLKL terminals are then toggled to perform the multiplication process.
5. The product is then read through the product port (P15-PO). During this process, OEP is set low to enable the port.

### 6.3.4 Input/Output

Much of the interfacing between the MPU and other circuits in the Model 590 is performed by U313, a 6522A VIA (versatile interface adapter). This peripheral IC has two eight-bit bidirectional ports, two 16-bit timers, and includes automatic handshaking capabilities.

The input/output functions performed by U313 include:

1. Control word transmission: The 32-bit control word, which supervises the analog circuits, is sent over optoisolators U317, U322, and U326 via the CLK, DATA, and STB lines.
2. A/D data input: A/D data, in serial form is transmitted through opto-isolators U325 to U332, which converts the serial data into nibble form, is then read by the VIA through the C0-C3 lines.
3. Analog status information: Status bits, coming from the A/D converter, voltage source, and C modules, are transmitted through U320 and then read by the VIA.
4. External trigger input/output: The VIA reads the status of the external trigger input through its CA2 line, and it controls the external trigger output with the CA1 pin.
5. Display digit select and keyboard read: Control of display digits and keyboard matrix row select is performed through the DATA' and CLK' lines. Keyboard matrix reading is done through $\mathrm{SO}-\mathrm{S} 3$.
6. Calibration lock switch read: The status of the calibration lock switch is read through the PA2 terminal of the VIA.

### 6.3.5 IEEE-488 Interface

ICs associated with the IEEE-488 interface include U304, U311, and U313. U304 and U312 are bus drivers needed to supply the drive capability for up to 15 devices. U311 is a 9914A GPIA (general purpose interface adapter), which is designed to perform many bus functions automatically, thus freeing the MPU for more important tasks. For example, the GPIA can perform input/output handshaking automatically.

## MPU Interfacing

Terminals on the MPU side of the GPIA include:
Data lines (D7-D0): These lines are connected to the D7-D0 lines of the MPU data bus.

Register select lines (RS2-RS0): The register select lines are connect to the A2-A0 lines of the address bus, and they are used to select among the 14 internal registers (seven read, seven write).

Clock ( E ): The 2 MHz E clock is applied to this terminal.
Read/wxite $(R / \bar{W})$ : The state of this line determines whether a read or write action to a specific GPIA register is to occur.

Interrupt ( $\overline{\mathrm{IRQ}})$ : The $\overline{\mathrm{IRQ}}$ line is connected to the $6809 \overline{\mathrm{FIRQ}}$ terminal, allowing fast interrupt processing of IEEE-488 interrupts.

Reset $(\overline{\mathrm{RST}})$ : This terminal is held low for approximately 690 msec upon power up to reset the GPIA.

Chip enable $(\overline{C E})$ : The GPIB is enabled for a read or write action by placing $\overline{C E}$ low.

## Bus Interfacing

Bus lines are grouped into three general catagories: data, handshake, and bus management. All lines are active low with a true condition represented by approximately 0 V .

Data lines: The data lines are DIO8 through DIO1. DIO8 is the most significant bit, and DIO1 is the least significant bit.

Handshake lines: These lines, which include NRFD (Not Ready For Data), NDAC (Not Data Accepted), and DAV (Data Valid) are used to ensure proper transfer of each data byte.

Bus management lines: The following lines are used to send the appropriate uniline commands: REN (Remote Enable), IFC (Interface Clear), SRQ (Service Request), ATN (Attention), and EOI (End or Identify).

### 6.3.6 Data Segment Latches and Drivers

The Model 590 uses a multiplexed display, meaning that each display digit is actually on for only a brief period of time. This arrangement does minimize the amount of hardware necessary to drive the display, but at the expense of MPU overhead.

As a compromise between hardware and software requirements, data latches are incorporated to store display segment information. U319, U324, U327, and U329 are the latches used to store segment data, while U334-U341 provide the drive capabilities necessary to power the various segments in the display.

### 6.4 ANALOG CIRCUITRY

The following paragraphs discuss the various analog circuits, including the A/D converter, internal bias source, as well as the circuits necessary to control the converter, voltage source, and the capacitance modules.

Figure 6-4 shows a block diagram of the analog circuits, and a detailed schematic may be found on drawing number 590-106 (two sheets) located at the end of Section 8.


Figure 6-4. Analog Circuitry Block Diagram

### 6.4.1 Clock Signals

Y100 generates a stable 8 MHz clock that is used directly by the 6809 MPU (on the digital board) as well as the 1 MHz capacitance module (if present). The 8 MHz signal is further divided down by U133 to 4 MHz to act as a time base for the $A / D$ converter, and to 800 kHz for the 100 kHz capacitance module.

### 6.4.2 Serial Control

A 32-bit control word is shifted into four shift register ICs, U120-U123 via the DATA line. The shift-in process is controlled by the CLOCK signal; after all 32 bits are shifted in (long-shift), the STROBE line is brought low to latch the bits into the outputs of the shift registers.

## Control Bit Configuration

A simplified diagram of the shift register control section is shown Figure 6-5. As indicated, the bits control the following functions:

1. A/D converter control (U120, Q1 through Q7): These bits control various aspects of the A/D converter including final slope (Q1), $\mathbf{X} 1 / \mathrm{X} 10$ gain ( Q 2 ), initialize ( Q 3 ), the A/D sync signal (Q4), and input multiplexer switching (Q5 through Q7).
2. Short/long shift selection (U120, Q8): Basically, there are two shift-in modes. A long-shift sequence utilizes all 32 bits, and would be used when the configuration of the modules or voltage source is to be changed. A short-shift sequence, which places only the first eight bits into U120, would be used where only $A / D$ converter configuration must be changed. This arrangement minimizes MPU overhead and speeds up processing.
3. Module and input/output switching control (U121, Q1 through Q8): These bits control various C module or switching functions: Q1, driving point cable correction (ICCT); $\mathrm{Q} 2,2 \mathrm{nF}$ range control; $\mathrm{Q} 3,200 \mathrm{pF}$ range control; Q4, filter on or off; Q5, 20 pF reference capacitor select; Q6, 200pF reference capacitor select; $\mathrm{Q} 7,1 \mathrm{MHz}$ C module select; and Q8, cal zero enable.
4. Voltage source control (U122 and U123): Q5 fhrough Q8 of U 122 and all eight bits of U123 provide 12 -bit voltage programming data for the voltage source. Q4 of U122 selects voltage source polarity, while Q1 and Q2 of U122 select external or internal bias.


Figure 6-5. Serial Control Bit Format

## Relay Drive and Relays

In many cases, the outputs of the shift registers cannot directly drive the circuits they are to control. In those cases, additional drivers and relays are incorporated. For example, elements of U107 and U114 are necessary to drive relays located in the 5901 or 5902 modules. In a similar manner, sections of U112 and U124 drive relays K100 through K108, which are located on the mother board itself. These relays control various functions, as summarized in Table 6-2.

## Table 6-2. Relay Functions

| Relay | Function | Comments |
| :--- | :--- | :--- |
| K100, K103 | CAL zero | Disconnect input/ <br> output-during <br> calibration <br> Connect 200pF <br> reference capaci- <br> tor to module <br> input <br> K101, K104 <br> Connect 20pF <br> reference capaci- <br> tor to module <br> input |
| 200pF calibration | K102, K105 | 20 pF calibration |
| K108, K107 | Select 1MHz module <br> Select external bias <br> source | Kin |

## Power-on Safeguard

In order to prevent random circuit operation during the power up cycle, the outputs of the shift registers are tristated until they can be loaded with correct control information. U118 and U119 perform the safeguard function for the unit-

U118A and U118B form what is essentially an R-S flip-flop, which is reset upon power-up or power-down by signal derived from a 60 Hz signal from the power transformer. With the flip-flop reset, the output enable (OEN) pins of U120-U123 are held low, tri-stating the outputs. When the first STROBE pulse comes along, however, the flip-flop is set, and the shift register outputs are turned on. The control bits will then be applied to the various circuits to perform their assigned control functions.

### 6.4.3 Status Circuits

In order to keep tabs on the capacitance modules and the voltage source, the MPU must be able to obtain certain information status about these circuits. U125, which is a parallel-to-serial converter, provides this important information to the MPU.

The following status bits are applied to the parallel-to-serial converter:

1. Module present status: P 4 and P 7 indicate the presence of the 100 kHz and 1 MHz modules, respectively. This bit is held low by a jumper in the module when that module is present.
2. Module overload status: P5 and P6 indicate a module overload condition for the 1 MHz and 100 kHz modules respectively.
3. Voltage source current compliance: The voltage source status bit is applied to P8. This signal is generated by sections of U126, and is intended to flag an overcurrent condition in the voltage source.

To read the status, U125 is strobed to latch status information bits into that IC. The status information is then shifted serially out the Q8 line to the MPU using the same clock signal that sequences the control word shift registers.

### 6.4.4 Input Multiplexer

An input multiplexer is used to select among eight different signals that can be applied to the AD converter during the measurement cycle. Key aspects of the multiplexer include the control section and switching FETs, as discussed below.

## Multiplexer Control

Multiplexer control signals are derived by decoding the AD2-AD0 bits from the serial control section. This function is performed by U115, which is a one-of-eight decoder. The TIL logic levels are converted to appropriate signals by sections of U116 and U117 in order to drive the multiplexer FETs.

The signal routed through the multiplexer depends on the the logic levels applied to the A2-A0 lines. Table 6-3 summarizes signals applied for each combination of logic levels.

Table 6-3. Multiplexer Control Signals

| AD2 | AD1 | AD0 | Control | FET On |
| :---: | :---: | :---: | :--- | :---: |
|  |  |  |  |  |
| 0 | 0 | 0 | 100 kHz Conductance | Q105 |
| 0 | 0 | 1 | 100 kHz Capacitance | Q106 |
| 0 | 1 | 0 | 1 MHz Conductance | Q102 |
| 0 | 1 | 1 | 1MHz Capacitance | Q103 |
| 1 | 0 | 0 | Analog common | Q104 |
| 1 | 0 | 1 | V/10 | Q100 |
| 1 | 1 | 0 | V/100 | Q101 |
| 1 | 1 | 1 | 1V Reference | Q107 |

## Multiplexer Operation

A simplified schematic of the input multiplexer is shown in Figure 6-6. Each FET is essentially an analog switch that is controlled by the logic levels discussed above. Signals controlled by the multiplexer FETs include:

1. 100 kHz module signals: Q105 and Q106 control 100 kHz conductance and capacitance, respectively.
2. 1 MHz module signals: Q102 and Q103 switch 1 MHz conductance and capacitance signals.
3. Zero reference: The zero reference signal is controlled by Q104.
4. Bias voltage signals: The $\mathrm{V} / 10$ and $\mathrm{V} / 100$ signals are controlled by Q100 and Q101.
5. Reference voltage: Q107 switches the $1 V$ reference.

## Meausurement Phases

Figure 6-7 shows the measurement phases for a typical measurement cycle. During each phase, the appropriate FET is turned on in order to apply that particular signal to the $\mathrm{A} / \mathrm{D}$ converter. Note that the zero reference (analog common) phase is performed twice, once with X1 gain on the A/D input amplifier, and the second time with X10 gain on that amplifier.


Figure 6-6. Simplified Schematic of Input Multiplexer
diagram of $A / D$ converter circuits is shown in Figure 6-8.

## Time Base Circuits

Various elements-of the converter must be carefully synchronized-- a job performed by the converter time base circuits. U105 and U106 are counter ICs which divide down the 4 MHz signal generated by the clock circuits to 50 kHz , 100 kHz , and 400 kHz clock signals. One additional signal provided by the time base circuits is the SYNC signal, which is used to control integrator discharge.

## Reference Voltages

Two separate reference voltages of -10 and +5 V are used by the A/D converter. The basic voltage reference for both supplies is VR100, a nominal 6.33 V zener diode. The reference voltage is inverted by U112 and buffered by U113A to provide the -10 V reference source.

The nominal 6.33 V zener reference voltage is divided down to 5 V and 1 V by a voltage divider made up of R122, R123, and R124. The 5 V supply is further buffered by U113B and Q110, while the $1 V$ reference is fed to the multiplexer to be read as part of the measurement cycle.

## X1/X10 Gain Amplifier

The X1/X10 gain amplifier (U100A) is an operational amplifier configured with a switchable feedback network. U101C, which is an analog switch, controls the gain switching by either connecting the U100A output to its inverting input (X1 gain) or selecting the feedback network made up of R100 and R106 (X10 gain).

The gain of this amplifier is set to X 10 when the instrument is measuring capacitance or conductance on the $2 \mathrm{pF} / 2 \mu \mathrm{~S}$ range, and during the X 10 reference portion of the measurement phase (see Figure 6-7). At all other times, amplifier gain is $\mathrm{X1}$.

In addition to controlling gain, the amplifier also acts as a buffer between the multiplexer and the A/D converter.

## A/D Converter Operation

The Model 590 uses a combination frequency, variable pulse width analog converter for good resolution and fast conversion times. The discussion below covers integrator discharge, conversion phases, and the integrator itself.


Figure 6-8. Simplified Schematic of A/D Converter

Before integration is begun, the SYNC signal is applied to the gate of Q124, which turns that device on to discharge the integrator capacitor, C115. This step is necessary to minimize integrator offset that could affect measurement accuracy.

The converter has two basic phases of operation, charge balance and final slope. The charge balance phase begins when the input enable/disable line is set high. This action occurs at the end of a software-generated delay period that allows the the signal to settle after the appropriate multiplexer FET is turned on. Once the input is enabled, the signal from the $\mathrm{X} 1 / \mathrm{X} 10$ amplifier is added to the level shift current applied through R108. In this manner, the nominal $\pm 2 \mathrm{~V}$ bipolar signal from the $\mathrm{X} 1 / \mathrm{X10}$ amplifier is converted into a unipolar signal that can be integrated.

The integrator itself is made up U110 and C115. When the input to the integrator is applied, the integrator output ramps up until its voltage is slightly more positive than the reference voltage applied to the inverting input of the duty cycle comparator (U111A). The charge balance current, which is proportional to the input, is fed back to the integrator input through R111 and Q112. Since the charge balance current is much larger than the sum of the input and level shift currents, the integrator output now ramps in the negative direction until the Q output of U108A goes low. During this phase, the MPU counts the total number of pulses that occur.

At the end of the charge balance phase, the integrator output is resting at some positive voltage. Since the integrator output is connected to the non-inverting input of the finalslope comparator (U111B), the final-slope comparator output remains high until the integrator output ramps in the negative direction. During the final-slope phase, Q112 is turned off, and the feedback current is now fed through R113 to the integrator input. The final-slope comparator output is then gated with the 4 MHz clock by U104A, and the number of cycles of the 4 MHz clock that occur are then counted. Once the comparator output goes low, no further clock pulses are counted, and the measurement can then be computed by the MPU.

### 6.4.6 Voltage Source

A simplified schematic diagram of the internal bias voltage source is shown in Figure 6-9. Major sections of the source include the D/A converter, polarity switching, gain and output amplifier, and current compliance detection circuits.

## Digital-to-Analog Converter

12-bit programming information is applied to the digital inputs of U127, as 12-bit DAC (digital-to-analog converter). The nominal output range of the DAC is in the range of 0 to 10 V , with a 0 count input (all 0 s ) resulting in a 10 V output, and a 4095 count input (all 1s) giving a OV output. Actually, the maximum count input is limited to 4000 counts in order to achieve a minimum resolution value of 5 mV . Thus the actual maximum output voltage will be 9.768 V .

Gain and offset for the DAC IC are set with R156 and R157.

## Polarity Switching

Since the DAC output is unipolar, and the voltage source output must be bipolar, some form of polarity switching must be incorporated to allow positive and negative outputs. U128 and associated components perform the polarity switching function for the voltage source.

U128 is an operational amplifier configured for unity gain by feed back elements R149, R150, and R151. U131, an analog switch IC performs polarity switching by routing the DAC output to either the inverting or non-inverting input of U128. The POLARITY control signal is generated by the Q4 output of U122 as part of the serial control information. If the output of the voltage source is to be positive, U128 is operated as an inverting amplifier (since the output stage also inverts the signal). Conversely, U128 is operated as a non-inverting amplifier if the voltage source output is to be negative.

## Output Stage

The output stage provides the necessary gain and drive for the voltage source, and is actually a compound operational amplifier. U130 provides the gain while a complementary output stage made up of transistors Q116-Q119 provide the voltage and current output capabilities. The feedback network made up of R161 and R162 sets the gain of the stage. Since the output stage is essentially a compound operational amplifier, the gain of the stage is:
$\mathrm{A}=-\mathrm{R} 162 / 161$
$A=-20 \mathrm{k} / 9.76 \mathrm{k}$
$A=-2.049$


Figure 6-9. Simplified Schematic of Voltage Source

This seemingly strange gain factor is used to compensate for the fact that only 4000 of the possible 4095 input counts are used with the DAC. Since the maximum DAC output is 9.768 V , the maximum voltage source output is:
$\mathrm{V}=(9.768)(20.49)$
$V=20 \mathrm{~V}$

The resolution of the voltage source is simply $20 / 4000=$ 5 mV .

## Compliance Detection

A compliance bit in the status information tells the MPU if the voltage source has exceeded its current limit. That compliance information is generated by a detection circuit made up of elements of U126.

U126A and U126B are window comparators that monitor the output of U130 for excessive deviations in output voltage-a condition that would flag excessive current. Two comparators are required, one each for positive and negative outputs. Normally, the output of U 130 is approximately the same as the output voltage. However, if an over current condition occurs, Q123 or Q122 will turn on (depending on output polarity), causing the output voltage of U130 to increase in amplitude. The over-voltage condition is then detected by the comparators.

The compliance signal is inverted by U126C and then buffered by U126D before being applied to the status parallel-to-serial converter, U125. C130 provides a time delay of approximately 1 msec to prevent premature compliance detection with capacitive loads.

### 6.5 100kHz CAPACITANCE MODULE

A block diagram of the 100 kHz (5901) capacitance module
is shown in Figure 6-10. Refer to drawing number 5901-106, located at the end of Section 8, for a schematic diagram of the module.

### 6.5.1 Circuit Overview

The key sections of the module, which are shown in the block diagram of Figure 6-10, include:

1. Waveform synthesizer: This section generates the $10 \mu \mathrm{sec}$ reference waveform which ultimately becomes the test signal, as well as the timing waveforms for the synchronous detector.
2. Output amplifier: The output amplifier provides gain, bandwidth limiting via a tuned circuit, and also shapes the test signal into a low-distortion sine wave.
3. AGC: The automatic gain control circuits keep the amplitude of the test signal at a constant level.
4. Output coupling: A transformer couples the test signal to the output and also provides a $23.5: 1$ step-down ratio, which reduces the test signal amplitude to a nominal 15 mV RMS. Also, the DC bias voltage is applied at this point.
5. Trans-impedance amplifier: The primary purpose of this amplifier is to convert the test signal from the device under test from a current to a voltage. Range switching is also included in this amplifier.
6. Tuned amplifier: Provides X 4 gain for the input signal and some bandwidth limiting.
7. Gain amplifiers: These amplifiers provide X36 gain to provide sufficient drive for the detector circuits.
8. Synchronous detector: Multiplies the incoming signal by the quadrature reference signals from the waveform synthesizer.
9. Buffers: The buffers isolate the detector from the $\mathrm{A} / \mathrm{D}$ converter and from devices connected to the analog outputs.


Figure 6-10. Block Diagram of 100kHz Capacitance Module

### 6.5.2 Waveform Synthesizer

The waveform synthesizer is made up of U502, U504, U 505 , and U 507 . The 800 kHz clock signal from the mother board is applied through buffer U502C to the clock input of U504A, which is first in a chain of four D-type flip-flops. These flip-flops make up a four-stage counter with feedback necessary to generate the waveform. The flip-flop outputs are gated by elements of U507 and summed at the junction of R504, R505, and R564 in order to synthesize the waveform.

Additional signals produced by the synthesizer include the A, B, C, and D waveforms for the synchronous detector. These signals are first buffered and inverted by elements of U506 before being applied to the detector.

### 6.5.3 Output Amplifier

The synthesized waveform is applied to the base of Q500, which is a gain-controlled, tuned amplifier. Gain of this stage is controlled by varying the emitter resistance with opto-coupling, as discussed below. The collector circuit of Q500 is tuned to approximately 100 kHz by C502 and T500. This tuned amplifier configuration increases the gain and restricts the bandwidth, such that the output signal is essentially a 100 kHz sine wave.

From the tuned amplifier, the reference signal is coupled through the 10:1 step-down transformer, T500, which also provides a coarse phase adjustment for the 20 pF range. Fine phase adjustment for the 20pF range is performed by R513.

From the transformer, the signal is applied to the noninverting input of operational amplifier, U508, which acts as a buffer. The gain of this amplifier is set to unity by connecting the output directly to the inverting input.

The amplitude of the signal at this point is approximately 1V p-p. The amplified signal is then coupled from the output of U508, through C507 to the primary of transformer T501, which provides a $23.5: 1$ step-down ratio. The signal has now been attenuated down to its final 15 mV RMS value, and it is then applied to the test OUTPUT jack.

The DC bias voltage (external or internal) is also applied at this point in the circuit. The high side of the bias voltage is applied through R570 at the junction of C508, C567 and

R569. The low side is connected directly to the low terminal of the test OUTPUT jack.

### 6.5.4 Automatic Gain Control

In order to assure accurate measurements, the amplitude of the test signal must be kept constant-- a function performed by the automatic gain control circuits. Key components in the AGC circuits include U509, CR500, CR501, U510, Q501, and AT500.

The test signal is coupled from the output of U508 to the DC rectifier made up of U509, CR500, and CR501, which forms a DC error voltage. Filtering for the rectifier is performed by C510.

At this point, the DC signal, which is directly proportional to the 100 kHz test signal amplitude, is applied to the inverting input of U510, which is a combination comparator/integrator. The reference voltage for the comparator is provided by VR500, and the integrator time constant is set by the values of C514 and R517.

The output of the integrator/comparator is used to drive Q501, which controls the current through AT500. The signal is then optically coupled to the resistive element of AT500, which controls the gain of Q500 by controlling the total resistance in the emitter circuit.

To briefly discuss how the AGC circuit controls gain, let us assume that the test signal amplitude begins to rise slightly. This increase in amplitude will be reflected at the output of U508 and coupled to the DC rectifier. Thus, the output of the rectifier will go more positive with the increase in signal amplitude, resulting in a decrease in the output voltage of U510. The reduced output will decrease the current through the emitter circuit of Q501, which also decreases the current through the LED located in AT500. With the decrease in current, the LED light output will decrease, causing an increased Q500 emitter resistance. This increased resistance will decrease the gain of Q500 slightly to compensate for the increased amplitude.

### 6.5.5 Input Amplifiers

Key elements of the input amplifiers include the transimpedance, tuned stage, and X36 amplifiers, as discussed in the following paragraphs.

## Trans-impedance Amplifier

The input signal, which is a phase and magnitude varying current, is applied through the test INPUT jack to the input of the trans-impedance amplifier, Q510 and U511. At the input of this amplifier CR507 and CR508 are used for spike suppression, while C526 provides input coupling. The DC bias component is eliminated by L500, while L500 and C525 resonate at 100 kHz to provide maximum sensitivity.

The purpose of the trans-impedance amplifier, which includes Q510 and U511, is to convert the input signal current into a voltage that can be further amplified and ultimately used by the synchronous detector. Q510 forms a differential amplifier that is used to improve noise performance of the 20 pF range only, and is switched by contacts on K503. The approximate gain of this stage is X6.

Gain control of the input stage is performed by switching various feedback elements in or out of the circuit. K501 controls the 2 nF range, and $K 500$ switches in the necessary elements for the 200 pF range. Various adjustable elements allow control of gain or phase. For example, R521 controls 200 pF range gain, while C529 adjusts 200 pF phase.

Note that the nominal output of the trans-impedance amplifier is approximately 15 mV RMS with a full scale capacitance applied.

## Tuned Stage Amplifier

U512 and associated components form the tune stage amplifier. Tuning is done by the parallel resonant circuit made up of C539 and L501, located in the feedback network of U512. The circuit is tuned to the 100 kHz frequency of interest, and the $Q$ of the circuit is approximately 3, giving the amplifier somewhat broad band characteristics for a tuned amplifier.

The maximum gain of the tuned amplifier is approximately 4.12 , as set by the relative values of R531 and R530.

## X36 Amplifier

One final degree of input signal amplification is performed by two identical amplifier stages, U513 and U514. Each stage has a voltage gain of 6 , as determined by the feedback networks: R532 and R533 set the gain of U513, and R534 and R535 control the gain of U514.

From the output of the amplifier at pin 6 of U514, the signal is coupled through transformed T502 to the synchronous detector.

### 6.5.6 Synchronous Detector

The synchronous detector circuits are designed to extract magnitude and phase information from the input signal and provide voltage outputs that are analogous to the capacitance and conductance being measured. Basically, there are two virtually identical sections to the synchronous detector: Q502, Q503, Q506, Q507, and U515A form the detector for capacitance information, while Q504, Q505, Q508, Q509, and U517A detect the conductance signal.

Basically, each group of FETs acts as an RF mixer with two input signals: the local oscillator, and the measured signal itself. The local oscillator signals are supplied by the waveform synthesizer; the $A$ and $B$ signals control $Q 502$, Q503, Q506, and Q507, and the C and D signals, which are 90 degrees out of phase with A and B, switch Q504, Q505, Q508, and Q509. The output of each detector is buffered by an operational amplifier (U515A, capacitance; U517A, conductance), and filtering is incorporated into the feedback networks in order to limit bandwidth to about 720 Hz . U517A has an adjustable feedback element (R547) that allows the gain of the conductance detector output to be set controlled. R545 and R546 provide offset adjustment for capacitance and gain circuits, respectively.

After filtering and buffering, the full scale output is a nominal 2V. Thus the nominal output with zero scale input will be 0 V .

### 6.5.7 Buffers

In order minimize detector loading, additional buffering is used. U515B and U517B buffer the capacitance and conductance signals respectively, while still more buffering (U516A and U516B) is provided for the two analog outputs. R549 and R550 protect the buffer amplifiers should the analog outputs become shorted. Over voltage protection for the analog outputs is provided by CR509.

Low-pass analog filtering is controlled by K502, which switches filter capacitors C557 and C556. Filter roll-off point is determined by the relative values of C557 and R544 (capacitance), and C556 and R548 (conductance). The nominal -3 dB point is 37 Hz .

### 6.6 1MHz CAPACITANCE MODULE

A block diagram of the 1 MHz (5902) capacitance module is shown in Figure 6-11. Refer to drawing number 5902-106, located at the end of Section 8, for a schematic diagram of the module.

### 6.6.1 Circuit Overview

The key sections of the module, which are shown in the block diagram of Figure 6-11, include:

1. Waveform synthesizer: This section generates the $1 \mu \mathrm{sec}$ reference waveform which ultimately becomes the test signal, as well as the timing waveforms for the synchronous detector.
2. Output amplifier: The output amplifier provides gain, bandwidth limiting via a tuned circuit, and also shapes the test signal into a low-distortion sine wave.
3. AGC: The automatic gain control circuits keep the amplitude of the test signal at a constant level.
4. Output coupling and attenuation: A transformer couples the test signal to the output and also provides a stepdown ratio, which, combined with the attenuator, reduces the test signal amplitude to a nominal 15 mV RMS. Also, the DC bias voltage is applied at this point.
5. Trans-impedance amplifier: The purpose of this amplifier is to convert the test signal from the device under test from a current to a voltage. Some range switching is also included in this amplifier.
6. Differential amplifier: Provides gain for the input signal and some range switching. The differential configuration is used to minimize crosstalk from other circuits.
7. Synchronous detector: Demodulates the phase and amplitude of the input signal.
8. Buffers: The buffers isolate the detector from the $A / D$ converter and from devices connected to the analog outputs.

### 6.6.2 Waveform Synthesizer

The waveform synthesizer is made up of U602, U603, U604, and U605. The 8 MHz clock signal from the mother board is applied through buffers U602C and and U602D to the clock input of U603A, which is first in a chain of four D-type flip-flops. These flip-flops make up a four-stage counter with feedback necessary to generate the waveform.

The flip-flop outputs are gated by elements of U605 and summed at the junction of R606, R608, and R609 in order to synthesize the waveform.

Additional signals produced by the synthesizer include the $\mathrm{A}, \mathrm{B}, \mathrm{C}$, and D waveforms for the synchronous detector. These signals are first buffered and inverted by elements of U601 before being applied to the detector.

### 6.6.3 Output Amplifier

The synthesized waveform is applied to the base of Q601, which is a gain-controlled, tuned amplifier. Gain of this stage is controlled by varying the emitter resistance with opto-coupling, as discussed below. The collector circuit of Q601 is tuned to approximately 1 MHz by L 601 and C 601. This tuned amplifier configuration restricts the bandwidth, such that the output signal is essentially a 1 MHz sine wave.

From the tuned amplifier, the reference signal is applied to the base of Q602, which is used to shift the phase of the signal by 90 degrees. R681 and R619 provide phase adjustment for the 20 pF and 2 nF ranges respectively (other phase adjustments are incorporated into the input stages, as discussed in paragraphs below). These adjustments are selected by contacts on K607, depending on selected range.

From the phase-shift amplifier, the signal is applied to the non-inverting input of operational amplifier, U606. The gain of this amplifier is set to approximately +5 by resistors R622 and R621. The amplitude of the signal at this point is approximately 4.5 V p-p.

The amplified signal is then coupled from the output of U606, through C604 to the primary of transformer T601, which provides a $23.5: 1$ step-down ratio. The signal is further attenuated down to its final 15mV RMS value by a voltage divider made up of R624, R625, and R626. In addition to attenuation, this divider network also results in a very low output impedance.

The DC bias voltage (external or internal) is also applied at this point in the circuit. The high side of the bias voltage is applied through R623 at the junction of C607, C608 and R626. The low side is connected directly to the low terminal of the test OUTPUT jack.


Figure 6-11. Block Diagram of 1 MHz Capacitance Module

### 6.6.4 Automatic Gain Control

In order to assure accurate measurements, the amplitude of the test signal must be kept constant-- a function performed by the automatic gain control circuits. Key components in the AGC circuits include U607, CR602, CR601, U600, Q603, and AT601.

The test signal is coupled from the output of U606 to the inverting input of operational amplifier U607. The purpose of this amplifier is to provide gain, which is slightly less than -2 , with the gain determined by R633, R634, and R629. Note that R634 provides some adjustment in the gain of the circuit.

From U607, the signal is coupled through T602 to CR602, which rectifies the signal to form a DC error voltage. RF bypassing for the rectifier is performed by C619.

At this point, the DC signal, which is directly proportional to the 1 MHz test signal amplitude, is applied to the inverting input of U600, which is a combination comparator/integrator. The reference voltage for the comparator is provided by VR601, and the integrator time constant is set by the values of C611 and R631.

The output of the integrator/comparator is used to drive Q603, which controls the current through AT601. The signal is then optically coupled to the resistive element of AT601, which controls the gain of Q601 by controlling the total resistance in the emitter circuit.

To briefly discuss how the AGC circuit controls gain, let us assume that the test signal amplitude begins to rise slightly. This increase in amplitude will be reflected at the output of U607 and coupled through T602. Thus, the output of CR602 will go more positive with the increase in signal amplitude, resulting in a decrease in the output voltage of U600. The reduced output will decrease the current through the emitter circuit of Q603, which also decreases the current through the LED located in AT601. With the decrease in current, the LED light output will decrease, causing an increased Q601 emitter resistance. This increased resistance will decrease the gain of Q601 slightly to compensate for the increased amplitude.

### 6.6.5 Input Amplifiers

Key elements of the input amplifiers include the transimpedance, differential, and X10 amplifiers, as discussed in the following paragraphs.

## Trans-impedance Amplifier

The input signal, which is a phase and magnitude varying current, is applied through the test INPUT jack to the input of the trans-impedance amplifier, U609. At the input of this amplifier CR605 and CR606 are used for spike suppression, while C667 provides input coupling and blocks any DC bias component.

The purpose of the trans-impedance amplifier is to convert the input signal current into a voltage that can be further amplified and ultimately used by the synchronous detector. Because of the high ( 1 MHz ) frequency involved, a special 600 MHz operational amplifier is used. Because of the wide bandwidth, however, special compensation is required in the feed back circuit for stabilization. Key components here include: R674, R676, R677, R678, C668, R682, C669, and C670. The purpose of these feedback networks is to maintain approximately unity gain at 1 MHz while increasing the gain to X10 at higher frequencies in order to maintain stability. Feedback network switching is done by K602 and depends on the range.

Note that the nominal full scale output of the transimpedance amplifier is approximately 10 mV RMS.

## Differential Amplifiers

Two differential amplifiers, U610 and U611, are used to provide additional voltage gain. Note that only U610 is used for the 2 nF range, while U611 is added to increase gain for the 20 pF and 200 pF ranges. The differential configuration is used to minimize crosstalk and noise pick up from other circuits.

The amplified voltage signal is coupled through T605 to the input of U610, which is operated in the differential configuration. The input of this amplifier is tuned to approximately 1 MHz by C664 and L617. The $Q$ of this circuit is about 3, which is low enough to prevent excessive temperature drift, but high enough to remove interfering signals that may overload succeeding stages. Gain of U610 is set to approximately 15 by U669 and R670, with some adjustment provided by R669.

A second differential amplifier, U611, is used only for the 20 pF and 200 pF ranges. Amplifier gain is set nominally to X10 by R663 and R664, with adjustment provided by R663. The input is tuned by L613 and C661 ( $Q=1$ ), which are used to adjust the phase shift of U611 to zero. Gain switching is provided by K601 and K603, which select either the output of U610 or U611 depending on the range.

## X10 Amplifier

One final stage of input signal amplification is performed by U612, another 600 MHz bandwidth operational amplifier. The gain of this stage is fixed at X10 by the relative values of R659 and R662. The amplifier output is coupled through C642 to the primary to T'603, which coupled the signal to the synchronous detector.

### 6.6.6 Synchronous Detector

The synchronous detector circuits are designed to extract phase and amplitude information from the input signal and provide voltage outputs that are analogous to the capacitance and conductance being measured. Basically, there are two virtually identical sections to the synchronous detector: Q604 through Q607 and U614 form the detector for capacitance information, while Q608-Q611 and U615 detect the conductance signal.

Basically, each group of FETs acts as an RF mixer with two input signals: the local oscillator, and the measured signal itself. The output of each RF mixer is a function of both the phase and magnitude of the measured signal. The local oscillator signals are supplied by the waveform synthesizer; the A and B signals control Q604-Q607, and the C and D signals, which are 90 degrees out of phase with $A$ and $B$, switch Q608-Q611. The output of each detector is buffered by an operational amplifier (U614, capacitance; U615, conductance), and filtering is incorporated into the feedback networks in order to limit bandwidth to less than 1 kHz . U615 has an adjustable feedback element (R651) that allows the gain of the conductance detector output to be set controlled. R646 and R648 provide offset adjustment for capacitance and gain circuits, respectively.

The detector outputs for full scale inputs are pulsating $D C$. After filtering and buffering, the full scale output is a nominal 2V. Conversely, the detector waveform for zero scale inputs will be symmetrical, with an average value of zero. Thus the nominal output with zero scale input will be 0 V .

### 6.6.7 Buffers

In order minimize detector loading, additional buffering is used. U617A and U617B buffer the capacitance and conductance signals respectively, while still more buffering (U616A and U616B) is provided for the two analog outputs. R642 and R643 protect the buffer amplifiers should the analog outputs become shorted. Over voltage protection for the analog outputs is provided by CR603.

Low-pass analog filtering is controlled by K606, which switches filter capacitors C631 and C696. Filter roll-off point is determined by the relative values of C631 and R644 (capacitance), and C696 and R650 (conductance). The nominal -3 dB point is 37 Hz .

### 6.7 POWER SUPPLIES

A block diagram of the power supplies is shown in Figure $6-12$, and the power supply schematic may be found on drawing number 590-126, sheet 1 , located at the end of Section 8 .

### 6.7.1 AC Line Input

AC power is applied to the line filter (01010), through fuse F300 and the power switch S300 to the primary of the power transformer, T300. Note that both sides of the line input are switched by S300.

Power line voltage is selected by line voltage selection switch (S302) which places the transformer windings in parallel or series depending on whether the instrument is to be set up for nominal 115 V or 230 V operation.

From the primary, power is magnetically coupled to various secondary windings used by the analog and digital supplies discussed below. Secondary windings for the analog supplies are shielded to minimize noise coupling that could affect sensitive analog circuits.


Figure 6-12. Block Diagram of Power Supply

### 6.7.2 Analog Supplies

Supply voltages for the analog circuits include $\pm 5, \pm 15$, and $\pm 30 \mathrm{~V}$ regulated supplies, as well as 23 V unregulated and pulsed DC (VAC) circuits.

## $\pm 5 \mathrm{~V}$ Supplies

CR306 provides the rectification for the $\pm 5 \mathrm{~V}$ supplies, while C346 and C345 provide input filtering. VR300 and VR301 are IC regulators, while output filtering is provided by C347 and C348.

## $\pm 15 \mathrm{~V}$ Supplies

These supplies are essentially the same as the $\pm 5 \mathrm{~V}$ supplies, except, of course, for the fact that their output voltages are $\pm 15 \mathrm{~V}$. CR307 rectifies the AC input voltage, while C343 and C344 provide input filtering. VR302 and VR303 are the IC regulators, and C349 and C350 filter the outputs.

Diode CR309 is included in the circuit in order to isolate the VAC signal from the input filter of the +15 V supply. This signal is actually a pulsed DC waveform used by the safeguard circuit in the serial control section. See paragraph 6.4.2.

One final voltage supplied by these components is the 23 V DC supply. Since this voltage is taken directly from the input filter, this supply voltage is unregulated.

## $\pm 30 \mathrm{~V}$ Supplies

Rectification for the $\pm 30 \mathrm{~V}$ supplies is done by CR308, and C341 and C342 provide input filtering. Unlike the remaining supplies, an IC regulator is not used due to the higher voltage involved. Instead, each regulator is made up of a resistor, zener diode, and transistor. Each side of the supply operates essentially the same (except, of course, for polarity). For example, CR305 provides the reference voltage for the positive supply, while R393 limits zener current to a safe value. Q300 is the series pass transistor which regulates the output voltage.

### 6.7.3 Digital Supplies

In order to maintain complete electrical isolation between digital and analog sections, a separate digital supply is used. CR305 rectifies the AC voltage from a separate secondary winding of the power transformer, and C340 provides input filtering. Regulation is performed by VR304, and C351 filters the output.

A separate +12 V unregulated source used by the power up reset circuit (U302) in the digital section is tapped off at the input of the voltage regulator. See paragraph 6.3.1.

### 6.8 DISPLAY AND KEYBOARD CIRCUITS

A block diagram of the display and keyboard circuits is shown in Figure 6-13, and drawing number 590-116 shows a schematic diagram of most of these circuits. Segment latches may be found on drawing number 590-126, sheet 2, while segment drivers are located on drawing number $590-126$, sheet 3.

### 6.8.1 Display

DS201-DS210 are the 14 -segment display LEDs, while DS211 through DS224 are the LED annunciators. U319, U324, U327, and U329 are the segment latches, while U334-U341 are the segment drivers. R362 through R385 limit segment current to the correct value.

Digit drivers for the displays and LEDs include elements of U201-U203. These drivers are controlled by data from U206 and U207.

Turning on a particular display segment is a two-step process. First, the display segment latches are loaded with the information necessary to turn on the desired segments. These segments are paired into two groups, with the a0-a6 and $\mathrm{b0} 0 \mathrm{b6}$ information controlling segments in DS201-DS205, and c0-c6 and d0-d6 concerned with DS206-DS210.


Figure 6-13. Block Diagram of Display and Keyboard

Once the segment latches have been loaded, the appropriate display digit pair is selected with data shifted into U206 and U207 via the DATA line. The shift-in process is controlled a 1 kHz signal applied to the CLOCK line. The selection process begins with the A select line, which selects one-half of both DS201 and DS206. The process sequences through all digits, until all have been selected and is then repeated. As with the A select line, each signal (BJ) controls a pair of digits.

Each digit will be on for approximately $950 \mu \mathrm{sec}$ when selected. Since there are 10 selection steps (for the 20 digits), the display refresh rate is approximately $100 / \mathrm{sec}$ in order to minimize display flicker.

The selection process is similar for the discrete annunciator LEDs. For example, the b7 segment select and G digit select lines are used to control DS211.

### 6.8.2 Keyboard

The keyboard switches, S201-233, are organized into a four column by eight row matrix (except for column 1, which has nine rows). The switches are read by sequencing through the various rows with select signals shifted into U206 and U207 via the DATA and CLOCK lines. These select signals are first buffered by sections of U204 and U205 before being applied to the switch matrix.

Once a particular row is selected, the column lines (S1-S4) are then read through the VIA on the digital board to determine which, if any, keys in that row are pressed. The process repeats for all rows, with a column read operation performed after each row is selected.

### 6.9 CABLE CORRECTION PRINCIPLES

The following paragraphs discuss cable correction principles as implemented in the Model 590 . First an error model for internal and external correction is presented, followed by a discussion of correction algorithms.

### 6.9.1 Error Models

The error model for cable correction paths is shown in Figure 6-14. Figure $6-15$ shows the error model for the internal electronics of the instrument.

The model for internal error correction includes the input/output and transmission section, but excludes the external and device under test sections. Internal corrections are necessary to compensate for the three feet of internal cable between the 5902 module and the front panel test jacks.


Figure 6-14. Transmission Path Error Model


Figure 6-15. Electronics Error Model

### 6.9.2 Internal Model Corrections

The A/D gain and offset errors are combined with the capacitance and conductance gain and offset errors. The phase error, $\Theta \mathrm{F}$ and the sense amplifier gain error, $\mathrm{A}_{s,}$ are combined by treating the $C$ and $G$ readings as complex numbers. The correction factor for these terms is the result of one complex multiplication to perform both phase and gain correction in a single operation.

Keeping these points in mind, the steps necessary for internal error correction are as follows:

1. Subtract the C and G channel offset errors from the C and $G$ channel readings.
2. Multiply the $C$ and $G$ readings by the scaling factors required to put them into the correct units (farads and siemens).
3. Treat the $C$ and $G$ readings as a complex number, then multiply that number by the inverse value of the complex number representing gain and phase errors.

The process defined in step 3 is later combined into the I/O and transmission correction algorithm to avoid two successive complex products where one will perform both corrections.

### 6.9.3 I/O and Transmission Model Corrections

In order to correct the readings for the tranmission path to the front panel, the error terms $\mathrm{Z}_{n 2}, \mathrm{Y}_{n}, \mathrm{Z}_{n 2}, \mathrm{Y}_{22}, \mathrm{M}_{1}$, and $\mathrm{M}_{2}$ must be taken into account. These factors are included by considering the measurement signal path as a series of two-port networks.

Each two port network accounts for one of the error terms ( $\mathrm{Z}_{\mathrm{x} 1}-\left[\mathrm{T}_{\bar{z} 1}^{-}\right]$, etc.).

The total transmission matrix is then the product of the individual transmission matrices.
$\left[\mathrm{T}_{E X}\right]=$ Total transmission matrix

$$
=\left[\mathrm{T}_{Z 1}\right] \times\left[\mathrm{T}_{\mathrm{Y} 1}\right] \times\left[\mathrm{T}_{M 11}\right] \times\left[\mathrm{T}_{D U T}\right] \times\left[\mathrm{T}_{M z}\right] \times\left[\mathrm{T}_{Y 2}\right] \times\left[\mathrm{T}_{Z 2}\right]
$$

$$
=\left[\begin{array}{ll}
\mathrm{A}_{E X} & \mathrm{~B}_{E X} \\
\mathrm{C}_{E X} & \mathrm{D}_{E X}
\end{array}\right]
$$

Where $A_{E X}, B_{E X}, C_{E X}$, and $D_{E X}$ are the respective elements of the resulting transmission matrix.

Since,
$\mathrm{T}_{D U X}=\left[\begin{array}{cc}1 & \mathrm{Z}_{E} \\ 0 & 1\end{array}\right]$
Where $Z_{E}$ is equivalent (complex) impedance of the device under test.

Evaluation [ $\mathrm{T}_{\mathrm{Ex}}$ ] will result in matrix elements each of which will be a linear function of $Z_{E}$.

That is;
$\left[\mathrm{T}_{E X}\right]=\left[\begin{array}{cc}\mathrm{A}_{1} \times \mathrm{Z}_{E}+\mathrm{B}_{1} & \mathrm{~A}_{2} \times \mathrm{Z}_{E}+\mathrm{B}_{2} \\ \mathrm{~A}_{3} \times \mathrm{Z}_{E}+\mathrm{B}_{3} & \mathrm{~A}_{4} \times \mathrm{Z}_{E}+\mathrm{B}_{4}\end{array}\right]$
with $\mathrm{A}_{N}$ and $\mathrm{B}_{N}$ all complex numbers.

The Model 590 in making a measurement of [ $\mathrm{T}_{\text {Ex }}$ ], forces an input voltage and measures a short-circuit output current. In effect, the transfer short-circuit admittance of $\left[\mathrm{T}_{E X}\right]$ is being measured.

Converting a transmission matrix to an admittance matrix is as follows:
if
$[T]=\left[\begin{array}{ll}A & B \\ C & D\end{array}\right]$
$[Y]=\left[\begin{array}{ll}\frac{D}{B} & \frac{-1}{B} \\ \frac{-1}{B} & \frac{A}{B}\end{array}\right]$
where $-1 / B$ is the transfer short-circuit-admittance.
$=-Y_{X F E R}$

Then;
$Y_{\text {xFER }}=1 /\left(A_{2} Z_{E}+B_{2}\right)$

Replacing $A_{2}$ and $B_{2}$ with $K_{1}$ and $K_{2}$ respectively and solving for $\mathbf{1}_{z E ;}$
$1 /_{Z E}=Y_{D U T}=\mathrm{K} 1 /\left(1 / Y_{X F E R}-\mathrm{K} 2\right)$
or
$Z_{E}=1 / Y_{D U T}=\left(Z_{X F E R}-K 2\right) / K 1$

The complex constants K 1 and K 2 are determined through calibration of the Model 590 against known sources.

### 6.9.4 Cable Correction Algorithm

The correction algorithm used to correct the data for cable and other external effects is fundamentally the same for all three forms of correction: Driving Point Admittance, Calibration Source, and S-Parameter Methods. The fundamental difference in the correction modes is in the method used to calculate the coefficients for the correction algorithm.

### 6.9.5 Driving Point Correction

The following discussion shows how the correction terms are derived for the driving point mode. The driving point correction mode is the easiest to implement, but of the three methods, is the one that must make the most assumptions about the transmission paths.

## Basic Assumptions

When using the driving point mode, the following assumptions apply:

1. The correction coefficients are based on measurements made on only the cable connected to the test INPUT jack. The two cables are assumed to be identical.
2. The cables are assumed to be lossless.
3. The driving point measurements are taken with the opposite end of the cable open. This measurement assumes that shunt and offset capacitances present during the driving point measurement are the same as in actual use, and that the shunt capacitance at the end of the cable has the same value for each cable.
4. The cables are assumed to be RG-58 A/U with an impedance of $50 \Omega$ and a propagation velocity of $66 \%$ of the speed of light.
5. Only cables can be accommodated; no switch matrices or other unusual configurations can be used.

In making the driving point corrections two additional matrices are inserted into the previous model to account for the input and output cables. By measuring the shunt capacitance of the open ended input cable the length of that cable can be determined. Using the cable length, transmission matrices are constructed and used to modify the total transmission matrix described in 6.9.3

### 6.9.5 Calibration Source Correction

Using this method the calibration point for the Model 590 is moved from the front panel to the end of a measurement pathway. The process is equivalent to that described in paragraph 6.9.3.

### 6.9.7 S-Parameter Correction

Here the Model 590 accepts measurement pathway descriptions based on measured S-parameters and characteristic impedance. These are then converted to transmission matrix parameters and used according to the procedure in paragraph 6.9.3

## SECTION 7 MAINTENANCE

### 7.1 INTRODUCTION

This section contains information necessary to maintain, calibrate, and troubleshoot the Model 590 CV Analyzer. Fuse replacement and fan filter cleaning procedures are also included.

## WARNING

The procedures in this section are intended only for qualified electronics service personnel. Do not attempt to perform these procedures uniess you are qualified to do so. Some of the procedures may expose you to potentially lethal voltages ( $>\mathbf{3 0 V}$ RMS) that could result in personal injury or death if normal safety precautions are not observed.

This section is outlined as follows:
7.2 Fuse Replacement: Gives the procedures for replacing the line fuse located on the rear panel, and the external bias voltage input fuse located internally.
7.3 Calibration: Details the procedures necessary for calibrating the Model 590 including recommended calibrating equipment and sources.

### 7.4 Special Handling of Static-Sensitive Devices: Covers

 precautions necessary when handling static-sensitive parts within the instrument.7.5 Disassembly/Re-assembly: Covers the procedures for disassembling and re-assembling the instrument--including the case and all circuit boards.
7.6 Troubleshooting: Outlines troubleshooting procedures for the various circuit boards within the Model 590 and the 100 kHz and 1 MHz modules.
7.7 Fan Filter Cleaning/Replacement: Gives the procedure for fan filter removal, cleaning, and replacement, if necessary.

### 7.2 FUSE REPLACEMENT

The paragraphs below give the basic procedures for replacing the line fuse located on the rear panel and the external bias input fuse located internally.

WARNING Disconnect the instrument from the power line and all other equipment before removing the top cover or replacing fuses.

### 7.2.1 Line Fuse Replacement

The line fuse, located on the rear panel (Figure 7-1), protects the power line input of the instrument. Use the following procedure to replace the fuse, if necessary.

1. With the power off, place the end of a flat-bladed screwdriver into the slot in the rear panel fuse holder. Press in gently and rotate the fuse holder approximately one quarter turn counterclockwise. Release pressure on the holder and allow the internal spring to push the carrier and fuse out of the holder.
2. Separate the fuse from the carrier by carefully pulling the two apart.
3. Using an ohmmeter, check the fuse for continuity. A good fuse will show low resistance, while a blown fuse will read high (essentially infinite) resistance.
4. If the old fuse is defective, replace it with the type recommended in Table 7-1.

CAUTION
Do not use a fuse with a higher rating than specified, or instrument damage may occur. If the instrument repeatedly blows fuses, locate and correct the cause of the problem before resuming operation of the unit.
5. Install the new fuse, located in the fuse carrier, by reversing the above procedure.


Figure 7-1. Line Fuse Location

Table 7-1. Line Fuse Values

| Line Voltage <br> Range | Fuse Rating | Keithley <br> Part No. |
| :---: | :--- | :---: |
|  |  |  |
| $90-110 \mathrm{~V}$ | 1 A, slow blow, 250V, 3AG | FU-10 |
| $105-125 \mathrm{~V}$ | $3 / 4 \mathrm{~A}$, slow blow, 250V, 3AG | FU-19 |
| $180-220 \mathrm{~V}$ | $1 / 2 \mathrm{~A}$, slow blow, 250V, 3AG | FU-4 |
| $210 \mathrm{~V}-250 \mathrm{~V}$ | $3 / \mathrm{s}$, , slow blow, 250V, 3AG | FU-18 |
| $105-125 \mathrm{~V}$ | 0.8 A, slow blow, 5 mm | $\mathrm{FU}-11^{*}$ |
| $210-250 \mathrm{~V}$ | 0.4 A , slow blow, 5 mm | $\mathrm{FU}-80^{*}$ |

*Use of 5 mm fuse types requires different fuse carrier; order
part number FH-26.

### 7.2.2 External Bias Input Fuse

An internal $1 / 8$ A fuse protects the instrument from excessive currents applied to the VOLTAGE BIAS INPUT jack on the rear panel. Use the procedure below to test and replace this fuse, if necessary.

CAUTION
The external bias fuse may blow if your external bias source or DC calibrator shorts its output terminals when it is placed in standby. To
avoid blowing fuses in this situation, press the 590 BIAS ON key to turn off the bias voltage (BIAS ON LED off) before placing the external bias source or DC calibrator in standby.

1. Remove the two screws that secure the top cover to the rear panel, and slide the cover off to the rear of the instrument.
2. Refer to Figure 7-2 for the location of the external bias fuse. Using a fuse puller, remove the fuse from the fuse clips.
3. Check the fuse for continuity with an ohmmeter. A good fuse will show low resistance, while a blown fuse will give a very high (infinite) resistance reading.
4. If necessary, replace the fuse with the following type:
$1 / 8$ A, 250V, 8AG, Fast Blow, Keithley Part Number FU-5

## CAUTION

Do not use a fuse with a higher current rating than specified above, or instrument damage may occur.
5. After replacing the fuse, replace the top cover and secure it properly before resuming normal operation.


Figure 7-2. External Bias Fuse Location

### 7.3 CALIBRATION

The following paragraphs discuss various aspects of instrument calibration including recommended calibration equipment and standards, environmental conditions, as well as the basic calibration procedures for instruments equipped with 100 kHz and 1 MHz modules.

## WARNING

Certain steps in the calibration procedures require the use of hazardous voltage. Be careful not to contact these voltages to ensure personal safety.

## NOTE

These calibration procedures are intended for those who are familiar with electronics test equipment and calibration procedures in general. Do not carry out-these procedures unless you are thoroughly qualified to so. Unless the procedures are carefully performed, serious accuracy degradation of the instrument may occur.

### 7.3.1 Factory Calibration

Because of the difficulty in obtaining accurate capacitance and conductance sources and the complexity of the procedures, it is recommended that the instrument be returned to the factory for calibration. Consult your Keithley representative or the factory for details on obtaining factory calibration.

### 7.3.2 Calibration Cycle

Calibration should be performed every 12 months, or if the performance verification procedures discussed in Section 5 show that the instrument is operating outside its stated specifications (detailed Model 590 specifications may be found at the front of this manual). If any of the calibration procedures cannot be properly performed, refer to the troubleshooting information in this section.

### 7.3.3 Environmental Conditions

Calibration should be performed under laboratory conditions having an ambient temperature of $23 \pm 2^{\circ} \mathrm{C}$ and a relative humidity of less than $70 \%$. If the instrument has been subjected to temperatures outside this range, or to higher humidity allow at least one additional hour for the instrument to stabilize before beginning the calibration procedure.

## NOTE

The calibration procedure should be done as quickly as possible to avoid the effects of temperature changes during calibration.

### 7.3.4 Recommended Calibration Equipment and Sources

Table 7-2 summarizes the equipment and sources necessary to perform the various calibration procedures. Other equip-
ment may be substituted as long as accuracy is at least as good as those values given in the table.

## NOTE

Capacitance and conductance sources must be traceable to recognized standards and must have minimal internal shunt capacitance. For that reason, it is recommended that only the sources listed in Table 7-2 be used for calibration.

### 7.3.5 Calibration Switch

An internal switch, located on the mother board (see Figure $7-3$ ), must be set to the enabled position before the instrument will accept calibration commands. Sending calibration commands with the switch in the disabled position will result in the following front panel error message:

## CAL LOCKED

Calibration will not take place under these conditions. The CAL LOCKED bit in the U1 status word will also be set (paragraph 4.9.15), and the Model 590 can be programmed to generate an SRQ under these conditions (paragraph 4.9.16).

Once calibration has been completed, it is recommended that the switch be placed in the disabled position to avoid the possibility of miscalibration during normal operation.

Table 7-2. Recommended Calibration Equipment and Sources

| Description | Specifications | Manufacturer <br> and Model |
| :--- | :---: | :--- |
| $0.5 \mathrm{pF}, 1.5 \mathrm{pF}, 4.7 \mathrm{pF}, 18 \mathrm{pF}$ | $*$ | Keithley Models |
| $47 \mathrm{pF}, 180 \mathrm{pF}, 470 \mathrm{pF}, 1.8 \mathrm{nF}$, |  | 505,5906 |
| $4.7 \mathrm{nF}, 18 \mathrm{nF}$, capacitance |  |  |
| sources | $*$ | Keithley Models |
| $1.8 \mu \mathrm{~S}, 18 \mu \mathrm{~S}, 180 \mu \mathrm{~S}, 1.8 \mathrm{mS}$, |  | 5905,5906 |
| 18 mS conductance |  |  |
| sources |  |  |
| DC calibrator | $20 \mathrm{~V}, 200 \mathrm{~V}$ DC | Fluke 343A |
| DMM (2)** | $\pm 0.002 \%$ | Keithley Model |
|  | $2 \mathrm{~V}, \pm 0.06 \%$ |  |

[^2]

Figure 7-3. Calibration Lock Switch Location

### 7.3.6 Calibration Commands

Table 7-3 summarizes calibration commands for the Model 590 . These commands include:

1. Phase drift calibration (Q0): This command performs the same function as pressing the front panel CAL key. This command is not used as part of this calibration procedure, but is intended merely to optimize accuracy during normal use. Note that this command can be used even if the calibration switch is in the disabled position.
2. Normal mode calibration (Q1, Q2, Q3, and Q4): These four commands perform calibration of the normal $C$ and $G$ measurement ranges.
3. Driving point calibration (Q5, Q6, and Q7): Calibration of the driving point mode of cable correction is performed by these commands.
4. Voltage calibration (Q8 and Q9): Calibration of the voltage read back circuits is performed with these two commands.

Table 7-3. Calibration Command Summary

| Command | Description | Comments |
| :--- | :--- | :--- |
| Q0 | Phase drift calibration | Same as pressing CAL |
| Q1 | Normal mode offset cal |  |
| Q2, C, 0 | Normal mode 1st C cal point | Use actual C value |
| Q3, C, 0 | Normal mode 2nd C cal point | Use actual C value |
| Q4, 0, G | Normal mode G cal point | Use actual C value |
| Q5 | Driving point offset cal |  |
| Q6, C, 0 | Driving point 1st cal point | Use actual C value |
| Q7, C, 0 | Driving point 2nd cal point | Use actual C value |
| Q8, | Voltage offset calibration |  |
| Q9, V | Voltmeter gain calibration |  |

### 7.3.7 Calibration Program

You can use the program below to send the calibration commands to the instrument. As written, the program is in HP-85 BASIC but can be modified for other controllers. Some error checking is included in the program to notify the operator of possible programming errors.

| Program | Comments |
| :---: | :---: |
| 10 EEHOTE 715 | ! Put 590 in remote. |
| 20 LLEAR |  |
| $30 \mathrm{IIMAF[100]}$ | ! Dimension input string. |
| 40 IISP: "COMMANI": | $!$ Prompt for command string. |
| 56 INPUT A ${ }^{\text {a }}$ | ! Input command string. |
| EQUUTPUT $715: A$ | ! Output command string to 590. |
| 70 S=SPOLL (715) | ! Check status. |
| 80 IF EIT (S:5) THEN GOSUE 106 | ! Bit set indicates an error. |
| 90607640 | ! Repeat. |
| 16 CEESTORE | ! Clear data pointer. |
| 116 OUTPUT 715 : $11 \%$ \% | ! Find out which error. |
| 120 ENTER 715 A A | ! Get error status from 590. |
| $130 \mathrm{FIRI}=5 \mathrm{TO} 15$ | ! Parse error word. |
| 140 REHII E* | $!$ Read error messagè. |
| ```150 IF A$[I,I]=:"!"*THEN```  | ! Display error message. |
| 160 NEMT I | ! Loop for next message. |
| 170RETUEK |  |

```
18G IATA " TRIGGER OUER-
    RLHN", "*NEED 1GGK"*
190 DATA""HEED 1N":
    "STRINLGNERFLOW":
20日 DATA "CAL LACKEI":"
    "COHFLICT":
210 IATA "'TRAHSLATOR";
    "HO REMOTE":
ZZQ IATA:"IDDC:"
    "InNCO":
    "IHUALIII"
230 EHD
```


### 7.3.8 Module Calibration

The calibration procedures for the 100 kHz (5901) and 1 MHz (5902) capacitance modules are covered below.

## NOTE

The modules should be calibrated before attempting digital calibration, which is covered in paragraph 7.3.9.

## DMM Connections

In order to calibrate the modules, a DMM is used to measure the voltages at the analog outputs of the instrument. The two DMMs should be connected to the CONDUCTANCE and CAPACITANCE ANALOG OUTPUT jacks; Figure 7-4 shows the connecting method for one of the DMMs. A single DMM can be used by switching connections during the procedure, if desired.

Since the DMM reading will be in volts, it will be necessary to convert the applied standard value to voltage. For example, a nominal 180 pF standard value will yield a nominal 1.8 V DMM reading with the Model 590 on the 200 pF range.


Figure 7-4. Module Calibration Connections

## Source Connections

In all cases, the sources are to be connected directly to the front panel test INPUT and OUTPUT jacks. Cables should not be used, as these will degrade calibration accuracy.

## Calibration Adjustment Locations

The calibration adjustments and jumpers are shown in Figure 7-5. Be sure to carry out the procedures in the order given here.


Figure 7-5. Module Calibration Adjustments

## 100kHz (5901) Module Calibration

Calibrate the 100 kHz module as follows:
1.-Turn on the Model 590 and allow it to warm up for at least one hour before beginning calibration. Also allow the DMMs to warm up for the period stated in their instruction manuals.
2. Select the following operating modes on the Model 590: Frequency: 100 kHz
Filter: ON
Range: 2 nF
3. Select the 2V DC range on both DMMs. Temporarily short the ends of the DMM connecting cables, and then enable zero on both DMMs. Make sure the DMMs are connected to the analog outputs after zeroing them.
4. Change the position of jumper $W 500$ to the ZERO position, as shown in Figure 7-5.
5. Adjust R545 (CAPACITANCE ZERO) for a reading of $0 \mathrm{~V} \pm 100 \mu \mathrm{~V}$ as measured on the DMM connected to the CAPACITANCE OUTPUT.
6. Adjust R546 (CONDUCTANCE ZERO) for a reading of $0 \mathrm{~V} \pm 100 \mu \mathrm{~V}$, as measured on the DMM connected to the CONDUCTANCE OUTPUT.
7. Return jumper W500 to its normal position, as shown in Figure 7-5.
8. Select the 20 pF range on the Model 590 and re-zero the DMMs with nothing connected to the front panel test jacks.
9. Connect the 18 pF nominal capacitance source to the front panel test INPUT and OUTPUT jacks.
10. Adjust R513 (20pF FINE PHASE) for a reading of 0 V $\pm 100 \mu \mathrm{~V}$ as measured on the conductance DMM .
11. Adjust R515 ( 20 pF GAIN) for a voltage reading analogous to the 100 kHz capacitance value marked on the standard, $\pm 1 \mathrm{mV}$. For example, if the marked 100 kHz standard value is 18.05 pF , adjust for a DMM reading of $1.805 \mathrm{~V} \pm 1 \mathrm{mV}$.
12. Disconnect the 18 pF source and make sure the Model 590 is on the $20 \mu \mathrm{~S}$ range.
13. Re-zero the DMMs connected to the analog outputs.
14. Connect the $18 \mu \mathrm{~S}$ conductance source to the front panel test jacks and adjust R547 (CONDUCTANCE GAIN) for a conductance DMM reading analogous to the conductance value marked on the source, $\pm 1 \mathrm{mV}$. For example, if the marked value is $18.1 \mu \mathrm{~S}$, adjust for a voltage reading of $1.81 \mathrm{~V} \pm 1 \mathrm{mV}$.
15. Remove the $18 \mu \mathrm{~S}$ source from the instrument.
16. Select the 200 pF range on the Model 590 and re-zero the DMMs.
17. Connect the 180 pF source to the front panel test $I N-$ PUT and OUTPUT jacks of the Model 590.
18. Adjust R521 (200pF GAIN) for a voltage reading analogous to the marked 100 kHz source value, $\pm 1 \mathrm{mV}$ on the capacitance DMM. For example, if the source value is 180.6 pF , adjust for a DMM reading of $1.806 \pm 1 \mathrm{mV}$.
19. Adjust C529 (200pF PHASE) for a reading of $0 \mathrm{~V} \pm 1 \mathrm{mV}$ on the conductance DMM.
20. Remove the 180 pF source from the instrument.
21. Select the 2 nF range on the Model 590 and re-zero the DMMs.
22. Connect the 1.8 nF source to the front panel test INPUT and OUTPUT jacks.
23. Adjust R523 (2000pF GAIN) for a voltage reading analogous to the marked 1.8 nF source value, $\pm 1 \mathrm{mV}$ on the capacitance DMM. For example, if the marked source value is 1.795 nF , adjust for a voltage reading of $1.795 \mathrm{~V} \pm 1 \mathrm{mV}$.
24. Adjust C527 (2000pF PHASE) for a reading of $0 \mathrm{~V} \pm 1 \mathrm{mV}$ on the conductance DMM.
25 . Remove the 1.8 nF capacitance source from the unit.

This concludes calibration of the 100 kHz module. If the Model 590 has a 1 MHz module installed, calibrate that unit using the procedure below. Otherwise, proceed to paragraph 7.3.9 for digital calibration procedures.

## 1MHz (5902) Module Calibration

Use the following procedure to calibrate the 1 MHz module. Note that the procedure must be repeated several times until no adjustment is required at any point in order for the module to be properly calibrated.

1. Turn on the Model 590 and allow it to warm up for at least one hour before beginning calibration. Also allow the DMMs to warm up for the period stated in their instruction manuals.
2. Select the 2 V DC range on the DMMs. Temporarily short the ends of the DMM test leads, then enable zero on both DMMs. Connect the DMMs to the CAPACITANCE and CONDUCTANCE ANALOG OUTPUTS.
3. Select the following operating modes on the Model 590: Frequency: 1 MHz
Filter: On
Range: 2 nF
Initially, nothing should be connected to the front panel test jacks.
4. Move jumper W601 to the ZERO position (see Figure 7-5).
5. Adjust R646 (CAPACITANCE ZERO) for a reading of $0 \mathrm{~V} \pm 100 \mu \mathrm{~V}$ on the capacitance DMM (the DMM connected to the CAPACITANCE OUTPUT).
6. Adjust R648 (CONDUCTANCE ZERO) for a reading of $0 \mathrm{~V} \pm 100 \mu \mathrm{~V}$ on the conductance DMM (the DMM connected to the CONDUCTANCE OUTPUT).
7. Re-zero both DMMs.
8. Return jumper W601 to the normal position (see Figure 7-5).
9. Verify that the voltage readings on both DMMs are less than $\pm 15 \mathrm{mV}$. If higher offset values are noted, check to see that all module shields are properly secured.
10. Check to see that the Model 590 is on the 2 nF range and re-zero the conductance and capacitance DMMS.
11. Connect the 1.8 nF Model 5905 capacitance source to the test INPUT and OUTPUT jacks of the instrument.
12. Adjust R620 ( 2000 pF PHASE) for a value of $0 \mathrm{~V} \pm 3 \mathrm{mV}$, as indicated on the conductance DMM.
13. Adjust R669 ( 2000 pF GAIN) for a voltage reading analogous to the 1 MHz capacitance value marked on the source, $\pm 2 \mathrm{mV}$. For example, if the 1 MHz value is 1.7996 nF , adjust for a DMM reading of $1.7996 \mathrm{~V} \pm 2 \mathrm{mV}$.
14. Remove the 1.8 nF source from the instrument.
15. Select the 200 pF range on the Model 590 and re-zero both DMMs.
16. Connect the 180 pF capacitance source to the front panel test INPUT and OUTPUT jacks.
17. Adjust L613 ( 200 pF PHASE) for a reading on $0 \mathrm{~V} \pm 1 \mathrm{mV}$ on the conductance DMM.
18. Adjust R663 (200pF GAIN) for a DMM reading analogous to the 1 MHz capacitance value marked on the 180 pF source to within 1 mV . For example, if the marked 1 MHz value is 181.4 pF , adjust R663 for a reading of $1.814 \mathrm{~V} \pm 1 \mathrm{mV}$.
19. Remove the 180 pF source from the instrument.

20 . Place the Model 590 on the 20 pF range and re-zero both the capacitance and conductance DMMs.
21. Connect the 18 pF source to the front panel test INPUT and OUTPUT jacks.
22. Adjust R681 ( 20 pF PHASE) for a reading of $0 \mathrm{~V} \pm 1 \mathrm{mV}$ on the conductance DMM.
23. Adjust R675 (20pF PHASE) for a DMM reading analogous to the 1 MHz value marked on the capacitance source to within 1 mV . For example, if the marked $1 \mathrm{MH} z$ value is 18.13 pF , adjust R675 for a DMM reading of $1.813 \mathrm{~V} \pm 1 \mathrm{mV}$.
24. Remove the 18 pF source from the instrument.
25. Repeat steps 11 through 24 until no further adjustment is required.
26. Select the 2 mS range an re-zero the DMMs.
27. Connect the 1.8 mS source to the front panel test INPUT and OUTPUT jacks.
28. Adjust R651 (CONDUCTANCE GAIN) for a conductance DMM reading analogous to the marked conductance source value to within 14 mV . For example, if the marked value is 1.802 mS , adjust R651 for a DMM reading of $1.802 \mathrm{~V} \pm 14 \mathrm{mV}$.
29. Remove the 1.8 mS source from the instrument.

This concludes 1 MHz module calibration. Proceed to paragraph 7.3.9 for digital calibration procedures.

### 7.3.9 Digital Calibration

## Initial Instrument Setup

Before each calibration procedure, send the command " S 3 T 2 X " to select the $10 / \mathrm{sec}$ reading rate and correct trigger mode.

## Voltage Read-Back Calibration

## WARNING

Hazardous voltages will be used in some of the following steps. Take care not to contact these voltages.

Use the following procedure to calibrate the read-back accuracy of the voltage display. Table 7-4 summarizes the procedure.

1. Connect the DC voltage calibrator to the rear panel VOLTAGE BIAS INPUT jack, as shown in Figure 7-6.
2. Initially set the calibrator to 0.0000 VDC .
3. Turn on the Model 590 and allow it to warm up for one hour. Send the command "S3T2X" to initialize the instrument.
4. Turn on the calibrator and allow it to warm up for the period recommended by the manufacturer.
5. Set the calibrator to operate.
6. Send the command "W4N1X" to select external bias and turn the bias on.
7. Send " $Q 8 X$ " to calibrate voltage offsets on the 200 V read-back range.
8. Set the DC calibrator $t+200.000 \mathrm{VDC}$.
9. Send the command " $\mathrm{Q} 9,200 \mathrm{X}$ " to calibrate full scale.
10. Set the DC calibrator to 0.0000 VDC and send the command string "W0XQ8X" to calibrate voltage offsets on the 20 V read back range.
11. Set the calibrator to +20.0000 V and send the command " $\mathrm{Q} 9,20 \mathrm{X}$ " to calibrate full scale.
12. Set the DC calibrator to 0.0000 V and disconnect it from the Model 590.

Table 7-4. Voltage Read-Back Calibration Summary

| Step | DC Calibrator <br> Voltage | Command | Comments |
| :---: | :---: | :---: | :--- |
|  |  |  |  |
| 1 | - | S3T2X | Initialize unit |
| 2 | 0.000 VDC | W4N1X | Select external bias |
| 3 | 0.000 VDC | Q8X | Calibrate offsets |
| 4 | +200.0000 VDC | Q9,200X | Calibrate full scale |
| 5 | 0.000 VDC | W0XQ8X | Select DC, cal offset |
| 6 | +20.0000 VDC | Q9,20X | Calibrate full scale |



Figure 7-6. Connections for 200V Read-Back Calibration


Figure 7-7. Source Connections

## Internal Bias Voltage Source Calibration

Perform the following procedure to calibrate the internal bias source. Calibration adjustments are shown in Figure 7-8. Table 7-5 summarizes the procedure.

## NOTE

Read-back calibration must be performed before attempting voltage source calibration.

1. With the power off, remove the two screws that secure the top cover and slide the top cover off to the rear of the instrument.
2. Turn on the power and allow the Model 590 to warm up for one hour. Send the command "S3T2X" to initialize the unit.--
3. Send the command "WOX" to select a DC waveform type.
4. Send the command "V0.001N1X" and note the reading on the voltage display. Record this value as reading $A$.
5. Send "V-0.001X" and note and record reading B.
6. Compute the average of the two readings from steps 4 and 5: (A-B)/2.
7. Adjust R152 to display the average computed in step 5.
8. Adjust R157 for a reading of 00.000 V on the voltage display.
9. Send the command "V-19X" and then adjust R156 for a reading of exactly -19.000 V on the voltage display.
10. Send "V19X" and then adjust R150 for a reading of +19.000 V on the voltage display.
11. Turn off the power, mount the module support tray, and replace the top cover. Paragraph 7.5 covers assembly in more detail.

## Table 7-5. Voltage Source Calibration Summary

| Step | Command | Adjustment | Comments |
| :---: | :---: | :---: | :---: |
| 1 | S3T2X |  | Initialize 590 |
| 2 | W0X |  | DC waveform |
| 3 | V0.001N1X |  | Record reading A |
| 4 | V-0.001X |  | Record reading B |
| 5 |  |  | Take average: $(\mathrm{A}-\mathrm{B}) / 2$ |
| 6 |  | R152 | Adjust to display average computed in Step 5 |
| 7 |  | R157 | Adjust for display of 00.000 V |
| 8 | V-19X | R156 | Adjust to display $-19.000 \mathrm{~V}$ |
| 9 | V19X | R150 | Adjust to display $+19.000 \mathrm{~V}$ |



Figure 7-8. Voltage Source Calibration Adjustment Locations

## 100kHz Calibration

Follow the steps below in the order shown to calibrate the unit at 100 kHz . Table $7-6$ summarizes the procedure, commands, and necessary sources.

1. Turn on the power and allow the unit to warm up for one hour. Send the command "S3T2X" to initialize the unit.
2. Send the command string "F0R1X" to select 100 kHz and place the unit on the 2 pF range.
3. With nothing connected to the test INPUT and OUTPUT jacks, send the command "Q1X" to calibrate offsets.
4. Connect the 1.5 pF source to the instrument and send the command " $\mathrm{Q} 2, \mathrm{C}, 0 \mathrm{X}^{\prime}$ ' where C is the actual 100 kHz value marked on the capacitor.
5. Connect the 0.5 pF source and send the command "Q3,C,0X" where $C$ is the actual 100 kHz capacitance value.
6. Connect the $1.8 \mu \mathrm{~S}$ source and send the command " $\mathrm{Q} 4,0, \mathrm{GX}^{\prime}$, using the actual 100 kHz value G .
7. Send the command " $R 2 X^{\prime \prime}$ to place the unit on the 20 pF range.
8. With nothing connected to the test INPUT and OUTPUT jacks, send "Q1X" to calibrate offsets.
9. Connect the 18 pF source to the instrument and send the command "Q2,C,0X' where C represents the actual 100 kHz C value.
10. Connect the 4.7 pF source to the Model 590 and send the command " $\mathrm{Q} 3, \mathrm{C}, 0 \mathrm{X}^{\prime}$ ", using actual C value.
11. Connect the $18 \mu \mathrm{~S}$ source to the instrument and send " $Q 4,0, G X$ " where $G$ is the actual value.
12. Repeat steps 7 through 11 for the 200 pF and 2 nF ranges by using the appropriate sources and the R3 and R4 commands, as summarized in Table 7-6

Table 7-6. 100kHz Calibration Summary

| Step | Source (Nominal Value) | Command | Comments |
| :---: | :---: | :---: | :---: |
| 1 |  | S3T2X | Initialize 590 |
| 2 |  | FOR1X | Select $100 \mathrm{kHz}, 2 \mathrm{pF}$ |
|  |  |  | range |
| 3 | None* | Q1X | Calibrate offsets |
| 4 | 1.5 pF | Q2, C, 0X | Use actual C value |
| 5 | 0.5 pF | Q3, C, 0X | Use actual C value |
| 6 | $1.8 \mu \mathrm{~S}$ | Q4, 0, GX | Use actual $G$ value |
| 7 |  | R2X | Select 20 pF range |
| 8 | None* | Q1X | Calibrate offsets |
| 9 | 18 pF | Q2, C, 0X | Use actual C value |
| 10 | 4.7 pF | Q3, C, 0X | Use actual C value |
| 11 | $18 \mu \mathrm{~S}$ | Q4, 0, GX | Use actual $G$ value |
| 12 |  | R3X | Select 200pF range |
| 13 | None* | Q1X | Calibrate offsets |
| 14 | 180pF | Q2, C, 0X | Use actual C value |
| 15 | 47 pF | Q3, C, 0X | Use actual C value |
| 16 | $180 \mu \mathrm{~S}$ | Q4, 0, GX | Use actual $G$ value |
| 17 |  | R4X | Select 2 nF range |
| 18 | None* | Q1X | Calibrate offsets |
| 19 | 1.8 nF | Q2, C, 0X | Use actual C value |
| 20 | 470 pF | Q3, C, 0X | Use actual C value |
| 21 | 1.8 mS | Q4, 0, GX | Use actual $G$ value |

*Test jacks must be left open when performing these tests.

## 20nF/20mS Range Model 5904 Input Adapter Calibration

Use the procedure below to calibrate the Model 590/5904 for use on the $20 \mathrm{nF} / 20 \mathrm{mS}$ range (see below for complete calibration procedure.

1. Turn on the power and allow the unit to warm up for one hour. Send the command "S3T2X".
2. Connect the Model 5904 to the test INPUT and OUTPUT jacks of the Model 590.
3. Send the command string "F0R8X" to select 100 kHz and place the unit on the 20 nF range.
4. With nothing connected to the Model 5904 jacks, send the command " Q 1 X " to calibrate offsets.
5. Connect the 18 nF source to the Model 5904 and send the command " $\mathrm{Q} 2, \mathrm{C}, 0 \mathrm{X}$ " where C is the actual 100 kHz value marked on the capacitor.
6. Connect the 4.7 nF source and send the command " $\mathrm{Q} 3, \mathrm{C}, 0 \mathrm{X}$ " where C is the actual 100 kHz capacitance value.
7. Connect the 18 mS conductance source to the instrument and send the command " $\mathrm{Q} 4,0, \mathrm{GX}$ ' using the actual 100 kHz value.

## Complete Model 5904 Input Adapter Calibration

Use the following procedure to calibrate the unit for use with the Model 5904 Input Transformer on the 20 pF through 20 nF ranges. Table 7-7 summarizes the Model 5904 calibration procedure.

## NOTE

The procedure below assumes that the Model 5904 is to be calibrated for the $20 \mathrm{pF}-20 \mathrm{nF}$ ranges. Since calibration constants for the attenuated $20 \mathrm{pF}-2 \mathrm{nF}$ ranges are shared with unattenuated $20 \mathrm{pF}-2 \mathrm{nF}$ ranges, complete calibration using the procedure below will miscalibrate the unit for unattenuated use on the 20 pF through 2 nF ranges. Use the 20 nF only calibration procedure above for cases where the instrument is to be used without the Model 5904 adapter on the $20 \mathrm{pF}-2 \mathrm{nF}$ ranges.

1. Turn on the power and allow the unit to warm up for one howr. Send the command "S3T2X".
2. Connect the Model 5904 to the test INPUT and OUTPUT jacks of the Model 590.
3. Send the command string "FOR5X" to select 100 kHz and place the unit on the 20 pF range.
4. With nothing connected to the Model 5904 jacks, send the command " Q 1 X " to calibrate offsets.
5. Connect the 18 pF source to the Model 5904 and send the command " $\mathrm{Q} 2, \mathrm{C}, 0 \mathrm{O}$ " where C is the actual 100 kHz value marked on the capacitor.
6. Connect the 4.7 pF source and send the command " $\mathrm{Q} 3, \mathrm{C}, 0 \mathrm{X}$ " where C is the actual 100 kHz capacitance value.
7. Connect the $18 \mu \mathrm{~S}$ source and send the command ' $\mathrm{Q} 4,0, \mathrm{GX}$ ', using the actual 100 kHz value for G .
8. Send the command "R6X" to place the unit on the 200 pF range.
9. With nothing connected to the Model 5904 jacks, send "Q1X" to calibrate offsets.
10. Connect the 180 pF source capacitor to the Model 5904 jacks and send the command " $\mathrm{Q} 2, \mathrm{C}, 0 \mathrm{X}$ " where C represents the actual C value.
11. Connect the 47 pF source to the Model 5904 and send the command " $\mathrm{Q} 3, \mathrm{C}, 0 \mathrm{X}$ ", using the actual C value.
12. Connect the $180 \mu \mathrm{~S}$ source to the Model 5904 and send " $\mathrm{Q} 4,0, \mathrm{GX}$ " where G is the actual value at 100 kHz .
13. Repeat steps 8 through 12 for the 2 nF and 20 nF ranges by using the appropriate sources and the R7 and R8 commands, as summarized in Table 7-7.

Table 7-7. Model 5904 Calibration Summary

| Step | Source <br> (Nominal Value) | Command | Comments |
| :---: | :---: | :---: | :---: |
| 1 |  | S3T2X | Initialize 590 |
| , |  | F0R5X | Select $100 \mathrm{kHz}, 20 \mathrm{pF}$ range |
| 3 | None | Q1X | Calibrate offsets |
| 4 | 18pF | Q2, C, 0X | Use actual C value |
| 5 | 4.7 pF | Q3, C, 0X | Use actual $C$ value |
| 6 | $18 \mu \mathrm{~S}$ | Q4, 0, GX | Use actual G value |
| 7 |  | R6X | Select 200pF range |
| 8 | None | Q1X | Calibrate offsets |
|  | 180pF | Q2, C, 0X | Use actual C value |
| 10 | 47 pF | Q3, C, 0X | Use actual C value |
| 11 | $180 \mu \mathrm{~S}$ | Q4, 0, GX | Use actual G value |
| 12 |  | R7X | Select 2 nF range |
| 13 | None | Q1X | Calibrate offsets |
| 14 | 1.8pF | Q2, C, 0X | Use actual C value |
| 15 | 470 pF | Q3, C, 0X | Use actual C value |
| 16 | 1.8mS | Q4, 0, GX | Use actual value |
| 17 |  | R8X | Select 20nF range |
| 18 | None | Q1X | Calibrate offsets |
| 19 | 18nF | Q2, C, OX | Use actual C value |
| 20 | 4.7 nF | Q3, C, 0X | Use actual C value |
| 21 | 18mS | Q4, 0, GX | Use actual $G$ value |

NOTE: Using this procedure will miscalibrate the unit for unattenuated use on $20 \mathrm{pF} / 20 \mu \mathrm{~S}$ through $2 \mathrm{nF} / 2 \mathrm{mS}$ range.

## 1MHz Calibration

Follow the steps below in the order shown to calibrate the unit at 1 MHz . Table $7-8$ summarizes the procedure, commands, and necessary sources

1. Turn on the power and allow the unit to warm up for one hour. Send the command "S3T2X" to initialize the unit.
2. Send the command string "F1R2X" to select 1 MHz and place the unit on the 20 pF range.
3. With nothing connected to the test INPUT and OUTPUT jacks, send the command "Q1X" to calibrate offsets.
4. Connect the 18 pF source to the instrument and send the command " $\mathrm{Q} 2, \mathrm{C}, 0 \mathrm{X}$ " where C represents the actual C value at 1 MHz .
5. Connect the 4.7 pF source to the Model 590 and send the command " $\mathrm{Q} 3, \mathrm{C}, 0 \mathrm{X}$ ", using the actual C value at 1 MHz .
6. Connect the $180 \mu \mathrm{~S}$ source to the instrument and send " $\mathrm{Q} 4,0, \mathrm{GX}$ " where G is the actual value at 1 MHz .
7. Repeat steps 7 through 11 for the 200 pF and 2 nF ranges by using the appropriate sources and the R3 and R4 commands, as summarized in Table 7-8.

Table 7-8. 1MHz Calibration Summary

| Step | Source Nominal Value) | Command | Comments |
| :---: | :---: | :---: | :---: |
| 1 |  | S3T2X | Initialize 590 |
| 2 |  | F1R2X | Select 1 MHz , 20pF range |
| 3 | None | Q1X | Catibrate offsets |
| 4 | 18pF | Q2, C, 0X | Use actual C value |
| 5 | 4.7 pF | Q3, C, 0X | Use actual C value |
| 6 | $180 \mu \mathrm{~S}$ | Q4, 0, GX | Use actual $G$ value |
| 7 |  | R3X | Select 200 pF range |
| 8 | None | Q1X | Calibrate offsets |
| 9 | 180pF | Q2, C, OX | Use actual C value |
| 10 | 47 pF | Q3, C, 0X | Use actual C value |
| 11 | 1.8 mS | Q4, 0, GX | Use actual $G$ value |
| 12 |  | R4X | Select 2 nF range |
| 13 | None | Q1X | Calibrate offsets |
| 14 | 1.8 nF | Q2, C, OX | Use actual C value |
| 15 | 470pF | Q3, C, 0X | Use actual C value |
| 16 | 18mS | Q4, 0, GX | Use actual G value |

## Cable Correction Calibration

Use the procedure below to calibrate the driving point cable correction mode of the Model 590 .

## NOTE

If your Model 590 is equipped only with a 100 kHz CV module, perform this procedure at 100 kHz instead of 1 MHz as indicated.

Perform the steps below in the indicated order. Table 7-9 summarizes_the procedure, commands, and required sources.

1. Turn on the power and allow the Model 590 to warm up for at least one hour.
2. Send the command string "F1R4S3T2Z0X" to select 1 MHz and place the unit on the 2 nF range.
3. With nothing connected to the test INPUT and OUTPUT jacks, send the command "Q5X" to calibrateoffsets.
4. Connect the 470 pF capacitor to the test INPUT jack only using the right angle adapter supplied with the Model 5905. Short the source jack normally connected to the test OUTPUT using the supplied shorting plug.
5. Send the command " $\mathrm{Q} 6, \mathrm{C}, 0 \mathrm{X}$ ", using the actual 1 MHz $C$ value marked on the source.
6. Connect the 180 pF source to the instrument (see step 4 for connections) and send the command "Q7,C, $0 X$ " where C represents the actual 1 MHz C value.

Table 7-9. Driving Point Calibration Summary

| Step | Source <br> (Nominal Value) | Command | Comments |
| :---: | :---: | :---: | :---: |
| 1 |  | S3T2Z0X | Initialize 590 |
| 2 |  | F1R4X | 1 MHz , 2 nF range* |
| 3 | None | Q5X | Calibrate offsets |
| 4 | 470 pF | Q6, C, 0x | Use actual C value |
| 5 | 180 pF | Q7, C, 0x | Use actual C value |

*Use FOR4X for 100 kFIz .

### 7.4 SPECIAL HANDLING OF STATICSENSITIVE DEVICES

CMOS devices are designed to operate at high impedance levels for lower power consumption. As a result, any static charge that builds up on your person or clothing may be sufficient to destroy these devices if they are not handled properly. In general, it should be assumed that all devices are static sensitive.

Use the precautions below when handling static-sensitive devices.

1. Transport such devices only in containers designed to prevent static build-up. Typically, these parts will be received in anti-static containers of plastic or foam. Always leave the devices in question in their orignal containers until ready for installation.
2. Remove the devices from their protective containers only at a properly-grounded work station. Also ground yourself with a suitable wrist strap.
3. Handle the devices only by the body; do not touch the pins or terminals.
4. Any printed circuit board into which the device is to be inserted must also be properly grounded to the bench or table.
5. Use only anti-static type de-soldering tools.
6. Use only soldering irons with properly-grounded tips.
7. Once the device is installed on the PC board, it is usually adequately protected, and normal handling can resume.

### 7.5 DISASSEMBLY

The following paragraphs contain disassembly procedures
for the Model 590 and modules. In general, disassembly should be carried out in the order presented here unless otherwise noted. The various sections can be re-assembled by reversing the corresponding disassembly procedure.

## WARNING

Disconnect the line cord and all other equipment from the instrument before beginning the disassembly procedure.

### 7.5.1 Top and Bottom Cover Removal

Refer to Figure 7-9 and remove the top or bottom cover using the corresponding procedure below.

## Top Cover Removal

1. Remove the two screws that secure the top cover to the rear-panel.
2. Carefully slide the top cover to the rear of the instrument until it is completely clear of the case sides then remove it.

## Bottom Cover Removal

1. Place the Model 590 upside down on a soft cloth to avoid scratching the case.
2. Remove the two screws that secure the cover to the rear panel.
3. Remove the four feet located on the bottom cover.
4. Slide the bottom cover to the rear of the instrument until it is free of the case and remove it completely.


Figure 7-9. Top and Bottom Cover Removal

### 7.5.2 Module and Circuit Board Removal and Replacement

Removal and replacement of the modules and circuit boards is covered below. These items should be removed in the order shown and replaced in reverse order. General module and circuit board configuration is shown in Figure 7-10, while cable connections are shown in Figure 7-11.

## Removal

1. Remove the rear panel in the following manner:
A. Remove the two screws that secure the IEEE- 488 connector to the rear panel.
B. Remove the four screws that secure the rear panel to the case sides (two screws on each side).
C. Pull the rear panel an inch or so away from the instrument to allow access to the various connectors. Be careful not to excessively strain the wires.
D. Disconnect the four coaxial connectors going to the rear panel at the $A / D$ board end.
E. Disconnect the line and fan wiring connectors from the digital board.
F. Disconnect the grounding strap.
G. Remove the rear panel completely.
2. Remove the module support tray and modules as follows:
A. Disconnect all cables going to the $5901(100 \mathrm{kHz})$ or 5902 ( 1 MHz ) modules.
B. To remove a module from the support tray, take out the screws that secure the module to the tray, then remove the module.
C. Remove the screws that attach the support tray to the top case rails and then remove the tray with modules still attached from the unit.
3. The mother board can be removed as follows:
$A$. If the rear panel has been removed, go on to step $B$. Otherwise use a small screwdriver to pry out the upper trim strip from each case side, then remove the screws that attach the upper support rails. Remove the support rails from the unit.
B. Disconnect the two cables connected to the digital board.
C. Disconnect the two coaxial cables going to the front panel test jacks.
D. Turn the instrument upside down, and remove the six screws that secure the mother board to the bottom support rails.
E. Place the unit right side up, and remove the $A / D$ board.
4. Remove the digital board using the procedure below:
A. Disconnect the display board ribbon cable at the front of the board.
B. Turn the instrument upside down, and remove the six screws that attach the board to the bottom support rails.
C. Turn the instrument right side up, slide the board to the rear to clear the power switch, and remove the board.

## Circuit Board and Module Installation

In general, the boards and modules can be installed by reversing the above procedure. However, the following points should be noted when installing these items:

1. Make sure that all screws are properly installed.
2. Make sure the all connectors are properly replaced, using Figure 7-11 as a guide. In particular check to see that module connections are not interchanged $(5901,100 \mathrm{kHz}$ and $5902,1 \mathrm{MHz}$ connections are marked on the mother board.
3. Pay particular attention to the installation of ribbon cables, as it is possible to improperly position these cables so that the connector is one or more pins off.
4. Make sure that the rear panel is properly attached to the case, and that the IEEE-488 connector screws are securely tightened.

### 7.5.3 Case Disassembly

At this point in the disassembly process, the top support rails and rear panel should have already been removed. Use the procedure below to complete case disassembly, using Figure 7-12 as a guide.

1. Using a small screwdriver, pry the bottom trim strips from the case sides.
2. Remove the four screws that secure the front panel to the case sides and then remove the front panel.
3. Remove the two screws that attach each of the three bottom rails to the case sides and remove the three rails.
4. If desired, remove the two screws that attach each handle to the case sides. Compress the handle and guide it through the slots to remove it.
5. When re-assembling the case, make sure that the top and bottom rails are installed in the correct positions, or it will not be possible to properly secure the module support tray and circuit boards that attach to the rails.


Figure 7-10. Circuit Board Removal and Replacement


Figure 7-11. Cable Connections


Figure 7-12. Case Disassembly

### 7.5.4 Rear Panel Disassembly

Refer to Figure 7-13 and remove parts from the rear panel as follows:

1. Remove the four screws that secure the fan and fan guard and remove them.
2. Remove the nut that holds the green ground wire to the rear panel and disconnect the wire.
3. Remove the two nuts that secure the line receptacle/filter and remove it.
4. To remove the four BNC jacks, remove the screws that secure the bracket to the rear panel, and remove the bracket.
5. When installing these parts, make certain all screws and nuts are tight, and that the ground wires and capacitor solder lugs are properly secured.

## WARNING

The ground wires must be properly installed to ensure continued protection against possible shock hazards.

### 7.5.5 Front Panel Disassembly

An exploded view of the front panel assemble is shown in Figure 7-14. Use the following procedure to disassemble the front panel.

1. Remove the screws that attach the test jack bracket to the front panel and remove the bracket.
2. Using an allen wrench, loosen the two allen screws that secure each front panel rail, and remove each rail.
3. Remove the remaining screw that secures the display board to the front panel, and remove the board.
4. Re-assemble the front panel as follows:
A. Insert the display board between the top and bottom rails, but do not tighten the screws at this time.
B. Attach the rail and board assembly to the case sides with four screws (two on each side).
C. Align the buttons in the holes, making sure that no buttons are sticking. Now tighten the rail set screws to secure the display board.
D. Tighten the screw holding the display board to the front panel.

### 7.6 TROUBLESHOOTING

The troubleshooting information contained in this section is intended for qualified personnel who have a basic understanding of analog and digital circuitry. The individual should also be experienced at using typical test equipment, as well as ordinary troubleshooting procedures.

This information has been written to assist in isolating a defective circuit or circuit section. Isolation of a specific component is left to the technician.

Schematic diagrams, component layout drawings, and parts lists for the various circuit boards within the instrument are located at the end of Section 8.

### 7.6.1 Recommended Test Equipment

Success in troubleshooting complex electronic equipment such as the Model 590 relies both on the skill of the technician and the use of accurate, reliable test equipment. Table 7-10 lists recommended equipment for troubleshooting the Model 590.

## Table 7-10. Recommended Troubleshooting Equipment

| Description | Manufacturer <br> and Model | Use |
| :--- | :--- | :--- |
| 51/2 Digit DMM | Keithley; 196 | DCV, ACV, <br> resistance checks |
| Dual-trace 100 MHz <br> oscilloscope <br> DC Calibrator | Tektronix; <br> 2235 <br> Fligital waveform <br> checks <br> Accurate DC <br> signal source |  |

### 7.6.2 Self Test

The instrument has a built-in self-test program which can be used to locate some problems. To run the test, simply press the front panel SELF TEST button, or send the command J1X over the IEEE-488 bus. If a problem is found, the unit will display an appropriate message, as summarized in Table 7-11. To return the display to normal, press any key.

Table 7-11. Self Test Display Messages

| Message | Description |
| :--- | :--- |
|  |  |
| MULTIPLIER FAIL | Hardware multiplier failure |
| INVALID | Test failure* |
| 00000 | ROM Error |
| AAAAA | RAM Error |

*Indicates excessive offsets or possible range calibration problem.


Figure 7-13. Rear Panel Disassembly


Figure 7-14. Front Panel Disassembly

### 7.6.3 Diagnostic Program

The diagnostic program can be used as an aid in tracing analog signals through to the input of the A/D converter. Basically, this program selects which of eight signals are routed to the converter for digitization.

Use the diagnostic program as follows:

1. Turn off the power if the instrument is presently turned on.
2. Turn on the power. When the initial Model 590 message is displayed, press and hold CAL until the unit enters the diagnostic program.
3. Use any front panel key to select which multiplexer FET is turned on, as indicated by the associated display message (Table 7-12).
4. To exit the diagnostic program, turn the power off.

Table 7-12. Diagnostic Program Summary

| Display <br> Message | Applied Signal* |
| :---: | :--- |
| 5901 G | 100 kHz module conductance |
| 5901 C | 100 kHz module capacitance |
| 5902 G | 1 MHz module conductance |
| 5902 C | 1 MHz module capacitance |
| COMMON | Anaiog common |
| V NTT | Internal voltage source |
| V EXT | External voltage source |
| V REF | Internal voltage reference source |

*Indicated signal is constantly applied to A/D converter input while message is displayed.

### 7.6.4 Troubleshooting Sequence

The exact troubleshooting sequence will, of course, depend on the particular problem. However, the general sequence shown in the flow chart of Figure 7-15 can be used in many cases. The simplified block diagram in Figure 7-16 indicates which table to consult for procedures to check out various circuits.


Figure 7-15. Troubleshooting Flow Chart


Figure 7-16. Troubleshooting Block Diagram

### 7.6.5 Power Supply Checks

The various power supplies should be checked first to make sure that all are operating as intended. If the various operating voltages are not within required limits, troubleshooting the remaining circuitry can be quite difficult, if not impossible.

Table 7-13 summarizes the procedure for checking the various power supply voltages. In addition to the usual voltage checks, it is a good idea to check the supplies with an oscilloscope to make sure that no noise or ripple is present.

### 7.6.6 Microcomputer and Digital Circuitry Checks

Table 7-14 summarizes the procedure to check out the microcomputer and other digital circuitry located on the digital board.

### 7.6.7 Mother Board

Two of the more important circuits located on the mother board are the $A / D$ converter and the voltage bias source. Check these and other circuits on the board using the procedure summarized in Table 7-15.

### 7.6.8 Display Board

Check out the display board, including the display and keyboard circuits, by using the procedure in Table 7-16. If some of the signals are incorrect, the problem may be on the digital board.

### 7.6.9 100kHz and 1 MHz Capacitance Modules

Table 7-17 gives the procedure for checking out the 100 kHz (5901) capacitance module, and Table 7-18 lists a similar procedure for troubleshooting the 1 MHz (5902) capacitance module.

### 7.7 FAN FILTER CLEANING AND REPLACEMENT

The fan filter, which is located on the rear panel, should be checked periodically for dirt build-up, and cleaned or replaced, as necessary. Use the following procedure to clean or replace the filter, using Figure 7-17 as a guide.

1. Disconnect the line cord from the power line receptacle. 2. Grasp the filter holder, and pull it free of the rear panel. 3. Remove the filter element from the holder.
2. Soak the filter in a solution of warm water and mild detergent until clean. Rinse thoroughly in clean water, and allow the filter to dry completely before installation. If a new filter assembly is required, one may be obtained from Keithley Instruments, Inc. Order part number FL-6.

NOTE
Do no operate the instrument with the filter re-
moved to avoid dirt build-up within the instru-ment-
5. If necessary, clean the fan guard with a damp cloth.
6. Install the filter element in the holder and snap the holder back onto the fan guard. The two tabs on the holder should be oriented at the top and bottom.


Figure 7-17. Fan Filter Removal

Table 7-13. Power Supply Checks

| Step | Item/Component | Required Condition | Remarks |
| ---: | :--- | :--- | :--- |
|  |  |  |  |
| 1 | S302 (Line voltage select) | 115V or 230V as required | Operate on correct voltage |
| 2 | Line fuse (F300) | Continuity | Check with ohmmeter |
| 3 | Power on | Plugged into live outlet |  |
| 4 | VR300, pin 1 | $+11 \mathrm{~V}, \pm 20 \%$ | Referenced to analog common |
| 5 | VR300, pin 2 | $+5 \mathrm{~V}, \pm 5 \%$ | Referenced to analog common |
| 6 | VR301, pin 2 | $-11 \mathrm{~V}, \pm 20 \%$ | Referenced to analog common |
| 7 | VR301, pin 3 | $-5 \mathrm{~V}, \pm 5 \%$ | Referenced to analog common |
| 8 | VR302, pin 1 | $+23 \mathrm{~V}, \pm 20 \%$ | Referenced to analog common |
| 9 | VR302, pin 2 | $+15 \mathrm{~V}, \pm 5 \%$ | Referenced to analog common |
| 10 | VR303, pin 2 | $-23 \mathrm{~V}, \pm 20 \%$ | Referenced to analog common |
| 11 | VR303, pin 3 | $-15 \mathrm{~V}, \pm 5 \%$ | Referenced to analog common |
| 12 | Q300, collector | $+43 \mathrm{~V}, \pm 20 \%$ | Referenced to analog common |
| 13 | Q300, emitter | $+30 \mathrm{~V}, \pm 5 \%$ | Referenced to analog common |
| 14 | Q301, collector | $-43 \mathrm{~V}, \pm 20 \%$ | Referenced to analog common |
| 15 | Q301, emitter | $-30 \mathrm{~V}, \pm 5 \%$ | Referenced to analog common |
| 16 | VR304, pin 1 | $+12 \mathrm{~V}, \pm 20 \%$ | Referenced to digital common |
| 17 | VR304, pin 2 | $+5 \mathrm{~V}, \pm 5 \%$ | Referenced to digital common |

Table 7-14. Microcomputer and Digital Checks

| Step | Item/Component | Required Condition | Remarks |
| :---: | :---: | :---: | :---: |
| 1 |  |  | All signals referenced to digital common |
| 2 | U315, pin 37 | Goes low for $\approx 700 \mathrm{msec}$ upon power up, then stays high. | RESET signal |
| 3 | U315, pin 38 | 8 MHz square wave | MPU clock |
| 4 | U315, pin 34 | 2 MHz square wave | E clock |
| 5 | U315, pin 35 | 2 MHz square wave | Q clock |
| 6 | U315, pin 3 | 976 Hz square wave | 1.024msec $\mathbb{R} \mathrm{Q}$ clock |
| 7 | U315, pins 24-31 | Data bus (D0-D7) | Check for stuck bit |
| 8 | U315, pins 8-23. | Address bus (A0-A15) | Check for stuck bit |
| 9 | U321A, pin 2 | Variable pulses | A/D status information |
| 10 | U332, pin 1 | Varying pulses | A/D data |
| 11 | U316A, pin 2 | Pulse train | Serial clock |
| 12 | U316B, pin 4 | Pulse train | Serial control data |
| 13 | U316C, pin 6 | Pulse train | Serial control strobe |
| 14 | U313, pin 25 | 2 MHz square wave | VIA clock |
| 15 | U311, pin 18 U313, pins 13-16 | 2 MHz square wave Pulse train | IEEE chip clock A/D data |

Table 7-15. Mother Board Checks

| Step | Item/Component | Required Condition | Remarks |
| :---: | :---: | :---: | :---: |
| 1 | Signal reference |  | All voltages referenced to analog common |
| 2 | U134, pin 5 | 8 MHz square wave | 8 MHz clock |
| 3 | U134, pin 7 | 4 MHz square wave | 4 MHz clock |
| 4 | U133, pin 11 | 800 kHz square wave | 800 kHz clock |
| 5 | U119, pin 15 | Pulse train | Serial control data |
| 6 | U119, pin 6 | Pulse train | Serial control clock |
| 7 | U119, pin 12 | Pulse train | Serial control strobe |
| 8 | Programming | Select DC waveform, -19V default bias | Sweep inactive |
| 9 | U127, pin 15 | +9.25V | DAC output |
| 10 | U128, pin 6 | $+9.25 \mathrm{~V}$ |  |
| 11 | Q123 emitter | -19V | Voltage source output |
| 12 | Programming | Program +19V default bias |  |
| 13 | U127, pin 15 | $\div 9.25 \mathrm{~V}$ | DAC output |
| 14 | U128, pin 6 | $-9.25 \mathrm{~V}$ |  |
| 15 | Q123 emitter | $+19 \mathrm{~V}$ | Voltage source output |
| 16 | F100 | Check continuity | External bias fuse |
| 17 | U104, pin 10 | 4 MHz square wave | A/D clock |
| 18 | U106, pin 6 | 50 kHz pulse train | During active sweep |
| 19 | U106, pin 2 | 100 kHz pulse train | During active sweep |
| 20 | U105, pin 6 | 400 kHz pulse train | During active sweep |
| 21 | U110, pin 6 | ${\underset{k}{k-2.5 \rightarrow} \mid}_{M W M}^{M}$ | Integrator waveform during sweep |
| 22 | U113, pin 1 | -10V DC | -10 V reference |
| 23 | Q110 emitter | +5V DC | +5 V reference |
| 24 | R122, R123 function | +1V | A/D reference |
| 25 | CAL button | Press and hold during power up | Enter diagnostic program |
| 26 | Display | Press any key until VREF message is displayed. |  |
| 27 | U100, pin 1 | +1V DC |  |

Table 7-16. Display Board Checks

| Step | Item/Component | Required Condition | Remarks |
| :---: | :---: | :---: | :---: |
| 1 | Self Test | Display segments and LEDs | All on at start of self test |
| 2 | U201 pins 10-16 | Digit select pulses | All voltages referenced to |
| 3 | U202 pins 10-16 | Digit select pulses | digital common |
| 4 | U203 pins 10-16 | Digit select pulses |  |
| 5 | U204, pin 2 | 1 msec negative going pulse every 10 msec when S201-S204 closed | Switch matrix strobe |
| 6 | U204, pin 2 | 1 msec pulse every 10 msec when S205-S208 closed |  |
| 7 | U204, pin 6 | 1 msec pulse every 10 msec when S209-S212 closed |  |
| 8 | U204, pin 12 | 1 msec pulse every 10 msec when S213-S216 closed |  |
| 9 | U204, pin 10 | 1 msec pulse every 10 msec when S217-S220 closed |  |
| 10 | U204, pin 8 | 1 msec pulse every 10 msec when S221-S224 closed |  |
| 11 | U205, pin 2 | 1 msec pulse every 10 msec when S225-S228 closed |  |
| 12 | U205, pin 4 | 1 msec pulse every 10 msec when S229-S232 closed |  |
| 13 | U205, pin 6 | 1 msec pulse every 10 msec when S233 closed |  |

Table 7-17. 100kHz Capacitance Madule Checks

| Step | Item/Component | Required Condition | Remarks |
| :---: | :---: | :---: | :---: |
| 1 | Reference point |  | Following voltages reference to digital common. |
| 2 | U502, pin 10 | 800 kHz square wave | 800 kHz clock |
| 3 | U506, pin 10 | 100 kHz square wave | Detector A signal |
| 4 | U506, pin 12 | 100 kHz square wave | Detector B signal |
| 5 | U506, pin 8 | 100 kHz square wave | Detector C signal |
| 6 | U506, pin 6 | 100 kHz square wave | Detector D signal |
| 7 | Q500 base |  | Synthesized waveform |
| 8 | Reference point |  | Following voltages referenced to analog common |
| 9 | Q500 collector | $100 \mathrm{kHz}, 10 \mathrm{~V}$ p-p sine wave | Test frequency |
| 10 | U508, pin 6 | $100 \mathrm{kHz}, 1 \mathrm{~V}$ p-p sine wave | Test frequency |
| 11 | Test output high | 100 kHz 42 mV p-p sine wave | Test frequency |
| 12 | U510, pin 6 | +4 VDC - | AGC voltage |
| 13 | Range, frequency | Select 2 nF range, 100 kHz |  |
| 14 | Reference capacitor | Connect full scale ( $1.8-2 \mathrm{nF}$ ) capacitor between test INPUT and test OUTPUT jacks | Leave capacitor connected for following tests |
| 15 | U512, pin 6 | $100 \mathrm{kHz}, 175 \mathrm{mV}$ p-p sine wave | Amplitude depends on capacitance value |
| 16 | U513, pin 6 | $100 \mathrm{kHz}, 1 \mathrm{~V}$ p-p sine wave | Amplitude depends on capacitance value |
| 17 | U514, pin 6 | $100 \mathrm{kHz}, 6.3 \mathrm{~V}$ p-p sine wave | Amplitude depends on capacitance value |
| 18 | U515, pin 7 | $1.8-2 \mathrm{~V}$ DC | Voltage analogous to applied capacitance |
| 19 | U515, pin 1 | $1.8-2 \mathrm{~V}$ DC | Voltage analogous to applied capacitance |
| 20 | U516, pin 7 | 1.8-2V DC | Voltage analogous to applied capacitance |
| 21 | Test jacks | Connect 2 mS conductance | Leave conductance connected for following tests |
| 22 | U517, pin 1 | 2V DC | Voltage depends on applied conductance |
| 23 | U517, pin 1 | 2V DC | Voltage depends on applied conductance |
| 24 | U516, pin 1 | 2V DC | Voltage depends on applied conductance |

Table 7-18. 1 MHz Capacitance Module Checks

| Step | Item/Component | Required Condition | Remarks |
| :---: | :---: | :---: | :---: |
| 1 | Reference point |  | Following voltages referenced to digital common. |
| 2 | U602, pin 13 | 8 MHz square wave | 8 MHz clock |
| 3 | U601, pin 4 | 1 MHz square wave | Detector A signal |
| 4 | U601, pin 2 | 1 MHz square wave | Detector B signal |
| 5 | U601, pin 6 | 1 MHz square wave | Detector C signal |
| 6 | $\text { U601, pin } 10$ Q601 base | 1 MHz square wave | Detector D signal Synthesized waveform |
|  |  |  |  |
| 8 | Reference point |  | Following voltages referenced to analog common |
| 9 | Q601 collector | $1 \mathrm{MHz}, 12 \mathrm{~V}$ p-p sine wave | Test frequency |
| 10 | U606, pin 6 | 1 MHz , $4.5 \mathrm{p}-\mathrm{p}$ sine wave | Test frequency |
| 11 | Test output high | $1 \mathrm{MHz}, 42 \mathrm{mV}$ p-p sine wave | Test frequency |
| 12 | U608, pin 6 | $+3 \mathrm{VDC}$ | AGC voltgae. |
| 13 | Range, frequency | Select 2 nF range, 1 MHz |  |
| 14 | Reference capacitor | Connect full scale ( 2 nF ) capacitor between test INPUT and test OUTPUT jacks | Leave capacitor connected for following tests |
| 15 | U610, pins 7 and 8 | $1 \mathrm{MHz}, 300 \mathrm{mV}$ p-p sine wave | Amplitude depends on capacitance value |
| 16 | U611, pins 7 and 8 | $1 \mathrm{MHz}, 2.5 \mathrm{~V}$ p-p sine wave | Amplitude depends on capacitance value |
| 17 | U612, pin 8 | 1 MHz , 5 V p -p sine wave | Amplitude depends on capacitance value |
| 18 | U614, pin 6 | $1.8-2 \mathrm{~V}$ DC | Voltage is analogous to capacitance |
| 19 | U617, pin 1 | 1.8-2V DC | Voltage is analogous to capacitance |
| 20 | U616, pin 1 | 1.8-2V DC | Voltage is analogous to capacitance |
| 21 | Test jacks | Connect 20 mS conductance | Leave conductance connected for following tests |
| 22 | U615, pin 6 | 2V DC | Voltage depends on conductance value |
| 23 | U617, pin 7 | 2V DC | Voltage depends on conductance value |
| 24 | U616, pin 7 | 2V DC | Voltage depends on conductance value |

## SECTION 8 <br> REPLACEABLE PARTS

### 8.1 INTRODUCTION

This section contains replacement parts information, schematic diagrams, and component layout drawings for the Model 590 CV Analyzer, as well as the 100 kHz and 1 MHz capacitance modules. Also included is an exploded view showing the general mechanical layout of the instrument for parts identification.

### 8.2 ELECTRICAL PARTS LISTS

Electrical parts for the Model 590 circuit boards as well as the 100 kHz and 1 MHz modules are listed in Tables 8-1 through 8-6. Parts in each table are listed alphabetically in order of circuit designation. The parts lists are integrated with the component layout drawings and schematic diagrams for the respective circuit boards.

### 8.3 MECHANICAL PARTS

Parts for the case assembly are listed in Table 8-7. Miscellaneous mechanical parts are listed in Table 8-8, while Table 8-9 lists parts for the Model 5904 Input Adapter. See the assembly drawings in Section 7 for the location of parts.

### 8.4 ORDERING INFORMATION

Keithley Instruments, Inc. maintains a complete inventory of all normal replacement parts. To place an order, or to obtain information concerning replacement parts, contact your Keithley representative or the factory. See the inside front cover of this manual for addresses.

When ordering parts, include the following:
2. Instrument serial number.
3. Part description.
4. Circuit designation, including schematic diagram and component layout numbers (ii applicable).
5. Keithley part number.

### 8.5 FACTORY SERVICE

If the instrument or modules are to be returned to the factory for service, carefully pack them and include the following information:

1. Complete the service form at the back of this manual and return it with the instrument.
2. Advise as to the warranty status of the instrument (see the inside front cover of this manual for warranty information.
3. Write the following on the shipping label: ATTENTION REPAIR DEPARTMENT.

### 8.6 COMPONENT LOCATION DRAWINGS AND SCHEMATIC DIAGRAMS

Component location drawings and schematic diagrams for the various circuit boards can be found on the following pages arranged as follows:

| Board | Component <br> Layout <br> Number | Schematic <br> Diagram <br> Number | Parts <br> Table <br> Number |
| :--- | :---: | :---: | :---: |
| Mother | $590-100$ | $590-106$ | $8-1$ |
| Display | $590-110$ | $590-116$ | $8-2$ |
| Digital | $590-120$ | $590-126$ | $8-3$ |
| $5901(100 \mathrm{kHz})$ | $5901-100$ | $5901-106$ | $8-4$ |
| $5902(1 \mathrm{MHz})$ | $5902-100$ | $5902-106$ | $8-5$ |
| KI590 Op Amp (U607) | $5902-180$ | $5902-186$ | $8-6$ |

1. Instrument model number.

Table 8-1. Mother Board, Parts List

| Circuit <br> Designation | Description | Keithley Part Number |
| :---: | :---: | :---: |
| C100 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%, 50 \mathrm{~V}$ | C-365-0.1 |
| C101 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 0 V | C-365-0.1 |
| C102 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C103 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C104 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 00 V | C-365-0.1 |
| C105 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C106 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C107 | Capacitor, 0.1 $\mu \mathrm{F}, 20 \%$, 50V | C-365-0.1 |
| C108 | Capacitor, $470 \mathrm{pF}, \mathrm{Ceramic}$ Disc | C-64-470p |
| C109 | Capacitor, 0.1pF, $20 \%, 50 \mathrm{~V}$ | C-365-0.1 |
| C110 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%, 50 \mathrm{~V}$ | C-365-0.1 |
| ${ }^{C 111}$ | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%, 50 \mathrm{~V}$ | C-365-0.1 |
| ${ }_{C} 112$ | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%, 50 \mathrm{~V}$ | C-365-0.1 |
| ${ }^{\text {Cl13 }}$ | Capacitor, $0.001 \mu \mathrm{~F}$, Ceramic Disc | C-64-0.001 |
| ${ }^{\text {c114 }}$ | Capacitor, $10 \mu \mathrm{~F}, 25 \mathrm{~V}$, Aluminum Electrolytic | C-314-10 |
| C115 | Capacitor, $0.0047 \mu \mathrm{~F}, 10 \%$, 100 V , Metallized Polypropylene | C-306-0.0047 |
| C116 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C117 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%, 50 \mathrm{~V}$ | C-365-0.1 |
| C118 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%, 50 \mathrm{~V}$ | C-365-0.1 |
| C119 | Capacitor, $0.47 \mu$ F, 50V, Ceramic Film | C-237-0.47 |
| C120 | Capacitor, $0.01 \mu \mathrm{~F}, 500 \mathrm{~V}$, Ceramic Disc | C-22-0.01 |
| C121 | Capacitor, 100pF, Ceramic Disc | C-64-100p |
| C122 | Capcitor, $0.01 \mu \mathrm{~F}, 500 \mathrm{~V}$, Ceramic Disc | C-22-0.01 |
| C123 | Capcitor, $0.01 \mu \mathrm{~F}, 500 \mathrm{~V}$, Ceramic Disc | C-22-0.01 |
| C124 | Capcitor, $0.01 \mu \mathrm{~F}, 500 \mathrm{~V}$, Ceramic Disc | C-22-0.01 |
| C125 | Capacitor, $0.1 \mu \mathrm{~F}, 250 \mathrm{~V}$, Metallized Polyester | C-178-0.1 |
| C126 | Capacitor, 220pF, Ceramic Disc | C-64-220p |
| C127 | Capacitor, $0.001 \mu \mathrm{~F}, 500 \mathrm{~V}$, Ceramic Disc | C-22-0.001 |
| C128 | Capacitor, $10 \mu \mathrm{~F}, 35 \mathrm{~V}$, Aluminum Electrolytic | C-309-10 |
| C129 | Capacitor, $10 \mu \mathrm{~F}, 35 \mathrm{~V}$, Aluminum Electrolytic | C-309-10 |
| C130 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.01 |
| C131 | Capacitor, 0.1 $\mu \mathrm{F}, 20 \%$, 50 V | C-365-0.01 |
| C132 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%, 50 \mathrm{~V}$ | C-365-0.01 |
| C133 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.01 |
| C134 | Capacitor, $10 \mu \mathrm{~F}, 25 \mathrm{~V}$, Aluminum Electrolytic | C-314-10 |
| ${ }_{C} 135$ | Capacitor, $10 \mu \mathrm{~F}, 25 \mathrm{~V}$, Aluminum Electrolytic | C-314-10 |
| C136 | Capacitor, $200 \mathrm{pF}, 1 \%, 500 \mathrm{~V}$, Mica | C-209-200p |
| C137 | Capacitor, $10 \mu \mathrm{~F}, 16 \mathrm{~V}$, Aluminum Electrolytic | C-321-10 |
| C138 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C139 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%, 50 \mathrm{~V}$ | C-365-0.1 |
| C140 | Capacitor, 20pF, 5\%,500V Mica | C-236-20 |
| C141 | Not Used |  |
| C142 | Not Used |  |
| C143 | Not Used |  |
| C144 | Not Used |  |
| C145 | Capacitor, 0.01んF, 500V, Ceramic Disc | C-22-0.01 |
| CR100 | Diode, Silicon, 1N4148 | RF-28 |
| CR101 | Diode, Silicon, 1N4148 | RF-28 |
| CR102 | Diode, Silicon, 1N4148 | RF-28 |
| CR103 | Diode, Silicon, 1 N4148 | RF-28 |

Table 8-1. Mother Board, Parts List (Cont.)

| Circuit <br> Designation | Description | Keithley Part Number |
| :---: | :---: | :---: |
| CR104 | Diode, Silicon, 1 N4148 | RF-28 |
| CR105 | Diode, Silicon, 1 N4148 | RF-28 |
| CR106 | Diode, Silicon, 1N4148 | RF-28 |
| CR107 | Not Used |  |
| CR108 | Diode, Silicon, 1 N4148 | RF-28 |
| F100 | Fuse, $1 / 8 \mathrm{~A}, 250 \mathrm{~V}, 8 \mathrm{AG}$ | FU-5 |
| J1017 | Connector, SMB Jack | CS-545 |
| J1020 | Connector | CS-533-9 |
| J1021 | Connector, Modified | 590-320-1 |
| 51023 | Connector, SMB Jack | CS-545 |
| 11024 | Connector, SMB Jack | CS-545 |
| J1025 | Connector | CS-533-2 |
| J1026 | Connector | CS-533-10 |
| J1027 | Connector, Modified | 590-320-1 |
| J1029 | Connector, SMB Jack | CS-545 |
| J1030 | Connector, SMB Jack | CS-545 |
| J1031 | Connector | CS-533-2 |
| J1032 | Connector, SMB Jack | CS-545 |
| J1033 | Connector, SMB Jack | CS-545 |
| J1034 | Connector, SMB Jack | CS-545 |
| J1035 | Connector, SMB Jack | CS-545 |
| J1036 | Connector, SMB Jack | CS-545 |
| J1037 | Connector, SMB Jack | CS-545 |
| J1038 | Connector, SMB Jack | CS-545 |
| K100 | Relay | RL-94 |
| K101 | Relay | RL-94 |
| K102 | Relay | RL-94 |
| K103 | Relay | RL-94 |
| K104 | Relay | RL-94 |
| K105 | Relay | RL-94 |
| K106 | Relay | RL-95 |
| K107 | Relay | RL-95 |
| K108 | Relay | RL-101 |
| K109 | Not Used |  |
| K110 | Not Used |  |
| K111 | Relay | RL-101 |
| Q100 | Transistor, N-Channel JFET, PF5301 | TG-139 |
| Q101 | Transistor, N-Channel JFET, PF5301 | TG-139 |
| Q102 | Transistor, N-Channel JFET, PF5301 | TG-139 |
| Q103 | Transistor, N-Channel JFET, PF5301 | TG-139 |
| Q104 | Transistor, N-Channel JFET, PF5301 | TG-139 |
| Q105 | Transistor, N-Channel JFET, PF5301 | TG-139 |
| Q106 | Transistor, N-Channel JFET, PF5301 | TG-139 |
| Q107 | Transistor, N-Channel JFET, PF5301 | TG-139 |
| Q108 | Transistor, N-Channel JFET, PF5301 | TG-139 |
| Q109 | Transistor, N-Channel JFET, PF5301 | TG-139 |
| Q110 | Transistor, Silicon, NPN, 2N3904 | TG-47 |

## Table 8-1. Mother Board, Parts List (Cont.)

| Circuit Designation | Description | Keithley Part Number |
| :---: | :---: | :---: |
| Q111 | Transistor, N-Channel FET, 2N4392 | TG-128 |
| Q112 | Transistor, N-Channel FET, 2N5434 | TG-174 |
| Q113 | Not Used |  |
| Q114 | Not Used |  |
| Q115 | Not Used |  |
| Q116 | Transistor, MP8099 | TG-157 |
| Q117 | Transistor, Power, NPN, MJE240 | TG-185 |
| Q118 | Transistor, Power, PNP, MJE250 | TG-186 |
| Q119 | Transistor, Power, PNP, MPS8599 | TG-158 |
| Q120 | Diode, Current Regulator, $J 505$ | TG-140 |
| Q121 | Diode, Current Regulator, 1505 | TG-140 |
| Q122 | Transistor, Silicon, PNP, 2N3906 | TG-84 |
| Q123 | Transistor, Silicon, PNP, 2N3904 | TG-47 |
| Q124 | Transistor, N-Channel FET, 2N4392 | TG-128 |
| R100 | Resistor, Thick Film | TF-177-3 |
| R101 | Resistor, $4.7 \mathrm{k} \Omega$, $5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-4.7k |
| R102 | Resistor, $4.7 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-4.7k |
| R103 | Resistor, $1 \mathrm{Ma}, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R.76-1M |
| R104 | Resistor, $1 \mathrm{M} \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-1M |
| R105 | Resistor, $1 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-1k |
| R106 | Resistor, 200@, $0.1 \%, 1 / 10 \mathrm{~W}$, Metal Film | R-263-1k |
| R107 | Resistor, 11.5k 1 , 1\%, 1/8 W | R-88-11.5k |
| R108 | Resistor, $26.7 \mathrm{k} \Omega, 1 \%, 1 / \mathrm{W}$ | R-88-26.7k |
| R110 | Resistor, $10 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}, \mathrm{Composition}$ | R-76-10k |
| R111 | Resistor, $7.78 \mathrm{k} \Omega, 0.1 \%, 1 / 8 \mathrm{~W}$ | R-176-7.78k |
| R112 | Resistor, 142.8k ${ }^{\text {, }} 0.1 \%, 1 / 8 \mathrm{~W}$ | R-176-142.8k |
| R113 | Resistor, 1M8, $0.1 \%$, $1 / \mathrm{s}$ W | R-176-1M |
| R114 | Resistor, $10 \mathrm{ka}, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-10k $\mathrm{R}-76-3.9 \mathrm{k}$ |
| R115 | Resistor, 3.9kn, 5\%, 1/4W, Composition | R-76-3.9k R-76-3k |
| R116 | Resistor, 3ks, 5\%, 1/4W, Composition | R-76-3k |
| R117 | Resistor, $3 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}, \mathrm{Composition}$ | R-76-3k |
| R118 | Resistor, $10 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}, \mathrm{Composition}$ | ${ }_{\text {R } 776-200 \mathrm{k}}$ |
| R119 | Resistor, $220 \mathrm{k} \mathrm{l}_{5} 5 \%$, 1/4W, Composition | R-76-220k |
| R120 | Resistor, $10 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}, \mathrm{Composition}$ | R-88-7.87k |
| R121 | Resistor, 7.87k ${ }^{\text {, }} 1 \%$, $1 / \mathrm{s} \mathrm{W}$ | ${ }_{\text {R-88-7.87-1k }}$ |
| R122 |  | R-263-1k |
| R123 | Resistor, 4k ${ }^{\text {c }}$, 0.1\%. $1 / 10 \mathrm{~W}$, Metal Film | R-263-4k |
| R124 R125 | Resistor, $1.33 \mathrm{k} \Omega, 0.1 \%, 1 / 10 \mathrm{~W}$, Metal Film Resistor, $1 \mathrm{k}, 1 \%, 1 / 8 \mathrm{~W}$ | R-263-1.33k R-88-1k |
| R126 | Resistor, $3.65 \mathrm{k} \Omega, 1 \%, 1 / 3 \mathrm{~W}$ | R-88-3.65k |
| R127 | Resistor, $6.49 \mathrm{k} \Omega, 1 \%, 1 / \mathrm{sW}$ | R-88-6.49k |
| R128 | Resistor, $10 \mathrm{k} \Omega, 1 \%, 1 / \mathrm{s} \mathrm{W}$ | R-88-10k |
| R129 | Resistor, $10 \mathrm{k} \Omega, 1 \%, 1 / \mathrm{W}$ | R-88-10k |
| R130 | Resistor, $1 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}, \mathrm{Composition}$ | R-76-1k |
| R131 | Resistor, Thick Film | TF-108 |
| R132 | Resistor, 1M8, 5\%, 1/4W, Composition | R-76-1M |
| R133 | Resistor, $1 \mathrm{M} \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R76-1M |
| R134 | Resistor, Thick Film | TF-179-1 |
| R135 | Resistor, $1 \mathrm{k} \Omega, 5 \%$, 1/4W, Composition | R-76-1k |
| R136 | Not Used |  |

## Table 8-1. Mother Board, Parts List (Cont.)

| Circuit Designation | Description | Keithley Part Number |
| :---: | :---: | :---: |
| R 137 | Resistor, $10 \mathrm{k} \Omega, 0.1 \%, 1 / \mathrm{so}$ W, Metal Film | R-263-10k |
| R138 | Resistor, 10k ${ }^{\text {, }} 5 \%$, $1 / 4 \mathrm{~W}$, Composition | R-76-10k |
| R139 | Resistor, $6.2 \mathrm{k} \Omega, 5 \%$, 14 W , Composition | R-76-6.2k |
| R140 | Resistor, $10 \mathrm{k} \Omega, 5 \%$, $1 / 4 \mathrm{~W}$, Composition | R76-10k |
| R141 | Resistor, $6.2 \mathrm{k} \Omega, 5 \%, 1 / \mathrm{W}$, Composition | R.76-6.2k |
| R 142 | Resistor, 4.7 k , , 5\%, 1/4W, Composition | R-76-4.7k |
| R143 | Resistor, $4.7 \mathrm{k} \Omega, 5 \%$, $1 / \mathrm{WW}$, Composition | R.76-4.7k |
| R144 | Resistor, $10 \mathrm{kQ}, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-10k |
| R145 | Resistor, $10 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R.76-10k |
| R146 | Resistor, $10 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}, \mathrm{Composition}$ | R-76-10k |
| R147 | Resistor, 2.2 M , $5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-2.2M |
| R148 | Resistor, 4.7k@, 5\%, $1 / 4 \mathrm{~W}$, Composition | R-76-4.7k |
| R149 | Resistor, $20 \mathrm{kQ}, 0.1 \%, 1 / 10 \mathrm{~W}$, Metal Film | R-263-20k |
| R150 | Potentiometer, 2009, $1 / 2 \mathrm{~W}$, Cermet | RP-97-200 |
| R151 | Resistor, 20kn, 0.1\%, $1 / 10 \mathrm{~W}$, Metal Film | R-263-20k |
| R152 | Potentiometer, $10 \mathrm{k} \Omega, 1 / 2 \mathrm{~W}$, Cermet | RP-97-10k |
| R153 | Resistor, $301 \mathrm{kS}, 1 \%, 1 / 5 \mathrm{~W}$ | R-88-301k |
| R154 | Resistor, 6.04 k , 1\%, $1 / 1 / \mathrm{W}$ | R-88-6.04k |
| R155 | Resistor, 301k ${ }^{\text {, }} 1 \%$, $1 / 6 \mathrm{~W}$ | R-88-301k |
| R156 | Potentiometer, $100 \mathrm{k} \Omega, 1 / 2 \mathrm{~W}$, Cermet | RP-97-100k |
| R157 | Potentiometer, $100 \mathrm{kr}, 1 / 2 \mathrm{~W}$, Cermet | RP-97-100k |
| R158 | Resistorr, 1M9, 1\%, $1 / \mathrm{s}$ W | R-88-1M |
| R159 | Resistor, 10 k , $1 \%$, $1 / 8 \mathrm{~W}$ | R-88-10k |
| R160 | Resistor, $49.9 \mathrm{k} \Omega, 1 \%$, $1 / \mathrm{s} \mathrm{W}$ | R-88-49.9k |
| R161 | Resistor, $9.76 \mathrm{k} \Omega, 0.1 \%, 1 / 1 \mathrm{I}^{\text {W }}$, Metal Film | R-263-9.76k |
| R162 | Resistor, 20k』, 0.1\%, $1 / 10 \mathrm{~W}$, Metal Film | R-263-20k |
| R163 | Resistor, $10 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-10k |
| R164 | Resistor, $4.7 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-4.7k |
| R165 | Resistor, 191kn, $1 \%$, 1/8 W | R-88-191k |
| R166 | Resistor, 2008, $5 \%$, 1/4W, Composition | R-76-200 |
| R167 | Resistor, 2008, 5\%, 1/4W, Composition | R-76-200 |
| R168 | Resistor, 12, 5\%, 1/4W, Composition | R-76-12 |
| R169 | Resistor, 12, 5\%, 1/4W, Composition | R-76-12 |
| R170 | Resistor, $10 \mathrm{k} \Omega, 1 \%, 1 / 8 \mathrm{~W}$ | R-88-10k |
| R171 | Resistor, 8660, 1\%, ${ }^{1 / 3} \mathrm{~W}$ | R-88-866 |
| R172 | Resistor, 3.83k ${ }^{\text {, }} 1 \%$, $1 / 8 \mathrm{~W}$ | R-88-3.83k |
| R173 | Resistor, $6.19 \mathrm{kd}$, , 1\%, $1 / 8 \mathrm{~W}$ | R-88-6.19k |
| R174 | Resistor, Thick Film | TF-39 |
| R175 | Resistor, 10kn, $1 \%$, $1 / s \mathrm{~W}$ | R-88-10k |
| ${ }^{\mathrm{R} 176}$ | Resistor, 10kn, 1\%, 1/s W | R-88-10k |
| R177 | Resistor, 8660, 1\%, $1 / \mathrm{s} \mathrm{W}$ | R-88-866 |
| R178 | Resitor, $4.7 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-4.7k |
| R179 | Resistor, Thick Film | TF-178-1 |
| R180 | Resistor, $1.8 \mathrm{k} \Omega, 0.1 \%, 1 / 20 \mathrm{~W}$, Metal Film | R-263-1.8k |
| R181 | Resistor, $10 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-10k |
| R182 | Resistor, $990 \mathrm{k} \Omega$, $0.1 \%$, 1/4 W, Metal Film | R-264-990k |
| R183 | Resistor, $100 \mathrm{kS}, 0.1 \%, 1 / 10 \mathrm{~W}$, Metal Film | R-263-100k |
| R184 | Resistor, $10 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-10k |
| R185 | Resistor, $10 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-10k |
| R186 R187 | Resistor, 1M 2 , 5\%, $1 / 4 \mathrm{~W}$, Composition Not Used | R-76-1M |

Table 8-1. Mother Board, Parts List (Cont.)

| Circuit Designation | Description | Keithley Part Number |
| :---: | :---: | :---: |
| R188 | Resistor, $900 \mathrm{k} \Omega, 0.1 \%, 1 / 4 \mathrm{~W}$, Metal Film | R-264-900k |
| S100 | Switch | SW-318 |
| U100 | IC, LF442A | IC-410 |
| U101 | IC, Triple 2-Channel Analog Mux, CD4053B | IC-283 |
| U102 | IC, Selected | 31847-1 |
| U103 | IC, Quad 2-Input NAND Gate, 74HC00 | IC-351 |
| U104 | IC, Quad 2-Input NOR Gate, 74 HCO 2 | IC-412 |
| U105 | IC, Synchronous Decade Counter, 74HC192 | IC-417 |
| U106 | IC, Synchronous Binary Counter, $74 \mathrm{HC193}$ | IC-416 |
| U107 | IC, Quad Comparator, LM339 | IC-219 |
| U108 | IC, Dual D Flip-Flop, 74HC74 | 1-3137 |
| U109 | IC, Dual D Flip-Flop, 74 HC 74 | IC-337 |
| U110 | IC, Operational Amplifier, LM356 | IC-209 |
| U111 | IC, Dual Comparator, LM393 | IC-343 |
| 0112 | IC, JFET Operational Amplifier, LM356 | IC-209 |
| U113 | IC, Dual JFET Operational Amplifier, LF442C | IC-325 |
| U114 | IC, Quad Comparator, LM339 | IC-219 |
| U115 | IC, 1-of-8 Decoder, 74HC138 | IC-431 |
| U116 | IC, Quad Comparator, LM339 | IC-219 |
| U117 | IC, Quad Comparator, LM339 | IC-219 |
| U118 | IC, CMOS, Quad 2-Input NAND Gate, 4011 | IC-102 |
| U119 | IC, CMOS, Hex Inverter, 4049 | IC-106 |
| U120 | IC, CMOS, 8 -Stage Shift/Store Register, 14094BCP | IC-251 |
| U121 | IC, CMOS, 8 -Stage Shift/Store Register, 14094BCP | IC-251 |
| U122 | IC, CMOS, 8 -Stage Shift/Store Register, 14094BCP | IC-251 |
| U123 | IC, CMOS, 8 -Stage Shift/Store Register, 14094BCP | IC-251 |
| U124 | IC, Darlington Transistor Array, 2003 | IC-206 |
| U125 | IC, CMOS 8-Stage Shift Register, 4021 | IC-130 |
| U126 | IC, Quad Comparator, LM339 | IC-219 |
| U127 | IC, D/A Converter, DAC80 | IC-323 |
| U128 | IC, Operational Amplifier, AD-3247 | IC-77 |
| U129 | IC, Quad Comparator, LM339 | IC-219 |
| U130 | IC, High Voltage Operational Amplifier, LM343H | IC-432 |
| U131 | IC, Quad CMOS Analog Switch, DG211 | IC-320 |
| U132 | Not Used |  |
| U133 | IC, Counter, 74LS90 | IC-373 |
| U134 | IC, Dual Power MOSFET Driver, TSC426 IC, Hex Inverter, 74 HC 04 | IC-437 |
| VR100 | Regulator, Zener Diode, $6.33 \mathrm{~V}, 400 \mathrm{~mW}, 1 \mathrm{~N} 4577 \mathrm{~A}$ | DZ-58 |
| VR101 | Regulator, Zener Diode, 5.1V, $10 \%$, $400 \mathrm{~mW}, 1 \mathrm{~N} 751$ | DZ-59 |
| Y100 | Crystal, $8 \mathrm{MHz}, \pm 100 \mathrm{ppm}$ | CR-25-4 |



Figure 8-1. Mother Board, Component Location Drawing, Dwg. No. 590-100


Figure 8-2. Mother Board, Schematic Diagram, Dwg. No. 590-106 (sheet 1 of 2)


Figure 8-2. Mother Board, Schematic Diagram, Dwg. N. 590-106 (sheet 2 of 2)

## Table 8-2. Display Board, Parts List

| Circuit <br> Designation | Description | Keithley Part Number |
| :---: | :---: | :---: |
| C201 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-1 |
| C202 | Capacitor, $10 \mu \mathrm{E}, 25 \mathrm{~V}$, Aluminum Electrolytic | C-314-10 |
| DS201 | Digital Display, Dual-Digit, 14-Segment | DD-39 |
| DS202 | Digital Display, Dual-Digit, 14-Segment | DD-39 |
| DS203 | Digital Display, Dual-Digit, 14-Segment | DD-39 |
| DS204 | Digital Display, Dual-Digit, 14-Segment | DD-39 |
| DS205 | Digital Display, Dual-Digit, 14-Segment | DD-39 |
| DS206 | Digital Display, Dual-Digit, 14-Segment | DD-39 |
| DS207 | Digital Display, Dual-Digit, 14-Segment | DD-39 |
| DS208 | Digital Display, Dual-Digit, 14-Segment | DD-39 |
| DS209 | Digital Display, Dual-Digit, 14-Segment | DD-39 |
| DS210 | Digital Display, Dual-Digit, 14-Segment | DD-39 |
| DS211 | LED, Red | PL-71 |
| DS212 | LED, Red | PL-71 |
| DS213 | LED, Red | PL-71 |
| DS214 | LED, Red | PL71 |
| DS215 | LED, Red | PL-71 |
| DS216 | LED, Red | PL-71 |
| DS217 | LED, Yellow | PL-72 |
| DS218 | LED, Red | PL-71 |
| DS219 | LED, Red | PL71 |
| DS220 | LED, Red | PLF1 |
| DS221 | LED, Red | PLT1 |
| DS222 | LED, Red | PL71 |
| DS223 | LED, Yellow | PL72 |
| P1014 | Cable Assembly | CA-32-5 |
| S201 | Switch, Pushbutton Momentary Contact | SW-435 |
| S202 | Switch, Pushbutton Momentary Contact | SW-435 |
| S203 | Switch, Pushbutton Momentary Contact | SW-435 |
| S204 | Switch, Pushbutton Momentary Contact | SW-435 |
| S205 | Switch, Pushbutton Momentary Contact | SW-435 |
| S206 | Switch, Pushbutton Momentary Contact | SW-435 |
| S207 | Switch, Pushbutton Momentary Contact | SW-435 |
| S208 | Switch, Pushbutton Momentary Contact | SW-435 |
| S209 | Switch, Pushbutton Momentary Contact | SW-435 |
| S210 | Switch, Pushbutton Momentary Contact | SW-435 |
| S211 | Switch, Pushbutton Momentary Contact | SW-435 |
| S212 | Switch, Pushbutton Momentary Contact | SW-435 |
| 5213 | Switch, Pushbutton Momentary Contact | SW-435 |
| S214 | Switch, Pushbutton Momentary Contact | SW-435 |
| S215 | Switch, Pushbutton Momentary Contäct | SW-435. |
| S216 | Switch, Pushbutton Momentary Contact | -SW-435 |
| S217 | Switch, Pushbutton Momentary Contact | SW-435 |
| S218 | Switch, Pushbutton Momentary Contact | SW-435 |
| S219 | Switch, Pushbutton Momentary Contact | SW-435 |
| S220 | Switch, Pushbutton Momentary Contact | SW-435 |
| S221 | Switch, Pushbutton Momentary Contact | SW-435 |
| S222 | Switch, Pushbutton Momentary Contact ${ }^{-}$ | SW-435 |

Table 8-2. Display Board, Parts List (Cont.)

| Circuit | Descrignation | Description |
| :--- | :--- | :--- |
| Designeithley |  |  |
| S223 | Switch, Pushbutton Momentary Contact | Part Number |
| S224 | Switch, Pushbutton Momentary Contact | SW-435 |
| S225 | Switch, Pushbutton Momentary Contact | SW-435 |
| S226 | Switch, Pushbutton Momentary Contact | SW-435 |
| S227 | Switch, Pushbutton Momentary Contact | SW-435 |
| S228 | Switch, Pushbutton Momentary Contact | SW-435 |
| S229 | Switch, Pushbutton Momentary Contact | SW-435 |
| S230 | Switch, Pushbutton Momentary Contact | SW-435 |
| S231 | Switch, Pushbutton Momentary Contact | SW-435 |
| S232 | Switch, Pushbutton Momentary Contact | SW-435 |
| S233 | Switch, Pushbutton Momentary Contact | SW-435 |
|  |  | SW-435 |
| $U 201$ | Int. Circuit (2003) |  |
| U202 | Int. Circuit (2003) | IC-206 |
| U203 | Int. Circuit (2003) | IC-206 |
| U204 | Int. Circuit (74LS05) | IC-206 |
| U205 | Int. Circuit (74LS05) | IC-141 |
| U206 | Int. Circuit (74HCT164) | IC-14I |
| U207 | Int. Circuit (74HCT164) | IC-456 |



Figure 8-3. Display Board, Component Location Drawing, Dwg. No. 590-110


Figure 8-4. Display Board, Schematic Diagram, Dwg. No. 590-116

Table 8－3．Digital Board，Parts List

| Circuit <br> Designation | Description | Keithley Part Number |
| :---: | :---: | :---: |
| C301 | Capacitor， $0.1 \mu \mathrm{~F}, 20 \%, 50 \mathrm{~V}$ | C－365－0．1 |
| C302 | Not Used |  |
| C303 | Capacitor，0．1 $\mu \mathrm{F}, 20 \%$ ， 50 V | C－365－0．1 |
| C304 | Capacitor，0．1 $\mu \mathrm{F}, 20 \%$ ，50V | C－365－0．1 |
| C305 | Capacitor，0．1 $\mu \mathrm{F}, 20 \%$ ， 50 V | C－365－0．1 |
| C306 | Capacitor， $0.1 \mu \mathrm{~F}, 20 \%$ ， 50 V | C－365－0．1 |
| C307 | Capacitor，0．1退，20\％，50V | C－365－0．1 |
| C308 | Capacitor，0．1 $\mu \mathrm{F}, 20 \%$ ， 50 V | C－365－0．1 |
| C309 |  | C－365－0．1 |
| C310． | Capacitor， $0.1 \mu \mathrm{~F}, 20 \%$ ， 50 V | C－365－0．1 |
| C311 | Capacitor， $0.1 \mu \mathrm{~F}, 20 \%$ ， 50 V | C－365－0．1 |
| C312 | Capacitor， $0.1 \mu \mathrm{~F}, 20 \%$ ， 50 V | C－365－0．1 |
| C313 | Capacitor，0．1震，20\％，50V | C－365－0．1 |
| C314 | Capacitor， $0.1 \mu \mathrm{~F}, 20 \%$ ， 0 V | C－365－0．1 |
| C315 | Capacitor， $0.1 \mu \mathrm{~F}, 20 \%, 50 \mathrm{~V}$ | C－365－0．1 |
| C316 | Capacitor， $0.1 \mu \mathrm{~F}, 20 \%$ ， 50 V | C－365－0．1 |
| C317 | Capacitor， $0.1 \mu \mathrm{~F}, 20 \%$ ， 50 V | C－365－0．1 |
| C318 | Capacitor，0．1 $\mathrm{F}, 20 \%$ ， 50 V | C－365－0．1 |
| C319 | Capacitor 0．1 $\mu \mathrm{F}, 20 \%$ ， 50 V | C－365－0．1 |
| C320 | Capacitor， $0.1 \mu \mathrm{~F}, 20 \%$ ， 50 V | C－365－0．1 |
| C321 | Capacitor， $0.1 \mu \mathrm{~F}, 20 \%$ ，50V | C－365－0．1 |
| C322 | Capacitor，0．1䂞，20\％，50V | C－365－0．1 |
| C323 | Capacitor，0．1还，20\％，50V | C－365－0．1 |
| C324 | Capacitor， $0.1 \mu \mathrm{~F}, 20 \%$ ， 50 V | C－365－0．1 |
| C325 | Capacitor， $0.1 \mu \mathrm{~F}, 20 \%$ ， 50 V | C－365－0．1 |
| C326 | Capacitor， $0.1 \mu \mathrm{~F}, 20 \%$ ， 50 V | C－365－0．1 |
| C327 | Capacitor， $0.1 \mu \mathrm{~F}, 20 \%, 50 \mathrm{~V}$ | C－365－0．1 |
| C328 | Capacitor， $0.1 \mu \mathrm{~F}, 20 \%$ ， 50 V | C－365－0．1 |
| C329 | Capacitor， $0.1 \mu \mathrm{~F}, 20 \%$ ， 50 V | C－365－0．1 |
| C330 | Capacitor， $0.1 \mu \mathrm{~F}, 20 \%$ ， 50 V | C－365－0．1 |
| C331 | Capacitor， $0.1 \mu \mathrm{~F}, 20 \%$ ， 0 V | C－365－0．1 |
| C332 | Capacitor， $0.1 \mu \mathrm{~F}, 20 \%$ ， 0 V | C－365－0．1 |
| C333 | Capacitor， $0.1 \mu \mathrm{~F}, 20 \%$ ， 50 V | C－365－0．1 |
| C334 | Capacitor，0．1 $\mu \mathrm{F}, 20 \%$ ，50V | C－365－0．1 |
| C335 | Capacitor， $10 \mu \mathrm{~F}, 25 \mathrm{~V}$ ，Aluminum Electrolytic | C－314－10 |
| C336 | Not Used |  |
| C337 | Not Used |  |
| C338 | Not Used |  |
| C339 | Not Used |  |
| C340 | Capacitor， $6800 \mu \mathrm{~F}, 25 \mathrm{~V}$ ，Aluminum Electrolytic | C－314－6800 |
| C341 | Capacitor， $470 \mu \mathrm{~F}, 50 \mathrm{~V}$ ，Aluminum Electrolytic | C－276－470 |
| C342 | Capacitor， $470 \mu \mathrm{~F}, 50 \mathrm{~V}$ ，Aluminum Electrolytic | C－276－470 |
| C343 | Capacitor， $2200 \mu \mathrm{~F}, 35 \mathrm{~V}$ ，Aluminum Electrolytic | C－309－2200 |
| C344 | Capacitor， $2200 \mu \mathrm{~F}, 35 \mathrm{~V}$ ，Aluminum Electrolytic | C－309－2200 |
| C345 | Capacitor， $4700 \mu \mathrm{~F}, 16 \mathrm{~V}$ ，Aluminum Electrolytic | C－313－4700 |
| C346 | Capacitor， $2200 \mu \mathrm{~F}, 16 \mathrm{~V}$ ，Aluminum Electrolytic | C－351－2200 |
| C347 | Capacitor， $10 \mu \mathrm{~F}, 25 \mathrm{~V}$ ，Aluminum Electrolytic | C－314－10 |
| C348 | Capacitor， $10 \mu \mathrm{~F}, 25 \mathrm{~V}$ ，Aluminum Electrolytic | C－314－10 |
| C349 | Capacitor， $10 \mu \mathrm{~F}, 25 \mathrm{~V}$ ，Aluminum Electrolytic | C－314－10 |
| C350 | Capacitor， $10 \mu \mathrm{~F}, 25 \mathrm{~V}$ ，Aluminum Electrolytic | C－314－10 |
| C351 | Capacitor， $10 \mu \mathrm{~F}, 25 \mathrm{~V}$ ，Aluminum Electrolytic | C－314－10 |

Table 8－3．Digital Board，Parts List（Cont．）

| Circuit Designation | Description | Keithley Part Number |
| :---: | :---: | :---: |
| C352 | Not Used |  |
| C353 | Capacitor， $0.01 \mu \mathrm{~F}, 500 \mathrm{~V}$ ，Ceramic Disc | C－22－0．1 |
| CR301 | Diode，Silicon， 1 N4148 | RF－28 |
| CR302 | Diode，Silicon， 1 N4148 | RF－28 |
| CR303 | Rectifier，Bridge，1A，100PIV | RF－52 |
| CR304 | Not Used |  |
| CR305 | Rectifier，Bridge，5A，50PIV，PE05 | RF－48 |
| CR306 | Rectifier，Bridge，14，100PIV | RF－52 |
| CR307 | Rectifier，Bridge，1A，100PIV | RF－52 |
| CR308 | Rectifier，Bridge，1A，100PIV | RF－52 |
| CR309 | Diode，1A，800PIV，1N4006 | RF－38 |
| F300 | Fuse，3AG， 0.5 A ，（ $180-220 \mathrm{~V}$ Operation） | FU－4 |
| F300 | Fuse，3AG，1A，（90－110V Operation） | FU－10 |
| F300 | Fuse，3AG， $3 / 8 \mathrm{~A}$ ，（210－250V Operation） | FU－18 |
| F300 | Fuse，3AG，3／4，（ $105-125 \mathrm{~V}$ Operation） | FU－19 |
| F300 | Fuse， $5 \mathrm{~mm}, 0.8 \mathrm{~A},(105-125 \mathrm{~V}$ ；requires $\mathrm{FH}-26$ Fuse Carrier） | FU－71 |
| F300 | Fuse，5mm，0．4A，（210－250V；requires FH－26 Fuse Carrier） | FU－80 |
| J1004 | Connector，BNC | CS－506 |
| J1005 | Connector，BNC | CS－506 |
| J1011 | Connector，IEEE－488 | CS－501 |
| J1012 | Connector，Modified | 740－309 |
| J1013 | Connector Pins | CS－288－2 |
| J1014 | Connector Pins | CS－389－9 |
| J1015 | Connector，Modified | 590－314－2 |
| J1016 | Connector，Modified | 590－314－1 |
| Q300 | Transistor，Power，PNP，2N5193 | TG－107 |
| Q301 | Transistor，Power，NPN，2N5190 | TG－108 |
| R301 | Resistor，100＠，5\％，1／4W，Composition | R－76－100 |
| R302 | Resistor，5100，5\％， $1 / 4 \mathrm{~W}$ ，Composition | R－76－510 |
| R303 | Resistor， 61.9 k ，1\％，1／8W | R－88－61．9K |
| R304 | Resistor， $1 \mathrm{M} \Omega, 5 \%$ ， $1 / 4 \mathrm{~W}$ ，Composition | R－76－1M |
| R305 | Resistor， $20 \mathrm{k} \Omega$ ， $1 \%$ ，1／8W | R－88－20k |
| R306 | Resistor， $3.3 \mathrm{kR}, 5 \%, 1 / 4 \mathrm{~W}$ ，Composition | R－76－3．3k |
| R307 | Resistor，3．3k』，5\％，1／4W，Composition | R－76－3．3k |
| R308 | Resistor， 3.3 kR ，5\％，1／4W，Composition | R－76－3．3k |
| R309 | Resistor，3．3k』，5\％，1／4W，Composition | R－76－3．3k |
| R310 | Resistor，3．3kR，5\％，1／4W，Composition | R－76－3．3k |
| R311 | Resistor，3．3k』，5\％，1／4W，Composition | R－76－3．3k |
| R312 | Resistor，3．3kn，5\％，1／4W，Composition | R－76－3．3k |
| R313 | Resistor， 3.3 kR ，5\％， $1 / 4 / \mathrm{W}$ ，Composition | R－76－3．3k |
| R314 | Resistor，360n， $5 \%$ ， $1 / 4 \mathrm{~W}$ ，Composition | R－76－360 |
| R315 | Resistor，470n， $5 \%$ ， $1 / 4 \mathrm{~W}$ ，Composition | R－76－470 |
| R316 | Resistor，360n，5\％，1／4W，Composition | R－76－360 |
| R317 | Resistor，4702，5\％，y／4W，Composition | R－76－470 |
| R318 | Resistor，3602，5\％， $1 / 4 \mathrm{~W}$ ，Composition | R－76－360 |
| R319 | Resistor，4708，5\％， $3 / 4 \mathrm{~W}$ ，Composition | R－76－470 |

## Table 8-3. Digital Board, Parts List (Cont.)

| Circuit <br> Designation | Description | Keithley Part Number |
| :---: | :---: | :---: |
| R320 | Resistor, 3608, 5\%, 1/4W, Composition | R-76-360 |
| R321 | Resistor, 4702, 5\%, 1/W, Composition | R-76-470 |
| R322 | Resistor, 360n, 5\%, 1/4W, Composition | R-76-360 |
| R323 | Resistor, 470n, 5\%, 1/4W, Composition | R-76-470 |
| R324 | Resistor, 3.3 k , $5 \%$, $1 / 4 \mathrm{~W}$, Composition | R-76-3.3k |
| R325 | Resistor, 1002, 5\%, Y/W, Composition | R-76-100 |
| R326 | Resistor, 3.3 kQ , 5\%, 1/4W, Composition | R-76-3.3k |
| R327 | Resistor, 3.3 k , , 5\%, $1 / 4 \mathrm{~W}$, Composition | R-76-3.3k |
| R328 | Resistor, 3.3 k , , 5\%, 1/4W, Composition | R-76-3.3k |
| R329 | Resistor, 3.3 k , , $5 \%$, 1/4W, Composition | R-76-3.3k |
| R330 | Resistor, $3.3 \mathrm{k} \Omega$, 5\%, 1/4W, Composition | R-76-3.3k |
| R331 | Resistor, $3.3 \mathrm{k} \Omega, 5 \%$, $1 / 4 \mathrm{~W}$, Composition | R-76-3.3k |
| R332 | Resistor, $3.3 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-3.3k |
| R333 | Resistor, $3.3 \mathrm{k} \Omega, 5 \%$, $1 / 4 \mathrm{~W}$, Composition | R-76-3.3k |
| R334 | Resistor, $3.3 \mathrm{k} \Omega, 5 \%$, $1 / 4 \mathrm{~W}$, Composition | R-76-3.3k |
| R335 | Resistor, $3.3 \mathrm{k} \Omega$, 5\%, 1/4W, Composition | R-76-3.3k |
| R336 | Resistor, $3.3 \mathrm{k} \Omega, 5 \%$, 1/4W, Composition | R-76-3.3k |
| R337 | Resistor, $3.3 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-3.3k |
| R338 | Resistor, $3.3 \mathrm{k} \Omega, 5 \%$, $1 / 4 \mathrm{~W}$, Composition | R76-3.3k |
| R339 | Resistor, 3.3 k , , 5\%, $1 / 4 \mathrm{~W}$, Composition | R-76-3.3k |
| R340 | Resistor, 3.3k@, 5\%, 1/4W, Composition | R-76-3.3k |
| R341 | Resistor, 3.3k@, 5\%, 1/4W, Composition | R-76-3.3k |
| R342 | Resistor, 3.3k@, 5\%, 1/4W, Composition | R-76-3.3k |
| R343 | Resistor, $3.3 \mathrm{k} \Omega, 5 \%$, 1/4W, Composition | R-76-3.3k |
| R344 | Resistor, 3.3k8, 5\%, 1/4W, Composition | R-76-3.3k |
| R345 | Resistor, $3.3 \mathrm{k} \Omega, 5 \%$, $1 / 4 \mathrm{~W}$, Composition | R-76-3.3k |
| R346 | Resistor, $3.3 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-3.3k |
| R347 | Resistor, 3.3ks, 5\%, $1 / 4 \mathrm{~W}$, Composition | R-76-3.3k |
| R348 | Resistor, $3.3 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-3.3k |
| R349 | Resistor, 3.3kn, 5\%, $1 / 4 \mathrm{~W}$, Composition | R-76-3.3k |
| R350 | Resistor, $3.3 \mathrm{k} \Omega, 5 \%$, $7 / 4 \mathrm{~W}$, Composition | R-76-3.3k |
| R351 | Resistor, $3.3 \mathrm{k} \Omega, 5 \%$, $1 / 4 \mathrm{~W}$, Composition | R76-3.3k |
| R352 | Resistor, $3.3 \mathrm{k} \Omega, 5 \%$, $1 / 4 \mathrm{~W}$, Composition | R-76-3.3k |
| R353 | Resistor, 3.3kn, 5\%, 1/4W, Composition | R-76-3.3k |
| R354 | Resistor, 3.3k』, 5\%, 1/4W, Composition | R-76-3.3k |
| R355 | Resistor, $3.3 \mathrm{k} \Omega, 5 \%$, $1 / 4 \mathrm{~W}$, Composition | R-76-3.3k |
| R356 | Resistor, $3.3 \mathrm{k} \Omega$, 5\%, $1 / 4 \mathrm{~W}$, Composition | R-76-3.3k |
| R357 | Resistor, $3.3 \mathrm{k} \Omega, 5 \%$, $1 / 4 \mathrm{~W}$, Composition | R-76-3.3k |
| R358 | Resistor, 62, $5 \%$, $1 / 4 \mathrm{~W}$, Composition | R-76-62k |
| R359 | Resistor, $62 \Omega, 5 \%$, 1/4W, Composition | R-76-62k |
| R360 | Resistor, 620, 5\%, 1/4W, Composition | R-76-62k |
| R361 | Resistor, $62 \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-62k |
| R362 | Resistor, 620, 5\%, 1/4W, Composition | R-76-62k |
| R363 | Resistor, $620,5 \%, 1 / 4 \mathrm{~W}, \mathrm{Composition}$ | R-76-62k |
| R364 | Resistor, 62n, 5\%, 1/4W, Composition | R-76-62k |
| R365 | Resistor, 620, 5\%, 1/4W, Composition | R-76-62k |
| R366 | Resistor, 62, 5\%, 1/4W, Composition | R-76-62k |
| R367 | Resistor, 620, 5\%, 1/4W, Composition | R-76-62k |
| R368 | Resistor, 620, 5\%, 1/4W, Composition | R-76-62k |
| R369 | Resistor, $620,5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-62k |
| R370 | Resistor, $62 \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-62k |

## Table 8-3. Digital Board, Parts List (Cont.)

| Circuit Designation | Description | Keithley <br> Paxt Number |
| :---: | :---: | :---: |
| R371 | Resistor, 62, $5 \%$, $1 / 4 \mathrm{~W}$, Composition | R-76-62k |
| R372 | Resistor, 62n,5\%, 1/4W, Composition | R.76-62k |
| R373 | Resistor, $620,5 \%, 1 / 4 \mathrm{~W}, \mathrm{Composition}$ | R-76-62k |
| R374 | Resistor, $62 \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-62k |
| R375 | Resistor, $620,5 \%, 1 / 4 \mathrm{~W}$, Composition | R.76-62k |
| R376 | Resistor, $62 \mathrm{n}, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-62k |
| R377 | Resistor, $620,5 \%, 1 / 4 \mathrm{~W}, \mathrm{Composition}$ | R-76-62k |
| R378 | Resistor, $62 \Omega, 5 \%, 1 / 4 \mathrm{~W}, \mathrm{Composition}$ | R-76-62k |
| R379 | Resistor, $62 \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-62k |
| R380 | Resistor, $62 \Omega, 5 \%, 1 / 4 \mathrm{~W}, \mathrm{Composition}$ | R-76-62k |
| R381 | Resistor, $62 \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-62k |
| R382 | Resistor, $620,5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-62k |
| R383 | Resistor, $620,5 \%$, 1/4W, Composition | R-76-62k |
| R384 | Resistor, $620,5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-62k |
| R385 | Resistor, $62 \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-62k |
| R386 | Resistor, $62 \Omega, 5 \%, 14 \mathrm{~W}$, Composition- | R-76-62k |
| R387 | Resistor, $620,5 \%, 1 / 4 \mathrm{~W}$, Composition | R.76-62k |
| R388 | Resistor, $620,5 \%, 1 / 4 \mathrm{~W}, \mathrm{Composition}$ | R-76-62k |
| R389 | Resistor, $62 \Omega, 5 \%, 1 / 4 \mathrm{~W}, \mathrm{Composition}$ | R-76-62k |
| R390 | Resistor, 3.3 kR , 5\%, $1 / 1 \mathrm{~W}$, Composition | R-76-3.3k |
| R391 | Resistor, 1000, 5\%, $1 / 4 \mathrm{~W}, \mathrm{Composition}$ | R-76-100k |
| R392 | Resistor, 220k, $5 \%$, $1 / 4 \mathrm{~W}$, Composition | R-76-220k |
| R393 | Resistor, $1 \mathrm{k} 2,5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-1k |
| R394 | Resistor, $1 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-1k |
| S300 | Switch, Off/On | SW-466 |
| S301 | Switch, Calibration Lock | SW-397 |
| S302 | Switch, Voltage Select | SW-318 |
| T300 | Transformer, Power, 105-125V, 210-250V | TR-226 |
| T300 | Transformer, Power, $90-110 \mathrm{~V}, 180-220 \mathrm{~V}$ | TR-229 |
| T301 | Transformer | TR-228 |
| U301 | IC, Quad 2-Input NOR Gate, 74HCTO2 | IC-510 |
| U302 | IC, Micropower Bipolar Monolithic, 8211 | IC-177 |
| U303 | IC, AND, OR Array, PAL16P8A | 590-802* |
| U304 | IC, Octal Bus Transceiver, 75160A | IC-298 |
| U305 | IC, 1-of-8 Decoder, $74 \mathrm{HCCTI38}$ | IC-398 |
| U306 | IC, ROM, $8 \mathrm{k} \times 8$ Bit, 2764 | 590-800** |
| U307 | IC, ROM, $64 \mathrm{k} \times 8$ Bit, 27256 | 590-801* |
| U308 | IC, 8k Byte Static CMOS, RAM, HM6264LP-15 | LSI-66 |
| U309 | IC, 8k Byte Static CMOS, RAM, HM6264LP-15 | LSI-66 |
| U310 | IC, Programmable E2ROM, 2816 | LSI-83 |
| U311 | IC, General Purpose Interface, 9914A | LSI-49 |
| U312 | IC, Octal Bus Transceiver, 75161A | IC-299 |
| U313 | IC, Versatile Interface Adapter (VIA), 6522A | LSI-45 |
| U314 | IC, Quad 2-Input OR Gate, 74HCT32 | IC-443 |
| U315 | IC, 8 -Bit Microprocessor ( 2 MHz ), 68B09 | LSI-65 |
| U316 | IC, Hex Inverter, 74 HCT 04 | IC-444 |
| U317 | IC, Opto-coupler, HCPL-2601 | 1C-239 |
| U318 | IC, CMOS, Octal D-Type Flip-Flop, 74HCI374 | IC-397 |

Table 8-3. Digital Board, Parts List (Cont.)

| Circuit <br> Designation | Description | Keithley Part Number |
| :---: | :---: | :---: |
| U319 | IC, CMOS, Octal D-Type Flip-Flop, 74HCT374 | IC-397 |
| U320 | IC, Optocoupler, HCPL-2601 | IC-239 |
| U321 | IC, 12-Stage Binary Counter, 4040B | IC-348 |
| U322 | IC, Optocoupler, HCPL-2601 | IC-239 |
| U323 | IC, CMOS Octal D-Type Flip-Flop, 74HCT374 | IC-397 |
| U324 | IC, CMOS Octal D-Type Flip-Flop, $74 \mathrm{HCT374}$ | IC-397 |
| U325 | IC, Optocoupler, HCPL-2601 | IC-239 |
| U326 | IC, Optocoupler, HCPL-2601 | IC-239 |
| U327 | IC, CMOS Octal D-Type Flip-Flop, 74HCT374 | IC-397 |
| U328 | IC, AND, OR Array, PAL16P8A | 590-803** |
| U329 | IC, CMOS Octal D-Type Flip-Flop, 74HCT374 | IC-397 |
| U330 | IC, 74LS273 | IC-263 |
| U331 | IC, 75157 | IC-429 |
| U332 | IC, 74 HCT 393 | IC-462 |
| U333 | IC, $16 \times 16$ Bit Parallel Multiplier, 7216 | LSI-71 |
| U334 | IC, Transistor Array, MPQ3906 | IC-396 |
| U335 | IC, Transistor Array, MPQ3906 | IC-396 |
| U336 | IC, Transistor Array, MPQ3906 | IC-396 |
| U337 | IC, Transistor Array, MPQ3906 | IC-396 |
| U338 | IC, Transistor Array, MPQ3906 | IC-396 |
| U339 | IC, Transistor Array, MPQ3906 | IC-396 |
| U340 | IC, Transistor Array, MPQ3906 | IC-396 |
| U341 | IC, Transistor Array, MPQ3906 | IC-396 |
| U342 | IC, 12-Stage Binary Counter, 74HC4040 | IC-407 |
| U343 | IC, Dual D-Type Flip-Flop, 74LS74 | IC-144 |
| VR300 | Regulator, IC, +5V, 7805 | IC-93 |
| VR301 | Regulator, IC, -5V, 7905 | IC-184 |
| VR302 | Regulator, IC, +15 V , 78M15CV | IC-194 |
| VR303 | Regulator, IC, $-15 \mathrm{~V}, \mathrm{MC} 7915 \mathrm{CT}$ | IC-174 |
| VR304 | Regulator, IC, $+5 \mathrm{~V}, 323$ | IC-240 |
| VR305 | Zener Diode, 30V, 1W, 1 N 4751 Zener Diode, 30V, 1W, 1N4751 | DZ-78 |
| W300 | Jumper | J-3 |

*Order same digits as present revision level marked on IC.


Figure 8-5. Digital Board, Bomponent Location Drawing, Dwg. No. 590-120


Figure 8-6. Digital Board, Schematic Diagram, Dwg. No. 590-126 (sheet 1 of 3)


Figure 8-6. Digital Board, Schematic Diagram, Dwg. No. 590-126 (sheet 2 of 3)


Figure 8-6. Digital Board, Schematic Diagram, Dwg. No. 590-126 (sheet 3 of 3)

Table $8-4.100 \mathrm{kHz}$ (5901) Module, Parts List

| Circuit <br> Designation | Description | Keithley Part Number |
| :---: | :---: | :---: |
| AT500 | IC, Optocoupler, CLM6500 | IC-440 |
| C500 | Not Used |  |
| C501 | Not Used |  |
| C502 | Capacitor, $1000 \mathrm{pF}, 100 \mathrm{~V}$, Ceramic | C-372-1000p |
| C503 | Capacitor, $1000 \mathrm{pF}, 100 \mathrm{~V}$, Ceramic | C-372-1000p |
| C504 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%, 50 \mathrm{~V}$ | C-365-0.1 |
| C505 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C506 | Capacitor, 22pF, 500 V , Ceramic Disc | C-22-22p |
| C507 | Capacitor, 1 1 F, 50V, Ceramic Film | C-237-1 |
| C508 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Metallized Polyester | C-350-1 |
| C509 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C510 | Capacitor, $0.01 \mu \mathrm{~F}, 50 \mathrm{~V}$, Metallized Polycarbonate | C-201-01 |
| C511 | Capacitor, 0.1 $\mu \mathrm{F}, 20 \%$, 50 V | C-365-0.1 |
| C512 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C513 | Capacitor, 1.5pF, 50V, Tubular Ceramic | C-282-1.5p |
| C514 | Capacitor, $0.1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Metallized Polycarbonate | C-201-0.1 |
| C515 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C516 | Capacitor, $10 \mu \mathrm{~F}, 25 \mathrm{~V}$, Aluminum Electrolytic | C-314-10 |
| C517 | Not Used |  |
| C518 | Not Used |  |
| C519 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C520 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C521 | Capacitor, $10 \mu \mathrm{~F}, 25 \mathrm{~V}$, Aluminum Electrolytic | C-314-10 |
| C522 | Not Used |  |
| C523 | Capacitor, $10 \mu \mathrm{~F}, 25 \mathrm{~V}$, Aluminum Electrolytic | C-314-10 |
| C524 | Not Used |  |
| C525 | Capacitor, 100pF | C-201-100p |
| C526 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C527 | Capacitor, Trimmer, 770pF | C-345 |
| C528 | Capacitor, 150pF, 100V, Ceramic | C-372-150p |
| C529 | Capacitor, Trimmer, 3-10pF | C-346 |
| C530 | Capacitor, 10pF, 100V, Ceramic | C-372-10p |
| C531 | Capacitor, 1.5pF, 50V, Tubular Ceramic | C-282-1.5p |
| C532 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C533 | Capacitor, $10 \mu \mathrm{~F}, 25 \mathrm{~V}$, Aluminum Electrolytic | C-314-10 |
| C534 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C535 | Capacitor, $10 \mu \mathrm{~F}, 25 \mathrm{~V}$, Aluminum Electrolytic | C-314-10 |
| C536 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C537 | Capacitor, 10pF, 500V Ceramic Disc | C-22-10p |
| C538 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C539 | Capacitor, 1000p, 100V, Ceramic | C-372-1000p |
| C540 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%, 50 \mathrm{~V}$ | C-365-0.1 |
| C541 | Capacitor, 15pF, 100V, Ceramic | C-372-15p |
| C542 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C543 | Capacitor, $1.5 \mathrm{pF}, 50 \mathrm{~V}$, Tubular Ceramic | C-282-1.5p |
| C544 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%, 50 \mathrm{~V}$ | C-365-0.1 |
| C545 | Capacitor, 15pF, 100V, Ceramic | C-372-15p |
| C546 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%, 50 \mathrm{~V}$ | C-365-0.1 |
| C547 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%, 50 \mathrm{~V}$ | C-365-0.1 |
| C548 | Capacitor, 1.5pF, 50V, Tubular Ceramic | C-282-1.5p |

Table 8-4. 100kHz (5901) Module, Parts List (Cont.)

| Circuit <br> Designation | Description | Keithley <br> Part Number |
| :---: | :---: | :---: |
| C549 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C550 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C551 | Capacitor, $0.01 \mu \mathrm{~F}, 500 \mathrm{~V}$, Ceramic Disc | C-22-0.01 |
| C552 | Capacitor, $0.01 \mu \mathrm{~F}, 500 \mathrm{~V}$, Ceramic Disc | C-22-0.01 |
| C553 | Capacitor, $0.022 \mu \mathrm{~F}, 100 \mathrm{~V}$ | C-371-0.022 |
| C554 | Capacitor, $0.033 \mu \mathrm{~F}, 100 \mathrm{~V}$ | C-371-0.033 |
| C555 | Capacitor, 100 pF , 500V, Ceramic Disc | C-22-100p |
| C556 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Metallized Polyester | C-350-1 |
| C557 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Metallized Polyester | C-350-1 |
| C558 | Capacitor, 100pF, 500 V , Ceramic Disc | C-22-100p |
| C559 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C560 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%, 50 \mathrm{~V}$ | C-365-0.1 |
| C561 | Not Used |  |
| C562 | Not Used |  |
| C563 | Not Used |  |
| C564 | Not Used |  |
| C565 | Not Used |  |
| C566 | Not Used |  |
| C567 | Capacitor, $0.01 \mu \mathrm{~F}, 500 \mathrm{~V}$, Ceramic Disc | C-22-0.01 |
| C568 | Capacitor, $0.01 \mu \mathrm{~F}, 500 \mathrm{~V}$, Ceramic Disc | C-22-0.01 |
| C569 | Not Used |  |
| C570 | Capacitor, $2.5 \mathrm{pF}, 50 \mathrm{~V}$, Tubular Ceramic | C-282-2.5p |
| C571 | Capacitor, $10 \mu \mathrm{~F}, 25 \mathrm{~V}$, Aluminum Electrolytic | C-314-10 |
| CR500 | Diode, Schottky Barrier, 1N5711 | RF-69 |
| CR501 | Diode, Schottky Barrier, 1N5711 | RF-69 |
| CR502 | Diode, Silicon, 1N4148 | RF-28 |
| CR503 | Diode, Silicon, 1N4148 | RF-28 |
| CR504 | Diode, Silicon, 1 N 4148 | RF-28 |
| CR505 | Diode, Silicon, 1 N4148 | RF-28 |
| CR506 | Diode, Silicon, 1N4148 | RF-28 |
| CR507 | Diode, Silicon, 1N4148 | RF-28 |
| CR508 | Diode, Silicon, 1N4148 | RF-28 |
| CR509 | Rectifier Bridge, 1A, 100PIV | RF-52 |
| CR510 | Not Used |  |
| CR511 | Not Used |  |
| CR512 | Diode, Silicon, 1N4148 | RF-28 |
| K500 | Relay | RL-65 |
| K501 | Relay | RL-65 |
| K502 | Relay | RL-95 |
| K503 | Relay | RL-48 |
| L500 | Choke | CH-24 |
| L501 | Choke | CH-23 |
| P1020 | Connector Housing | CS-534-9 |
| P1021 | Connector Housing | CS-534.7 |
| P1023 | Cable Assembly | CA-50-3 |
| P1024 | Cable Assembly | CA-50-1 |
| P1025 | Connector Housing | CS-534-2 |

Table 8－4．100kHz（5901）Module，Parts List（Cont．）

| Circuit Designation | Description | Keithley <br> Part Number |
| :---: | :---: | :---: |
| Q500 | Transistor，Silicon，NPN，2N3904 | TG－47 |
| Q501 | Transistor，Silicon，NPN，2N3904 | TG－47 |
| Q502 | Transistor，N－Channel JFET，2N4393 | TG－130 |
| Q503 | Transistor，N－Channel JFET，2N4393 | TG－130 |
| Q504 | Transistor，N－Channel JFET，2N4393 | TG－130 |
| Q505 | Transistor，N－Channel JFET，2N4393 | TG－130 |
| Q506 | Transistor，N－Channel JFET，2N4393 | TG－130 |
| Q507 | Transistor，N－Channel JFET，2N4393 | TG－130 |
| Q508 | Transistor，N－Channel JFET，2N4393 | TG－130 |
| Q509 | Transistor，N－Channel JFET，2N4393 | TG－130 |
| Q510 | Transistor，Matched Dual－channel JFET，DN5566 | TG－188 |
| Q511 | Not Used |  |
| Q512 | Transistor，Silicon，NPN，2N3904 | TG－47 |
| Q513 | Transistor，Silicon，NPN，2N3904 | TG－47 |
| R500 | Resistor，270n，5\％，1／4W，Composition | R－76－270 |
| R501 | Resistor，2700，5\％，1／4W，Composition | R－76－270 |
| R502 | Resistor，270＠，5\％，1／W，Composition | R－76－270 |
| R503 | Resistor， $270 \Omega, 5 \%, 1 / 4 \mathrm{~W}$ ，Composition | R－76－270 |
| R504 | Resistor， $1.07 \mathrm{k} \Omega, 1 \%, 1 / 8 \mathrm{~W}$ | R－88－1．07k |
| R505 | Resistor， $2.32 \mathrm{k} \Omega, 1 \%, 1 / 3 \mathrm{~W}$ | R－88－2．32k |
| R506 | Resistor，2ka，1\％，1／8 W | R－88－2k |
| R507 | Resistor，499，1\％，${ }^{1 / \mathrm{s}} \mathrm{W}$ | R－88－499 |
| R508 | Resistor， $510 \Omega, 5 \%, 1 / 4 \mathrm{~W}$ ，Composition | R－76－510 |
| R509 | Resistor， $4.99 \mathrm{k} \Omega, 1 \%, 1 / \mathrm{s} \mathrm{W}$ | R－88－4．99k |
| R510 | Resistor， $10 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}$ ，Composition | R－76－10k |
| R511 | Resistor，100』，5\％，\％W，Composition | R－76－100 |
| R512 | Resistor， $856 \Omega, 0.1 \%, 1 / 20$ W，Metal Film | R－263－856 |
| R513 | Potentiometer， $50 \mathrm{~S}, 1 / 2 \mathrm{~W}$ ，Cermet | RP－97－50 |
| R514 | Resistor，5102， $0.1 \%, 1 / 10 \mathrm{~W}$ ，Metal Film | R－263－510 |
| R515 | Potentiometer，5000， $1 / 2 \mathrm{~W}$ ，Cermet | RP－97－500 |
| R516 | Resistor，20k』，0．1\％， $1 / 10 \mathrm{~W}$ ，Metal Film | R－263－20k |
| R517 | Resistor，100k $\Omega, 5 \%, 1 / 4 \mathrm{~W}, \mathrm{Composition}$ | R $76-100 \mathrm{k}$ |
| R518 | Resistor， $4.32 \mathrm{k} \mathrm{l}^{\prime}, 1 \%, 1 / \mathrm{sW}$ | R－88－4．32k |
| R519 | Resistor，470n， $5 \%$ ， $1 / 4 \mathrm{~W}$ ，Composition | R－76－470 |
| R520 | Resistor， $79.6 \mathrm{k} \Omega, 0.1 \%, 1 / 10 \mathrm{~W}$ ，Metal Film | R－263－79．6k |
| R521 | Potentiometer，2000， $1 / 2 \mathrm{~W}$ ，Cermet | RP－97－200 |
| R522 | Resistor， $8.75 \mathrm{k} \Omega, 0.1 \%, 1 / 10 \mathrm{~W}$ ，Metal Film | R－263－8．75k |
| R523 | Potentiometer，20， $1 / 2 \mathrm{~W}$ ，Cermet | RP－97－20 |
| R524 | Resistor，7940， $0.1 \%, 1 / 10 \mathrm{~W}$, Metal Film | R－263－794 |
| R525 | Resistor，100』， $5 \%, 1 / 2 \mathrm{~W}$ ，Composition | R－76－100 |
| R526 | Resistor， 1.5 k ， $5 \%, 1 / 2 \mathrm{~W}, \mathrm{Composition}$ | R－76－1．5k |
| R527 |  | R－76－1．5k |
| R528 | Resistor， $1.5 \mathrm{k} \Omega, 5 \%, 1 / 2 \mathrm{~W}$ ，Composition | R－76－1．5k |
| R529 | Resistor， $100 \Omega, 5 \%, 1 / 2 \mathrm{~W}$ ，Composition | R－76－100 |
| R530 | Resistor， $1.5 \mathrm{k} \Omega, 0.1 \%, 1 / 10 \mathrm{~W}$ ，Metal Film | R－263－1．5k |
| R531 | Resistor，6．19k＠，0．1\％， $1 / 10 \mathrm{~W}$ ，Metal Film | R－263－6．19k |
| R532 | Resistor， 1.67 k ， $0.1 \%, 1 / 10 \mathrm{~W}$ ，Metal Film | R－263－1．67k |
| R533 | Resistor，10k ${ }^{\text {d }}$ ， $0.1 \%$ ， $1 / 10$ W，Metal Film | R－263－10k |
| R534 | Resistor， $10 \mathrm{k} \Omega, 0.1 \%,{ }^{1 / 10} \mathrm{~W}$ ，Metal Film | R－263－10k |
| R535 | Resistor， $1.67 \mathrm{k} \Omega, 0.1 \%, 1 / 10 \mathrm{~W}$ ，Metal Film | R－263－1．67k |

## Table 8-4. 100kHz (5901) Module, Parts List (Cont.)

| Circuit Designation | Description | Keithley Part Number |
| :---: | :---: | :---: |
| R536 | Resistor, $10 \mathrm{k} \Omega, 0.1 \%, 1 / 10$, Metal Film | R-263-10k |
| R537 | Resistor, $10 \mathrm{k} \Omega, 0.1 \%, 11_{10} \mathrm{~W}$, Metal Film | R-263-10k |
| R538 | Resistor, $10 \mathrm{k} \Omega, 0.1 \%, 1 / 10$, Metal Film | R-263-10k |
| R539 | Resistor, 10k $, 0.1 \%, 1_{10}$ W, Metal Film | R-263-10k |
| R540 | Resistor, $10 \mathrm{k} \Omega, 0.1 \%, 1 / 10 \mathrm{~W}$, Metal Film | R-263-10k |
| R541 | Resistor, $10 \mathrm{M} \Omega, 10 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-10M |
| R542 | Resistor, 6.8M0, 5\%, $1 / 4 \mathrm{~W}$, Composition | R76-6.8M |
| R543 | Resistor, $6.19 \mathrm{k} \Omega, 0.1 \%$, ${ }^{1 / 10}$ W, Metal Film | R-263-6.19k |
| R544 | Resistor, 4.3 k , $5 \%$, $1 / 4 \mathrm{~W}$, Composition | R-76-4.3k |
| R545 | Potentiometer, $20 \mathrm{k} \Omega, 1 / 2 \mathrm{~W}$, Cermet | RP-97-20k |
| R546 | Potentiometer, $20 \mathrm{k} \Omega, 1 / 2 \mathrm{~W}$, Cermet | RP-97-20k |
| R547 | Potentiometer, 200, 1/2W, Cermet | RP-97-200 |
| R548 | Resistor, $4.3 \mathrm{k} \Omega, 5 \%$, $1 / 4 \mathrm{~W}$, Composition | R-76-4.3k |
| R549 | Resistor, $1 \mathrm{k} \Omega, 5 \%$, $1 / 4 \mathrm{~W}$, Composition | R-76-1k |
| R550 | Resistor, $1 \mathrm{k} \Omega, 5 \%$, $1 / 4 \mathrm{~W}$, Composition | R-76-1k |
| R551 | Not Used |  |
| R552 | Not Used |  |
| R553 | Resistor, $47 \mathrm{k} \Omega, 5 \%$, $1 / 4 \mathrm{~W}$, Composition | R-76-47k |
| R554 | Resistor, selected with VR500 | 5901-600 |
| R555 | Not Used | --- -- ..... |
| R556 | Not Used |  |
| R557 | Not Used |  |
| R558 | Not Used |  |
| R559 | Not Used |  |
| R560 | Resistor, $4.7 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R $76-4.7 \mathrm{k}$ |
| R561 | Resistor, $4.7 \mathrm{k} \mathrm{\Omega}, 5 \%$, $1 / 4 \mathrm{~W}$, Composition | R-76-4.7k |
| R562 | Resistor, 470@, 5\%, $1 / 4 \mathrm{~W}$, Composition | R-76-470 |
| R563 | Resistor, $4.7 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R $76-4.7 \mathrm{k}$ |
| R564 | Resistor, 8662, 1\%, 1/s W | R-88-866 |
| R565 | Not Used |  |
| R566 | Not Used |  |
| R567 | Not Used |  |
| R568 | Not Used |  |
| R569 | Resistor, $100 \mathrm{k} \Omega, 10 \%$, $1 / 2 \mathrm{~W}$, Composition | R-1-100k |
| R570 | Resistor, 3.9n, 10\%, 1/2W, Composition | R-1-3.9 |
| T500 | Transformer | TR-221 |
| T501 | Transformer | TR-222 |
| T502 | Transformer | TR-220 |
| U500 | Not Used |  |
| U501 | Not Used |  |
| U502 | IC, Quad 2-Input NOR Gate, 74F02 | IC-435 |
| U503 | Not Used |  |
| U504 | IC, Dual D Edge Triggered Flip-Flop, 74 F74 | IC-446 |
| U505 | IC, Dual D Edeg Triggered Flip-Flop, 74 F74 | IC-446 |
| U506 | IC, Hex Inverter, 74F04 | IC-436 |
| U507 | IC, Quad 2-Input NAND Buffer, 74F38 | IC-434 |
| U508 | IC, Very Wide Band Operational Amplifier, HA2625 | IC-439 |
| U509 | IC, Very Wide Band Operational Amplifier, HA2625 | IC-439 |
| U510 | IC, Bi-FET Operational Amplifier, AD542 | IC-165 |

Table 8-4. 100kHz (5901) Module, Parts List (Cont.)

| Circuit <br> Designation | Description | Keithley <br> Part Number |
| :--- | :--- | :--- |
|  | U511 | IC, Very Wide Band Operational Amplifier, HA2625 |
| U512 | IC, Very Wide Band Operational Amplifier, HA2625 | IC-439 |
| U513 | IC, Very Wide Band Operational Amplifier, HA2625 | IC-439 |
| U514 | IC, Very Wide Band Operational Amplifier, HA2625 | IC-439 |
| U515 | IC, Bi-FET Operational Amplifier, LF442A | IC-439 |
| U516 | IC, Wideband Dual JFET Operational Amplifier, LF353N | IC-410 |
| U517 | IC, Bi-FET Operational Amplifier, LF442A | IC-246 |
| U518 | IC, Voltage Regalator, -5V, LM320LZ-5 | IC-410 |
| VR500 | Zener Diode, Selected with R554 | $5901-600$ |
| W500 | Connector Pin | CS-339-3 |
| W500 | Connector Pin Jumper | CS-476 |



Figure 8-7. Model 5901 (100kHz), Component Location Drawing, Dwg. No. 5901-100


Figure 8-8. Model 5901 (100kHz), Schematic Diagram, Dwg. No. 5901-106

Table 8-5. 1MHz (5902) Module, Parts List

| Circuit <br> Designation | Description | Keithley Part Number |
| :---: | :---: | :---: |
| AT601 | IC, Optocoupler, 6500 | IC-440 |
| C601 | Capacitor, 100pF, 500V, Mica | C-209-100p |
| C602 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C603 | Capacitor, 100pF, 500V, Mica | C-209-100p |
| C604 | Capacitor, 1 $\mu$ F, 50V, Ceramic Film | C-237-1 |
| C605 | Capacitor, $0.033 \mu \mathrm{~F}, 100 \mathrm{~V}$ | C-371-033 |
| C606 | Not Used |  |
| C607 | Capacitor, $1 \mu \mathrm{~F}, 10 \%$, 200V, Metallized Polypropylene | C-357-1 |
| C608 | Capacitor, $0.01 \mu \mathrm{~F}, 500 \mathrm{~V}$, Ceramic Disc | C-22-0.01 |
| C609 | Capacitor, $0.01 \mu \mathrm{~F}, 500 \mathrm{~V}$, Ceramic Disc | C-22-0.01 |
| C610 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C611 | Capacitor, $0.1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Metallized Polycarbonate | C-201-0.1 |
| C612 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%, 50 \mathrm{~V}$ | C-365-0.1 |
| C613 | Capacitor, $0.022 \mu \mathrm{~F}, 100 \mathrm{~V}$ | C-371-022 |
| C614 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C615 | Capacitor, $2.5 \mathrm{pF}, 50 \mathrm{~V}$, Tubular Ceramic | C-282-2.5p |
| C616 | Capacitor, 2200pF, Ceramic Disc | C-64-2200p |
| C617 | Not Used |  |
| C618 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50V | C-365-0.1 |
| C619 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 00 V | C-365-0.1 |
| C620 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C621 | Not Used |  |
| C622 | Capacitor, $1 \mu$ F, 50V, Ceramic Film | C-237-1 |
| C623 | Not Used |  |
| C624 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C625 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C626 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C627 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C628 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C629 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C630 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C631 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Metallized Polyester | C-350-1 |
| C632 | Capacitor, $0.01 \mu \mathrm{~F}, 500 \mathrm{~V}$, Ceramic Disc | C-22-0.01 |
| C633 | Capacitor, $0.022 \mu \mathrm{~F}, 100 \mathrm{~V}$ | C-371-0.022 |
| C634 | Capacitor, 15pF, Ceramic Disc | C-64-15p |
| C635 | Capacitor, 100 pF , Ceramic Disc | C-64-100p |
| C636 | Capacitor, $1 \mu \mathrm{~F}$, 50V, Metallized Polyester | C-350-1 |
| C637 | Capacitor, 15pF, Ceramic Disc | C-64-15p |
| C638 | Capacitor, 0.01 $\mathrm{F}^{\text {, 500V, Ceramic Disc }}$ | C-22-0.01 |
| C639 | Capacitor, 100 pF , Ceramic Disc | C-64-100p |
| C640 | Capacitor, $0.033 \mu \mathrm{~F}, 100 \mathrm{~V}$ | C-371-0.033 |
| C641 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C642 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C643 | Capacitor, 270 pF , EMI Suppression Filter | C-386-270p |
| C644 | Capacitor, $2.5 \mathrm{pF}, 50 \mathrm{~V}$, Tubular Ceramic | C-282-2.5p |
| C645 | Capacitor, 2200 pF , Ceramic Disc | C-64-2200p |
| C646 | Capacitor, 270 pF , EMI Suppression Filter | C-386-270p |
| C647 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C648 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1. |
| C649 | Capacitor, $0.01 \mu \mathrm{~F}, 500 \mathrm{~V}$, Ceramic Disc | C-22-0.01 |

## Table 8-5. 1 MHz (5902) Module, Parts List (Cont.)

| Circuit Designation | Description | Keithley <br> Part Number |
| :---: | :---: | :---: |
| C650 | Capacitor, 1000pF, Ceramic Disc | C-64-1000p |
| C651 | Capacitor, 1000pF, Ceramic Disc | C-64-1000p |
| C652 | Capacitor, $0.01 \mu \mathrm{~F}, 500 \mathrm{~V}$, Ceramic Disc | C-22-0.01 |
| C653 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C654 | Capacitor, 1 $\mu \mathrm{F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C655 | Capacitor, 1 $1 \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C656 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C657 | Capacitor, $0.01 \mu \mathrm{~F}, 500 \mathrm{~V}$, Ceramic Disc | C-22-0.01 |
| C658 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C659 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 00 V | C-365-0.1 |
| C660 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C661 | Capacitor, 100pF, 500V, Mica | C-209-100p |
| C662 | Capacitor, $0.01 \mu \mathrm{~F}, 500 \mathrm{~V}$, Ceramic Disc | C-22-0.01 |
| C663 | Capacitor, $1 \mu \mathrm{E}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C664 | Capacitor, 1800pF, 500 V , Mica | C-209-1800p |
| C665 | Capacitor, 1 1 E, 50V, Ceramic Film | C-237-1 |
| C666 | Capacitor, 270 pF , EMI Suppression Filter | C-386-270p |
| C667 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C668 | Capacitor, 33pF, Ceramic Disc | C-64-33p |
| C669 | Capacitor, 2200pF, Ceramic Disc | C-64-2200p |
| C670 | Capacitor, 100 pF , Ceramic Disc | C-64-100p |
| C671 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C672 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%, 50 \mathrm{~V}$ | C-365-0.1 |
| C673 | Capacitor, $0.01 \mu \mathrm{~F}, 500 \mathrm{~V}$, Ceramic Disc | C-22-0.01 |
| C674 | Capacitor, 1000 pF , Ceramic Disc | C-64-1000p |
| C675 | Caapcitor, 1000pF, Ceramic Disc | C-64-1000p |
| C676 | Capacitor, $0.01 \mu \mathrm{~F}, 500 \mathrm{~V}$, Ceramic Disc | C-22-0.01 |
| C677 | Capacitor, $0.1 \mu \mathrm{~F}, 20 \%$, 50 V | C-365-0.1 |
| C678 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C679 | Capacitor, 270pF, EMI Suppression Filter | C-386-270p |
| CR601 | Diode, Silicon, 1N4148 | RF-28 |
| CR602 | Diode, Schottky Barrier, 1N5711 | RF-69 |
| CR603 | Rectifier, Bridge, 1A, 100PIV | RF-52 |
| CR604 | Diode, Silicon, 1N4148 | RF-28 |
| CR605 | Diode, Silicon, 1N4148 | RF-28 |
| CR606 | Diode, Silicon, 1N4148 | RF-28 |
| CR607 | Diode, Silicon, 1N4148 | RF-28 |
| CR608 | Diode, Silicon, 1N4148 | RF-28 |
| K601 | Relay | RL-102 |
| K602 | Relay | RL-102 |
| K603 | Relay | RL-102 |
| K604 | Relay | RL-102 |
| K605 | Relay | RL-102 |
| K606 | Realy | RL-95 |
| K607 | Relay | RL-101 |
| L601 | Choke | CH-26-220 |
| L602 | Choke | $\mathrm{CH}-33$ |
| L603 | Choke | CH-33 |

## Table 8-5. 1MHz (5902) Module, Parts List

| Circuit <br> Designation | Description | Keithley Part Number |
| :---: | :---: | :---: |
| L604 | Choke | CH-33 |
| $L 605$ | Choke | CH-33 |
| L606 | Choke | CH-33 |
| L607 | Choke | CH-33 |
| $L 608$ | Choke | CH-33 |
| L609 | Choke | CH-33 |
| L610 | Choke | CH-33 |
| $L 611$ | Choke | CH-33 |
| 1612 | Choke | CH-33 |
| L613 | Choke | CH-26-220 |
| L614 | Choke | CH-33 |
| L615 | Choke | CH-33 |
| L616 | Choke | CH-33 |
| L617 | Choke | CH-26-15 |
| L618 | Choke | CH-33 |
| P1026 | Connector | CS-534-10 |
| P1027 | Connector | CS-534-7 |
| P1029 | Cable Assembly, $50 \Omega$ | CA-50-2 |
| P1030 | Cable Assembly, 502 | CA-50-1 |
| P1031 | Connector | CS-534-2 |
| P1034 | Cable Assembly, 50, | CA-50-3 |
| Q601 | Transistor, Silicon, NPN, 2N3904 | TG-47 |
| Q602 | Transistor, Silicon, NPN, 2N3904 | TG-47 |
| Q603 | Transistor, Silicon, NPN, 2N3904 | TG-47 |
| Q604 | Transistor, N-Channel JFET, 2N4393 | TG-130 |
| Q605 | Transistor, N-Channel JFET, 2N4393 | TG-130 |
| Q606 | Transistor, N-Channel JFET, 2N4393 | TG-130 |
| Q607 | Transistor, N-Channel JFET, 2N4393 | TG-130 |
| Q608 | Transistor, N-Channel JFET, 2N4393 | TG-130 |
| Q609 | Transistor, N -Channel - $\mathrm{FEET}, 2 \mathrm{~N} 4393$ | TG-130 |
| Q610 | Transistor, N-Channel JFET, 2N4393 | TG-130 |
| Q611 | Transistor, N-Channel JFET, 2 N4393 | TG-130 |
| R601 | Not Used |  |
| R602 | Resistor, 2708, 5\%, 1/4W, Composition | R76-270 |
| R603 | Resistor, 270, $5 \%$, 1/4 W, Composition | R76-270 |
| R604 | Resistor, $270 \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R76-270 |
| R605 | Resistor, 2708, $5 \%$, 1/4W, Composition | R-76-270 |
| R606 | Resistor, 866n, 1\%, 1/8W | R-88-866 |
| R607 | Resistor, $2 \mathrm{k} \Omega, 1 \%, 1 / 8 \mathrm{~W}$ | R-88-2k |
| R608 | Resistor, $1.07 \mathrm{k} \Omega, 1 \%,{ }^{1} / \mathrm{s} \mathrm{W}$ | R-88-1.07 ${ }^{-}$ |
| R609 | Resistor, $2.32 \mathrm{k} \Omega, 1 \%, 1 / \mathrm{W}$ | R-88-2.32k |
| R610 | Resistor, 499, 1\%, 1/8W | R-88-499 |
| R611 | Resistor, 4702, $5 \%$, $1 / 4 \mathrm{~W}$, Composition | R-76-470 |
| R612 | Resistor, 390, $5 \%$, 1/4W, Composition | R-76-390 |
| R613 | Resistor, $1.5 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-1.5k |
| R614 | Resistor, $1 \mathrm{k} \Omega, 5 \%$, $1 / 4 \mathrm{~W}$, Composition | R-76-1k |
| R615 | Resistor, 4.59 k , , 0.1\%, ${ }^{1} /{ }_{10} \mathrm{~W}$, Metal Film | R-263-4.59k |
| R616 | Resistor, $500 \Omega, 0.1 \%,{ }^{1} 10 \mathrm{~W}$, Metal Film | R-263-500 |

## Table 8－5． $\mathbf{1 M H z}$（5902）Module，Parts List（Cont．）

| Circuit Designation | Description | Keithley Part Number |
| :---: | :---: | :---: |
| R617 | Resistor，1000，1\％，1／s W | R－88－100 |
| R618 | Resistor， $1008,1 \%, 1 / 8 \mathrm{~W}$ | R－88－100 |
| R619 | Resistor， $1 \mathrm{k} \Omega, 1 \%$ ， $1 / \mathrm{s}$ W | R－88－1k |
| R620 | Potentiometer，200， $1 / 2 \mathrm{~W}, 25$ Turn Cermet | RP－104－200 |
| R621 | Resistor，1．1k』，1\％， $1 / 8 \mathrm{~s}$ W | R－88－1．1k |
| R622 | Resistor， $4.42 \mathrm{k} \Omega, 1 \%, 1 / 3 \mathrm{~W}$ | R－88－4．42k |
| R623 | Resistor， $3.90,10 \%$ ， $1 / 2 \mathrm{~W}$ ，Composition | R－1－3．9 |
| R624 | Resistor， $0.22 \Omega, 5 \%, 1 / 3 \mathrm{~W}$ ，Metal Film | R－346－0．22 |
| R625 | Resistor， $0.22 \Omega, 5 \%, 1 / 3 \mathrm{~W}$ ，Metal Film | R－346－0．22 |
| R626 | Resistor，0．22，5\％，1／3W，Metal Film | R－346－0．22 |
| R627 | Resistor， $100 \mathrm{k} \mathrm{\Omega}, 10 \%$ ， $1 / 2 \mathrm{~W}$ ，Composition | R－1－100k |
| R628 | Resistor， $1 \mathrm{k} \Omega, 5 \%$ ， $1 / 4 \mathrm{~W}$ ，Composition | R－76－1k |
| R629 | Resistor， $8.25 \mathrm{k} \Omega, 1 \%, 1 / 8 \mathrm{~W}$ | R－88－8．25k |
| R630 | Resistor， $10 \mathrm{k} \Omega, 5 \%$ ， $1 / 4 \mathrm{~W}$ ，Composition | R－76－10k |
| R631 | Resistor， $100 \mathrm{k} \Omega, 5 \%, 1 / \mathrm{W}$ ，Composition | R－76－100k |
| R632 | Resistor， $10 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}$ ，Composition | R－76－10k |
| R633 | Resistor，13k＠， $0.1 \%, 1 / 10 \mathrm{~W}$ ，Metal Film | R－263－13k |
| R634 | Potentiometer，5000， $1 / 2 \mathrm{~W}$ ，Cermet | RP－97－500 |
| R635 | Resistor，4708， $5 \%, 1 / 4 \mathrm{~W}$ ，Composition | R－76－470 |
| R636 | Resistor，4708，5\％， $1 / 4 \mathrm{~W}$ ，Composition | R－76－470 |
| R637 | Resistor， $10 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}$ ，Composition | R－76－10k |
| R638 | Resistor， $10 \mathrm{k} \boldsymbol{2}, 5 \%$ ， $1 / 4 \mathrm{~W}$ ，Composition | R76－10k |
| R639 | Resistor，20k＠，5\％，1／4W，Composition | R－76－20k |
| R640 | Resistor， $22 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}, \mathrm{Composition}$ | R－76－22k |
| R641 | Resistor，4700， $5 \%, 1 / 4 \mathrm{~W}$ ，Composition | R－76－470k |
| R642 | Resistor， $1 \mathrm{k} \Omega, 5 \%$ ， $1 / 1 \mathrm{~W}$ ，Composition | R－76－1k |
| R643 | Resistor，1k ${ }^{\text {，}}$ ， $5 \%, 1 / 4 \mathrm{~W}, \mathrm{Composition}$ | R－76－1k |
| R644 | Resistor，4．3k』，5\％，1／4W，Composition | R－76－4．3k |
| R 645 | Resistor，10k ${ }^{\text {a }}$ ，0．1\％，${ }^{1 / 10 \mathrm{~W}}$ ，Metal Film | R－263－10k |
| R646 | Potentiometer， $20 \mathrm{k} \Omega, 1 / 2 \mathrm{~W}$ ，Cermet | RP－97－20k |
| R647 | Resistor， 3.9 M ，, $5 \%$ ，1／4W，Composition | R－76－3．9M |
| R 648 | Potentiometer， $20 \mathrm{k} \Omega$ ， $1 / 2 \mathrm{~W}$ ，Cermet | RP－97－20k |
| R649 |  |  |
| R650 | Resistor， $4.3 \mathrm{kQ}, 5 \%, 1 / \mathrm{W}, \mathrm{Composition}$ Potentiometer， $200 \Omega, 1 / 2 \mathrm{~W}$, Cermet | R－76－97．300 |
| R652 | Resistor， $6.19 \mathrm{k} \Omega, 0.1 \%, 1 / 10 \mathrm{~W}$ ，Metal Film | R－263－6．19k |
| R653 | Resistor， $10 \mathrm{k} \Omega, 0.1 \%, 1 / 10 \mathrm{~W}$ ，Metal Film | R－263－10k |
| R654 | Resistor，10k ${ }^{\text {d }}$ ，0．1\％， $1_{10}$ W，Metal Film | R－263－10k |
| R655 | Resistor，10k』， $0.1 \%, 1 / 10$ W，Metal Film | R－263－10k |
| R656 | Resistor，10kn， $0.1 \%, 1 / 10 \mathrm{~W}$ ，Metal Film | R－263－10k |
| R657 | Resistor， $1 \mathrm{k} \Omega, 5 \%$ ， $1 / 4 \mathrm{~W}$ ，Composition | R－76－1k |
| R658 | Resistor， $10 \mathrm{M} \Omega, 10 \%$ ， $1 / 4 \mathrm{~W}, \mathrm{Composition}$ | R $76-10 \mathrm{M}$ |
| R659 | Resistor， $10 \mathrm{k} \Omega, 0.1 \%, 1 / 20 \mathrm{~W}$ ，Metal Film | R－263－10k |
| R660 | Resistor， $1.005 \mathrm{k} \Omega, 0.1 \%, 1 /{ }_{10}$ W，Metal Film | R－263－1．005k |
| R661 | Resistor，1008， $0.1 \%, 1 / 10$ W，Metal Film | R－263－100 |
| R662 | Resistor， $1.005 \mathrm{k} \Omega, 0.1 \%, 1 / 10 \mathrm{~W}$ ，Metal Film | R－263－1．005k |
| R663 | Potentiometer，2000， $1 / 2 \mathrm{~W}, 25$ Turn Cermet | RP－104－200 |
| R664 | Resistor，1．33k ${ }^{\text {a }}$ ，1\％， $1 / \mathrm{s}$ W | R－88－1．33k |
| R665 | Resistor，47kn，5\％，1／4W，Composition | R－76－47k |
| R666 | Resistor， $47 \mathrm{k} \Omega, 5 \%, 1 / 4 \mathrm{~W}$ ，Composition | R－76－47k |
| R667 | Resistor，7500， $5 \%, 1 / 4 \mathrm{~W}$ ，Composition | R－76－750 |

## Table 8-5. TMHz (5902) Module, Parts List (Cont.)

| Circuit Designation | Description | Keithley <br> Part Number |
| :---: | :---: | :---: |
| R668 | Resistor, 750n, 5\%, 1/4W, Composition | R-76-750 |
| R669 | Potentiometer, 2008 | RP-104-200 |
| R670 | Resistor, 634, 1\%, 1/sW | R-88-634 |
| R671 | Resistor, $47 \mathrm{k} \mathbf{2}$, 5\%, 1/4W, Composition | R-76-47k |
| R672 | Resistor, 47k』, 5\%, $1 / 4 \mathrm{~W}$, Composition | R-76-47k |
| R673 | Resistor, 1500, 5\%, 1/4W, Composition | R-76-150 |
| R674 | Resistor, 54.9n, $1 \%, 1 / 3 \mathrm{~W}$ | R-88-54.9 |
| R675 | Potentiometer, 100, $1 / 2 \mathrm{~W}, 25$ Turn Cermet | RP-104-100 |
| R676 | Resistor, 464, 1\%, $1 / \mathrm{sW}$ | R-88-464 |
| R677 | Resistor, $4.78 .5 \%, 1 / 4 \mathrm{~W}$, Composition | R.76-4.7 |
| R678 | Resistor, 49.98, $1 \%, 1 / 8 \mathrm{~W}$ | R-88-49.9 |
| R679 | Resistor, 4.32 k , 1\%, 1/s W | R-88-4.32k |
| R680 | Resistor, 845@, 1\%, $1 / \mathrm{s}$ W | R-88-845 |
| R681 | Potentiometer, 200, ${ }^{1 / 2} \mathrm{~W}, 25$ Turn Cermet | RP-104-200 |
| R682 | Resistor, 620,5\%, $1 / 4 \mathrm{~W}$, Composition | R-76-62 |
| T601 | Transformer | TR-224 |
| T602 | Transformer | TR-225 |
| T603 | Transformer | TR-225 |
| T604 | Transformer | TR-246 |
| T605 | Transformer | TR-244 |
| U601 | IC, Hex Inverter, 74F04 | IC-436 |
| U602 | IC, Quad 2-Input NOR Gate, 74F02 | IC-435 |
| U603 | IC, Dual D Edge Triggered Flip-Flop, 74F74 | IC-446 |
| U604 | IC, Dual D Edge Triggered Flip-Flop, 74F74 | IC-446 |
| U605 | IC, Quad 2-Input NAND Buffer, 74F38 | IC-434 |
| U606 | IC, Very Wide Band Operational Amplifier, 2625 | IC-439 |
| U607 | Operational Amplifier, KI590 (see Table 8-6 for parts) |  |
| U608 | IC, Bi-FET Operational Amplifier, AD542 | IC-165 |
| U609 | IC, Very High Slew Rate Operational Amplifier, 2539 | IC-512 |
| U610 | IC, Video Amplifier, NE592 | IC-511 |
| U611 | IC, Video Amplifier, NE592 | IC-511 |
| U612 | IC, Very High Slew Rate Operational Amplifier, 2539 | IC-512 |
| U613 | IC, Darlington Transistor Array, 2003A | IC-206 |
| U614 | IC, Very Wide Band Operational Amplifier, 2625 | IC-439 |
| U615 | IC, Very Wide Band Operational Amplifier, 2625 | IC-439 |
| U616 | IC, LF442A | IC-410 |
| U617 | IC, LF442A | IC-410 |
| U618 | IC, Voltage Regulator, -5V,-LM320L-5 | IC-395 |
| W601 | Connector Pins | CS-339-3 |
| W602 | Connector Pins | CS-339-3 |
| W601 | Jumper | CS-476 |
| W602 | Jumper | CS-476 |




Figure 8-9. Model 5902 (1MHz), Component Location Drawing, Dwg. No. 5902-100


Figure 8-10. Model 5902 (1MHz), Schematic Diagram, Dwg. No. 5902-106

Table 8-6. KI590 Operational Amplifier (4607), Parts List

| Circuit <br> Designation | Description | Keithley Part Number |
| :---: | :---: | :---: |
| C700 | Capacitor, $10 \mu \mathrm{~F}, 25 \mathrm{~V}$, Aluminum Electrolytic | C-377-10 |
| C701 | Capacitor, $0.1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-0.1 |
| C702 | Capacitor, $1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-1 |
| C703 | Capacitor, $0.1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-0.1 |
| C704 | Capacitor, $10 \mu \mathrm{~F}, 25 \mathrm{~V}$, Aluminum Electrolytic | C-377-10 |
| C705 | Capacitor, $0.1 \mu \mathrm{~F}, 50 \mathrm{~V}$, Ceramic Film | C-237-0.1 |
| C706 | Capacitor, 5pF, Ceramic Disc | C-64-5p |
| CR700 | Diode, Silicon, 1N4148 | RF-28 |
| CR701 | Diode, Silicon, 1N4148 | RF-28 |
| Q700 | Transistor, Silicon, NPN, 2N3904 | TG-47 |
| Q701 | Transistor, Silicon, PNP, 2N3906 | TG-84 |
| Q702 | Transistor, Silicon, PNP, 2N3906 | TG-84 |
| Q703 | Transistor, Silicon, NPN, 2N3904 | TG-47 |
| Q704 | Transistor, Silicon, NPN, 2N3904 | TG-47 |
| Q705 | Transistor, Silicon, NPN, 2N3904 | TG-47 |
| R700 | Resistor, 208, 5\%, 1/4W, Composition | R-76-20 |
| R701 | Resistor, 209, $5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-20 |
| R702 | Resistor, 1 k , 1\%, $1 / \mathrm{s} \mathrm{W}$ | R-88-1k |
| R703 | Resistor, 100, 5\%, 1/4W, Composition | R-76-10 |
| R704 | Resistor, 4320, $1 \%, 1 / s{ }^{\text {W }}$ W | R-88-432 |
| R705 | Resistor, $2.15 \mathrm{k} \Omega, 1 \%, 1 / \mathrm{W}$ | R-88-2.15k |
| R706 | Resistor, 108, 1\%, ${ }^{1 / 8} \mathrm{~W}$ | R-88-10 |
| R707 | Resistor, 15.8k』, 1\%, 1/s W | R-88-15.8k |
| R708 | Resistor, 10n, 1\%, $1 / 8 \mathrm{~W}$ | R-88-10 |
| R709 | Resistor, $8660,1 \%, 1 / s \mathrm{~W}$ | R-88-866 |
| R710 | Resistor, $4.99 \mathrm{k} \Omega, 1 \%, 1 / 5 \mathrm{~W}$ | R-88-4.99k |
| R711 | Resistor, 10n, $5 \%$, 1/4W, Composition | R-76-10 |
| R712 | Resistor, $82 \Omega, 5 \%, 1 / 4 \mathrm{~W}$, Composition | R-76-82 |



gure 8-11. KI590 Operational Amplifier (U607), Component Location Drawing, Dwg. N. 5902-180


Figure 8-12. KI590 Operational Amplifier (U607), Schematic Diagram, Dwg. No. 5902-186

## Table 8-7. Case Parts

| Quantity | Description | Keithley <br> Part Number |
| :--- | :--- | :--- |
|  |  |  |
| 2 | Side Panel | $228-301$ |
| 1 | Front Bezel | $228-303$ |
| 3 | P.C. Support | $228-318$ |
| 1 | Modified P.C. Support | $228-314-3$ |
| 1 | Modified P.C. Support | $228-314-4$ |
| 1 | Front Panel | $590-302$ |
| 1 | Display Window | $590-304-1$ |
| 1 | Display Window | $590-304-2$ |
| 1 | Front Panel Overlay | $590-305$ |
| 1 | Connector Bracket | $590-327$ |
| 1 | Capacitor (Bracket-to-Case) | C-22-.01 |
| 1 | Choke | CH-29 |
| 1 | Fastener (Routing Clip for CH-29) | FA-195 |
| 5 | Mounting Rails | $228-319$ |
| 1 | Module Mounting Shelf | $590-317$ |
| 1 | Rear Panel | $590-307$ |
| 1 | Fan | FN-8 |
| 1 | Fan Filter | FL-6 |
| $\mathbf{1}$ | BNC Bracket | $590-328$ |
| 1 | Capacitor, (Bracket-to-Case) | C-22-.01 |
| 1 | Choke | CH-29 |
| 1 | Fastener for CH-29 | FA-195 |
| 1 | Top Cover | $228-312$ |
| 1 | Bottom Cover | $228-313$ |
| 2 | Rear Foot | $706-316$ |
| 2 | Front Foot Assembly | $706-317$ |
| 2 | Decorative Strip | $706-321$ |
| 2 | Decorative Strip | $706-339$ |

Note: See assembly drawings in Section 7 for parts locations.

Table 8-8. Miscellaneous Mechanical Parts

| Quantity | Description | Keithley <br> Location | Part Number |
| :---: | :---: | :---: | :---: |
| 2 | Fuse Holder (Bias Fuse) | Mother Board | FH-12 |
| 1 | Heat Sink (for TG-185 and TG-186) | Mother Board | HS-30 |
| 2 | Mounting Kit (for TG-185 and TG-186) | Mother Board | MK-23 |
| 1 | Shield, A/D Converter | Mother Board | 590-313 |
| 1 | Shield, Input Multiplexer | Mother Board | CN-57 |
| 2 | Pushbutton (LOCAL, SHIFT) | Display Board | 228-317-4 |
| 7 | Pushbatton (RANGE through CAE) | Display Board | 228-317-5 |
| 8 | Pushbutton (MANUAL through SETUP) | Display Board | 228-317-6 |
| 16 | Pushbutton ( $\triangle$ through C vs t) | Display Board | 228-3177 |
| 1 | Heat Sink (for IC-240) | Digital Board | HS-22 |
| 1 | Mounting Kit (for-IC-240) | Digital Board | MK-16 |
| 1 | Heat Sink (for IC-240) | Digital Board | HS-27 |
| 1 | Mounting Kit (for IC-240) | Digital Board | MK-20 |
| 5 | Heat Sink (for IC-93 and IC-174) | Digital Board | HS-30 |
| 4 | Mounting Kit (for IC-93 and IC-174) | Digital Board | MK-18 |
| 1 | Mounting Kit (for TG-107 and TG-108) | Digital Board | MK-23 |
| 1 | BNC Jack Bracket | Digital Board | 590-310 |
| 2 | Socket (for LSI-56) | Digital Board | SO-69 |
| 1 | Fuse Holder Body | Digital Board | FH-21 |
| 1 | Fuse Carrier (for 3AG Fuse) | Digital Board | FH-25 |
| 1 | Fuse Carrier (for 5mm Fuse) | Digital Board | FH-26 |
| 1 | Line Cord |  | CO-7 |
| 1 | Shield, Top | 5901 Module | 5901-302 |
| 1 | Shield, Bottom | 5901 Module | 5901-304 |
| 1 | Shield, Op Amp | 5902 Module | 5902-307 |
| 1 | Skield | 5902 Module | 5902-304 |

Table 8-9. Model 5904 Input Adapter, Parts List

| Circuit <br> Quantity | Description | Keithley <br> Part Number |
| :---: | :--- | :--- |
|  | Box, Modified |  |
| 1 | Conector, BNC (Female) | $5904-302$ |
| 2 | Connector, BNC (Male) | CS-249 |
| 2 | Choke | CS-552 |
| 1 | Transformer | TR-242 |
| 1 | Tug | UU-27 |
| 1 | Lug | CU-100 |
| 1 | Washer, Black Neoprene | WA-86-2 |


| Decimal | Hexadecimal | ASCII | IEEE-488 Messages* |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
| 0 | 00 | NUL |  |
| 1 | 01 | SOH | GTL |
| 2 | 02 | STX |  |
| 3 | 03 | ETX | SDC |
| 4 | 04 | EOT | PPC |
| 5 | 05 | ENQ |  |
| 6 | 06 | ACK |  |
| 7 | 07 | BEL |  |
| 8 | 08 |  | BS |
| 9 | 09 | HT | TCT |
| 10 | 09 | LF |  |
| 11 | $0 B$ | VT |  |
| 12 | $0 C$ | FF |  |
| 13 | $0 D$ | CR |  |
| 14 | $0 E$ | SO |  |
| 15 | $0 F$ | SI |  |
| 16 | 10 | DLE |  |
| 17 | 11 | DC1 |  |
| 18 | 12 | DC2 |  |
| 19 | 13 | DC3 |  |
| 20 | 14 | DC4 |  |
| 21 | 15 | NAK |  |
| 22 | 16 | SYN |  |
| 23 | 17 | ETB |  |
| 24 |  |  |  |
| 25 | 18 | CAN |  |
| 26 | 19 | EM |  |
| 27 | $1 A$ | SUB |  |
| 28 | $1 B$ | ESC |  |
| 29 | $1 C$ | FS |  |
| 30 | $1 E$ | GS | RS |
| 31 | $1 F$ | US |  |

[^3]| Decimal | Hexadecimal | ASCII | IEEE-488 Messages* |
| :---: | :---: | :---: | :---: |
| 32 | 20 | SP | MLA 0 |
| 33 | 21 | ! | MLA 1 |
| 34 | 22 | " | MLA 2 |
| 35 | 23 | \# | MLA 3 |
| 36 | 24 | \$ | MLA 4 |
| 37 | 25 | \% | MLA 5 |
| 38 | 26 | \& | MLA 6 |
| 39 | 27 | , | MLA 7 |
| 40 | 28 | ( | MLA 8 |
| 41 | 29 | ) | MLA 9 |
| 42 | 2A | * | MLA 10 |
| 43 | 2B | + | MLA 11 |
| 44 | ${ }^{2} \mathrm{C}$ | , | MLA 12 |
| 45 | 2D | - | MLA 13 |
| 46 | 2 E |  | MLA 14 |
| 47 | 2F | 1 | MLA 15 |
| 48 | 30 | 0 | MLA 16 |
| 49 | 31 | 1 | MLA 17 |
| 50 | 32 | 2 | MLA 18 |
| 51 | 33 | 3 | MLA 19 |
| 52 | 34 | 4 | MLA 20 |
| 53 | 35 | 5 | MLA 21 |
| 54 | 36 | 6 | MLA 22 |
| 55 | 37 | 7 | MLA 23 |
| 56 | 38 | 8 | MLA 24 |
| 57 | 39 | 9 | MLA 25 |
| 58 | 3A | : | MLA 26 |
| 59 | 3B | ; | MLA 27 |
| 60 | 3 C | < | MLA 28 |
| 61 | 3D | $=$ | MLA 29 |
| 62 | 3E | > | MLA 30 |
| 63 | 3F | ? | UNL |

[^4]
## ASCII CHARACTER CODES AND IEEE-488 MULTILINE INTERFACE COMMAND MESSAGES

Decimal Hexadecimal ASCII IEEE-488 Messages*

| 64 | 40 | (1) | MTA 0 |
| :---: | :---: | :---: | :---: |
| 65 | 41 | A | MTA 1 |
| 66 | 42 | B | MTA 2 |
| 67 | 43 | C | MTA 3 |
| 68 | 44 | D | MTA 4 |
| 69 | 45 | E | MTA 5 |
| 70 | 46 | F | MTA 6 |
| 71 | 47 | G | MTA 7 |
| 72 | 48 | H | MTA 8 |
| 73 | 49 | I | MTA 9 |
| 74 | 4A | J | MTA 10 |
| 75 | 4B | K | MTA 11 |
| 76 | 4 C | L | MTA 12 |
| 77 | 4D | M | MTA 13 |
| 78 | 4E | N | MTA 14 |
| 79 | 4 F | 0 | MTA 15 |
| 80 | 50 | P | MTA 16 |
| 81 | 51 | Q | MTA 17 |
| 82 | 52 | R | MTA 18 |
| 83 | 53 | S | MTA 19 |
| 84 | 54 | T | MTA 20 |
| 85 | 55 | U | MTA 21 |
| -86 | 56 | V | MTA 22 |
| 87 | 57 | W | MTA 23 |
| 88 | 58 | X | MTA 24 |
| 89 | 59 | Y | MTA 25 |
| 90 | 5A | Z | MTA 26 |
| 91 | 5B | [ | MTA 27 |
| 92 | 5 C | 1 | MTA 28 |
| 93 | 5D | 1 | MTA 29 |
| 94 | 5E | $\wedge$ | MTA 30 |
| 95 | 5F | - | UNT |

[^5]
## ASCII CHARACTER CODES AND IEEE-488 MULTILINE INTERFACE COMMAND MESSAGES

Decimal Hexadecimal ASCI
IEEE-488 Messages*

| 96 | 60 | $\cap$ | MSA 0,PPE |
| :---: | :---: | :---: | :---: |
| 97 | 61 | a | MSA 1,PPE |
| 98 | 62 | , | MSA 2,PPE |
| 99 | 63 | c | MSA 3,PPE |
| 100 | 64 | d | MSA 4,PPE |
| 101 | 65 | e | MSA 5,PPE |
| 102 | 66 | f | MSA 6,PPE |
| 103 | 67 | g | MSA 7,PPE |
| 104 | 68 | h | MSA 8,PPE |
| 105 | 69 | , | MSA 9,PPE |
| 106 | 6A | j | MSA 10,PPE |
| 107 | 6B | k | MSA 11,PPE |
| 108 | 6 C | 1 | MSA 12,PPE |
| 109 | 6 D | m | MSA 13, PPE |
| 110 | 6E | n | MSA 14,PPE |
| 111 | 6F | 0 | MSA 15,PPE |
| 112 | 70 | p | MSA 16,PPD |
| 113 | 71 | q | MSA 17,PPD |
| 114 | 72 | r | MSA 18,PPD |
| 115 | 73 | s | MSA 19,PPD |
| 116 | 74 | t | MSA 20,PPD |
| 117 | 75 | u | MSA 21,PPD |
| 118 | 76 | v | MSA 22,PPD |
| 119 | 77 | w | MSA 23,PPD |
| 120 | 78 | $x$ | MSA 24,PPD |
| 121 | 79 | y | MSA 25,PPD |
| 122 | 7A | $z$ | MSA 26,PPD |
| 123 | 7 B | \{ | MSA 27,PPD |
| 124 | 7 C | ) | MSA 28,PPD |
| 125 | 7D | \} | MSA 29,PPD |
| 126 | 7E | $\sim$ | MSA 30,PPD |
| 127 | 7F | DEL |  |

*Message send or received with ATN true. Numbers represent secondary address values resulting in MSA (My Secondary Address).

The following programs have been supplied as a simple aid to the user and are not intended to suit specific needs. Each program allows you send a device-dependent command string to the instrument and obtain and display an instrument reading string.

Programs for the following controllers are included:

- IBM PC or XT (with Keithley Model 8573A IEEE-488 Interface)
- Apple II (equipped with the Apple II IEEE-488 Interface)
- Hewlett-Packard Model 85
- Hewlett-Packard Model 9816
- Hewlett-Packard Model 9825A
- DEC LSI 11


## NOTE

The Model 590 uses commas to separate parameters in some commands. Many controllers also use commas to delimit input strings. Use quotes around the command string to avoid problems.

## IBM PC OR XT（KEITHLEY MODEL 8573A INTERFACE）

The following program sends a command string to the Model 590 from an IBM PC or XT com－ puter and displays the instrument reading string on the CRT．The computer must be equipped with the Keithley Model 8573A IEEE－488 Interface and the DOS 2.00 operating system．Model 8573A software must be installed and configured as described in the instruction manual．

## DIRECTIONS

1．Using the front panel IEEE key，set the primary address of the Model 590 to 15.
2．With the power off，connect the Model 590 to the IEEE－488 interface installed in the IBM computer．
3．Type in BASICA on the computer keyboard to get into the IBM interpretive BASIC language．
4．Place the interface software disc in the default drive，type $\mathrm{LOAD}{ }^{\prime} \mathrm{DECL}^{\prime \prime}$ ，and press the return key．
5．Add the lines below to lines $1-6$ which are now in memory．Modify the address in lines 1 and 2，as described in the Model 8573A Instruction Manual．
6．Run the program and type in the desired command string．For example，to place the instru－ ment in autorange and 1 MHz frequency，type in ROFIX and press the return key．
7．The instrument reading string will then appear on the display．For example，the display might show NCPM＋1．2345E－12．
8．To exit the program，type in EXTT at the command prompt and press the return key．

## PROGRAM

10 ELS
201NA事＝＂GPIBO！：CALL IBFINI



$40 \mathrm{~V} \%=15: C A L L$ IBPAI（M59g\％sUR）
$504 \%=2 H 162: C A L L E P O K E(B R D W \%, W \%)$
$60 \mathrm{~V}=1: \mathrm{CALL}$ IBSEE（BRIWK，W\％）

ga IF CMDo＝isERIT＂：THEH 150
90 IF CNDF＝：：THEN 70
$95 \mathrm{CMD} \$=\mathrm{CMD} \$+\mathrm{CHR} \$(13)+\mathrm{CHR} \$(10)$
100 CALL IBWRT（1590\％，IMD家）
110RD末＝5FACE（106）

130 FRIMT RI丰
146 GOTO TO

160 EALL IROHL（ERTG\％：UK）

## COMMENTS

Clear screen．
Find board descriptor．
Find instrument descriptor．
Set primary address to 15 ．
Set timeouts．
Set REN true．
Prompt for command．
See if program is to be halted．
Check for null input．
Address 590 to listen，send string．
Define reading input buffer．
Address 590 to talk，get reading．
Display the string．
Repeat．
Close the instrument file．
Close the board file．

NOTE：For conversion to numeric variable，make the following changes：

135 PRINT RII

## APPLE II（APPLE II IEEE－488 INTERFACE）

The following program sends a command string to the Model 590 from an Apple II computer and displays the instrument reading string on the computer CRT．

The computer must be equipped with the Apple II IEEE－488 Interface installed in slot 5．Note that the program assumes that the computer is running under Apple DOS 3.3 or ProDOS．

## DIRECTIONS

1．Using the front panel IEEE key，set the primary address of the Model 590 to 15.
2．With the power off，connect the Model 590 to the IEEE－ 488 interface installed in the Apple II computer．
3．Enter the lines in the program below，using the RETURN key after each line．
4．Run the program and type in the desired command string at the command prompt．For exam－ ple，to place the instrument in the autorange and 1 MHz modes，type in R0F1X and press the return key．
5．The instrument reading string will then appear on the CRT．A typical display is： NCPK＋1．2345E－12．

PROGRAM

## COMMENTS

```
10 2$=CHR&(26):Dक=[HR生(4)
2a ADIR=15: 5LOT=5
```



```
40 PRINT J家; "PR,#* ; SLUT
50 FRIHT I*;'sIH##:; SLOT
6MFRIHT:"RA":
FOFRINT:&LFI:#
```



```
P0 FRINT "&RI":;DHR& (G4+ADIRO;Z疌 Address 590 to talk.
IGOINFUIT [AS:ANM
119 PRINT ":UT": Untalk the bus.
120 PRINT D*; "PR&#G", Define output to CRT.
130 PRINT DF; "IN#G": Define input from keyboard.
14E FRINT A* Display string.
15460T030, Repeat.
```

NOTES：
1．If conversion to numeric variable is required，make the following changes：


```
125 FRINT A
```

2．The Apple II INPUT statement terminates on commas．To avoid problems，program the Model 590 for the $\mathrm{O} 1, \mathrm{O} 2$ ，or O 3 data format to eliminate commas．

## HEWLETT-PACKARD MODEL 85

The following program sends a command string to the Model 590 from an $H P-85$ computer and displays the instrument reading string on the computer CRT. The computer must be equipped with the HP82937 GPIB Interface and an I/O ROM.

## DIRECTIONS

1. Using the front panel IEEE key, set the primary address of the Model 590 to 15.
2. With the power off, connect the Model 590 to the HP82937A GPIB interface installed in the HP-85 computer.
3. Enter the lines in the program below, using the END LINE key after each line.
4. Press the HP-85 RUN key and type in the desired command string at the command prompt. For example, to place the instrument in the autorange and 1 MHz average modes, type in R0F1X and press the END LINE key.
5. The instrument reading string will then appear on the CRT. A typical display is: NCPM $+1.2345 \mathrm{E}-12$.

## PROGRAM

## COMMENTS


Dimension strings.
20REMUTE 715
Place 590 in remote.
30 IISP: "COHMANIISTRING: ;
Prompt for command.
40 IHFUT A
Input command string.
50 DITPUT 715: H*
Address 590 to listen, send string.
60 EHTER 715; 时
Address 590 to talk, input reading.
7011SP EF
Display reading string.
80 GOTO 30
Repeat
90 EHD
NOTE: For conversion to numeric variable, change line 70 as follows:
70 DISP UAL《S $5[5 ; 15]$ )

## HEWLETT-PACKARD MODEL 9816

The following program sends a command string to the Model 590 from a Hewlett-Packard Model 9816 computer and displays the instrument reading string on the computer CRT. The computer must be equipped with the HP82937 GPIB Interface and BASICA 2.0.

## DIRECTIONS

1. Using the front panel IEEE key, set the primary address of the Model 590 to 15.
2. With the power off, connect the Model 590 to the HP82937A GPIB interface installed in the 9816 computer.
3. Type EDIT and press the EXEC key.
4. Enter the lines in the program below, using the ENTER key after each line.
5. Press the 9816 RUN key and type in the desired command string at the command prompt. For example, to place the instrument in the autorange and 1 MHz modes, type in ROFIX and press the ENTER key.
6. The instrument reading string will then appear on the CRT. A typical display is: NCPM $+1.2345 \mathrm{E}-12$.

## PROGRAM

## COMMENTS

```
10 REMOTET15
```



```
S0 OUTFIIT 715: A韦
40 ENTEF:715; B% 
50 FRIHT B$
60 GOTD 20
70 EHD
```

NOTE: For conversion to a numeric variable, change the program as follows:
4 ENTER $715: \mathrm{E}$
$50 \mathrm{FRIHT} E$

## HEWLETT-PACKARD MODEL 9825A

Use the following program to send a command string to the Model 590 from a Hewlett-Packard Model 9825A and display the instrument reading string on the computer printer. The computer must be equipped with the HP98034A HPIB Interface and a 9872A extended I/O ROM.

## DIRECTIONS

1. From the front panel, set the primary address of the Model 590 to 15.
2. With the power off, connect the Model 590 to the 98034A HPIB interface installed in the 9825A.
3. Enter the lines in the program below, using the STORE key after each line. Line numbers are automatically assigned by the 9825A.
4. Press the 9825A RUN key and type in the desired command string at the command prompt. For example, to place the instrument in the autorange and 1 MHz modes, type in $\mathrm{RO}=\mathrm{FIX}$ and press the CONT key.
5. The instrument reading string will then appear on the computer print out. A typical display is: NCPM $+1.2345 \mathrm{E}-12$.

## PROGRAM


1 dev" 590 ": 715
2 rem" 590 "
3 ent "COMmANISTRIHG", BE

5red"590": A*
6 prt A.
7 gto 3

## COMMENTS

Dimension data strings.
Define 590 at address 15.
Place 590 in remote.
Prompt for command string.
Address 590 to listen, send string.
Address 590 to talk, input data.
Print data string on printer.
Repeat.

NOTE: For conversion to numeric variable, modify the program as follows:
6 prt val (A) C [5])

## DEC LSI 11

The following program sends a command string to the Model 590 from a DEC LSI 11 minicomputer and displays the instrument reading string on the DEC CRT terminal. The LSI 11 must be configured with 16 K words of RAM and an IBV 11 IEEE- 488 interface. The software must be configured with the IB software as well as FORTRAN and the RT 11 operating system.

## DIRECTIONS

1. Using the front panel IEEE key, set the primary address of the Model 590 to 15.
2. With the power off, connect the Model 590 to the IBV 11 IEEE- 488 interface cable.
3. Enter the program below, using the editor under RT 11 and the name IEEE.FOR.
4. Compile using the FORTRAN compiler as follows: FORTRAN IEEE.
5. Link with the system and IB libraries as follows: LINK IEEE,IBLIB.
6. Type RUN IEEE and press the REIURN key.
7. The display will read "ENTER ADDRESS".
8. Type in 15 and press the RETURN key.
9. The display will read "TEST SETUP".
10. Type in the desired command string and press the RETURN key. For example, to program the instrument for the autorange and 1 MHz modes, type in ROFIX and press RETURN.
11. The instrument data string will appear on the computer display. A typical display is: NCPM+1.2345E-12.

FROGRAH IEEE
IWTEGERE PRIADR
LOGICAL*1 1 GG(80): INPUT(80)
DO2I = 1:10
CALL IBETER(I:G) Turn off IB errors
2 COHT IHLE
CALL IBSTER(15:5)
Allow 5 error 15's.
CHLL IETIMO(120)
EALL IETERM(10)
Allow 1 second bus timeout.
Set line feed as terminator.
Turn on remote.
4 TYFE 5

Input primary address.

```
ACEEPT 1区:PRIADR
```

10 FORMAT (2)
12 TYPE 15
15 FORMAT (1X: TEST SETUP: * $⿻$ : \% Prompt for command string.
CALL GETSTR (5, MSG:72)
EALL IBSEDI (NSG:-1:FRIADR)
18 I=IBRECU (INFUT: G
INFUT $(I+1)=0$
EHLL FUTSTR (7, INPUT: "E!
CHLL IEUNT
GOTO 12
Repeat.
EHD

## PET/CBM 2001

The following program sends a command string to the Model 590 from a PET/CBM 2001 computer and displays the instrument reading string on the computer CRT. As the PET/CBM computer has a standard IEEE-488 interface, no additional equipment is necessary.

## DIRECTIONS

1. Using the front panel IEEE key, set the primary address of the Model 590 to 15.
2. With the power off, connect the Model 590 to the PET/CBM IEEE- 488 interface.
3. Enter the lines of the program below, using the RETURN key after each line is typed.
4. Type RUN and press the RETURN key. Type in the desired command string at the command prompt. For example, to place the instrument in the autorange and 1 MHz modes, type in ROFIX and press the RETURN key.
5. The instrument reading string will then appear on the CRT. A typical display is: NCPM $+1.2345 \mathrm{E}-12$.

## PROGRAM <br> COMMENTS

| 10 DPEN 1:15 | Open file 1, primary address 15. |
| :---: | :---: |
|  | Prompt for, input command string. |
| 30 PRINT\#1: Eis | Address 590 to listen, send string. |
|  | Address 590 to talk, input data. |
| 50 IF ST $=2$ THEN 46 | If bus timeout, input again. |
| 60 FRINT A ${ }^{\text {a }}$ | Display reading string. |
| 70 cOTO CG | Repeat. |

## NOTES:

1. If conversion to numeric variable is required, modify the program as follows:
```
60A=UAL(MID$(A末:5:15))
70PFINT A
g0 GOT020
```

2. The PET INPUT\# statement terminates on a comma. Thus, when reading Model 590 strings which include commas, you should input each portion of the string into a separate string variable. For example, in the $O 0$ mode, to obtain and display readings, the program above can be modified as follows:
```
40 IHPIT#1: A末,B%,C*
```



## APPENDIX C

IEEE-488 BUS OVERVIEW

## BUS DESCRIPTION

The IEEE-488 bus, which is also frequently referred to as the GPIB (General Purpose Interface Bus), was designed as a parallel transfer medium to optimize data transfer with a minimum number of bus lines. In keeping with this goal, the bus has eight data lines that are used both for data and many commands. Additionally, the bus has five management lines, which are used to control bus operation, and three handshake lines that are used to control the data byte transfer sequence.

A typical configuration for controlled bus operation is shown in Figure C-1. A typical system will have one controller and one or more devices to which commands are given and, in most cases, from which data is received. Generally, there are three categories that describe device operation: controller, talker, and listener.

The controller does what its name implies: it controls other devices on the bus. A talker sends data (usually to the controller), and a listener receives data. Depending on the instrument, a particular device may be a talker only, a listener only, or both a talker and a listener. The Model 590 has both talker and listener capabilities.

There are two categories of controllers: system controller and basic controller. Both are able to control other devices, but only the system controller has absolute authority in the system. In a system with more than one controller, only one controller may be active at any given time. Certain command protocol allows control to be passed from one controller to another.

The bus is limited to 15 devices, including the controller. Thus, any number of devices may be present on the bus at one time. Although several active listeners may be present simultaneously, only one active talker may be present on the bus, or communications would be scrambled.


Figure C-1. IEEE Bus Configuration

A device is placed in the talk or listen mode from the controller by sending an appropriate talk or listen command. These talk and listen commands are derived from an instrument's primary address. The primary address may have any value between 0 and 30 and is generally set by rear panel switches or programmed in from the front panel (as in the case of the Model 590). The actual listen command value sent over the bus is derived by ORing the primary address with $\$ 20$ (the $\$$ symbol preceding the number designates a hexadecimal, or base 16 value). For example, if the primary address is 15 (the default Model 590 value), the actual listen command byte value is $\$ 2 F$ $(\$ 0 F+\$ 20=\$ 2 F)$. In a similar manner, the talk command byte is derived by ORing the primary address with $\$ 40$. With a primary address of 15 , the actual talk command byte would be $\$ 4 \mathrm{~F}(\$ 40+\$ 0 \mathrm{~F}=\$ 4 \mathrm{~F})$.

The IEEE-488 standards also include another addressing mode called secondary addressing. Secondary address byte values lie in the range of $\$ 60-\$ 7 \mathrm{~F}$. Note, however, that many devices, including the Model 590, do not use secondary addressing.

Once the device is properly addressed, bus transmission sequences are set to take place. For example, if an instrument is addressed to talk, it will usually output its data string on the bus one byte at a time. The listening device (frequently the controller) will then read this information as transmitted.

## BUS LINES

The signal lines on the IEEE-488 bus are grouped into three categories: data lines, management lines, and handshake lines. The eight data lines handle bus data and many commands, while the management and handshake lines ensure orderly bus operation. Each bus line is active low with approximately zero volts representing logic 1 (true). The following paragraphs briefly describe the operation of these lines.

## Data Lines

The bus uses eight data lines to transmit and receive data in bit-parallel, byte serial fashion. These lines use the convention DIO1-DIO8 instead of the more common D0-D7. DIO1 is the least significant bit, while DIO8 is the most significant bit. The data lines are bidirectional (with most devices), and, as with the remaining bus lines, low is considered to be true.

## Bus Management Lines

The five bus management lines ensure proper interface control and management. These lines are used to send uniline commands.

ATN (Attention)-The state of ATN determines how information on the data lines is to be interpreted.

IFC (Interface Clear)-IFC allows the clearing of active talkers or listeners from the bus.

REN (Remote Enable)-REN is used to place devices in the remote mode. Usually, devices must be in remote before they can be programmed over the bus.

EOI (End Or Identify)-EOI is used to mark the end of a multi-byte data transfer sequence. EOI is also used along with ATN, to send the IDY (identify) message for paralle polling.

SRQ (Service Request)-SRQ is used by devices to request service from the controller.

## Handshake Lines

Three handshake lines that operate in an interlocked sequence are used to ensure reliable data transmission regardless of the transfer rate. Generally, data transfer will occur at a rate determined by the slowest active device on the bus. These handshake lines are:

DAV (Data Valid)-The source (talker) controls the state of DAV to indicate to any listeners when data is valid.

NRFD (Not Ready For Data)-The acceptor (listener) controls the state of NRFD. It is used to signal the transmitting device to hold off the byte transfer sequence until the accepting device is ready.

NDAC (Not Data Accepted)-NDAC is also controlled by the accepting device. The state of NDAC tells the source whether or not the device has accepted the data byte.

Figure C-2 shows the basic handshake sequence for the transmission of one data byte. This sequence is used to transfer data, talk and listen addresses, as well as multiline commands.

## BUS COMMANDS

Commands associated with the IEEE-488 bus can be grouped into the following three general categories. Refer to Table C-1.

Uniline Commands-These commands are asserted by setting the associated bus line true. For example, to assert REN (Remote Enable), the REN line would be set low (true).

Multiline Commands-General bus commands which are sent over the data lines with the ATN line true.

Device-dependent Commands-Commands whose meanings depend on the device in question. These commands are transmitted via the data lines while ATN is false.

Figure C-2. IEEE Handshake Sequence
Table C-1. IEEE-488 Bus Command Summary

| Command Type | Command | State of ATN Line* | Comments |
| :---: | :---: | :---: | :---: |
| Uniline | REN (Remote Enable) <br> EOI <br> IFC (Interface Clear) <br> ATN (Attention) SRQ | $\begin{gathered} \hline X \\ X \\ X \\ \text { Low } \\ X \end{gathered}$ | Sets up devices for remote operation. Marks end of transmission. Clears interface Defines data bus contents. Controlled by external device. |
| Multiline |  |  |  |
| Universal | LLO (Local Lockout) | Low | Locks out local operation. |
|  | DCL (Device Clear) | Low | Returns device to default conditions. |
|  | SPE (Serial Enable) | Low | Enables serial polling. |
|  | SPD (Serial Poll Disable) | Low | Disables serial polling. |
| Addressed | SDC (Selective Device Clear) | Low | Returns unit to default conditions. |
|  | GTL (Go To Local) | Low | Returns device to local. |
|  | GET (Group Execute Trigger) | Low | Triggers device for reading. |
| Unaddressed | UNL (Unlisten) <br> UNT (Untalk) | $\begin{aligned} & \text { Low } \\ & \text { Low } \end{aligned}$ | Removes all listeners from bus. Removes any talkers from bus. |
| Device-dependent |  | High | Programs Model 590 for various modes. |

[^6]
## Uniline Commands

The five uniline commands include REN, EOI, IFC, ATN, and SRQ. Each command is associated with a dedicated bus line, which is set low to assert the command in question.

REN (Remote Enable)-REN is asserted by the controller to set up instruments on the bus for remote operation. When REN is true, devices will be removed from the local mode. Depending on device configuration, all front panel controls except the LOCAL button (if the device is so equipped) may be locked out when REN is true. Generally, REN should be asserted before attempting to program instruments over the bus.

EOI (End or Identify)-EOI may be asserted either by the controller or by external devices to identify the last byte in a multi-byte transfer sequence, allowing data words of various lengths to be transmitted.

IFC (Interface Clear)-IFC is asserted by the controller to clear the interface and return all devices to the talker and listener idle states.

ATN (Attention)-The controller asserts ATN while sending addresses or multiline commands.

SRQ (Service Request)-SRQ is asserted by a device on the bus when it requires service from the controller.

## Universal Multiline Commands

Universal multiline commands are those commands that required no addressing as part of the command sequence. All devices equipped to implement these commands will do so simultaneously when the commands are transmitted. As with all multiline commands, these commands are transmitted with ATN true.

LLO (Local Lockout)-LLO is sent to instruments to lock out front panel or local operation of the instrument.

DCL (Device Clear)-DCL is used to return instruments to some default state. Usually, devices return to their power-up conditions.

SPE (Serial Poll Enable)-SPE is the first step in the serial polling sequence, which is used to determine which device on the bus is requesting service.

SPD (Serial Poll Disable)-SPD is used by the controller to remove all devices on the bus from the serial poll mode and is generally the last command in the serial polling sequence.

## Addressed Multiline Commands

Addressed multiline commands are those commands that must be preceded by an appropriate listen address before the instrument will respond to the command in question. Note that only the addressed device will respond to the command. Both the command and the address preceding it are sent with ATN true.

SDC (Selective Device Clear)-The SDC command performs essentially the same function as DCL except that only the addressed device responds. Generally, instruments return to their power-up default conditions when responding to SDC.

GTL (Go To Local)-GTL is used to remove instruments from the remote mode and place them in local. With many instruments, GTL may also restore operation of front panel controls if previously locked out.

GET (Group Execute Trigger)-GET is used to trigger devices to perform a specific action that will depend on device configuration (for example, perform a measurement sequence). Although GET is an addressed command, many devices may respond to GET without addressing.

## Address Commands

Addressed commands include two primary command groups, and a secondary address group. ATN is true when these commands are asserted. These commands include:

LAG (Listen Address Group)-These listen commands are derived from an instrument's primary address and are used to address devices to listen. The actual command byte is obtained by ORing the primary address with $\$ 20$.

TAG (Talk Address Group)-The talk commands are derived from the primary address by ORing the address with $\$ 40$. Talk commands are used to address devices to talk.

SCG (Secondary Command Group)-Commands in this group provide additional addressing capabilities. Many devices (including the Model 590) do not use these commands.

## Unaddress Commands

The two unaddress commands are used by the controller to remove any talkers or listeners from the bus. ATN is true when these commands are asserted.

UNL (Unlisten)-Listeners are placed in the listener idle state by UNL.

UNT (Untalk)-Any previously commanded talkers will be placed in the talker idle state by UNT.

## Device-Dependent Commands

The purpose of device-dependent commands will depend on instrument configuration. Generally, these commands
are sent as one or more ASCII characters that command the device to perform a specific action. For example, the command string ROX is used to control the measurement range of the Model 590.

The IEEE-488 bus treats these commands as data in that ATN is false when the commands are transmitted.

## Command Codes

Command codes for the various commands that use the data lines are summarized in Figure C-3. Hexadecimal and and decimal values for the various commands are listed in Table C-2.


[^7]Figure C-3. Command Codes

## Table C-2. Hexadecimal and Decimal Command Codes

| Command | Hex Value | Decimal Value |
| :---: | :---: | :---: |
| GTL | 01 | 1 |
| SDC | 04 | 4 |
| GET | 08 | 8 |
| LLO | 11 | 17 |
| DCL | 14 | 20 |
| SPE | 18 | 24 |
| SPD | 19 | 25 |
| LAG | $20-3 \mathrm{~F}$ | $32-63$ |
| TAG | $40-5 \mathrm{~F}$ | $64-95$ |
| SGG | $60-7 \mathrm{~F}$ | $96-127$ |
| UNL | 3 F | 63 |
| UNT | 5 F | 95 |

## Typical Command Sequences

For the various multiline commands, a specific bus sequence must take place to properly send the command. In particular, the correct listen address must be sent to the instrument before it will respond to addressed commands. Table C-3 lists a typical bus sequence for sending an addressed multiline command. In this instance, the SDC command is being sent to the instrument. UNL is generally sent as part of the sequence to ensure that no other active listeners are present. Note that ATN is true for both the listen command and the SDC command byte itself.

Table C-3. Typical Addressed Command Sequence

|  |  |  | Data Bus |  |  |
| :---: | :---: | :--- | :---: | :---: | :---: |
| Step | Command | ATN State | ASCII | Hex | Decimal |
| 1 | UNL | Set low | $?$ | $3 F$ | 63 |
| 2 | LAG | Stays low | $i$ | $2 F$ | 47 |
| 3 | SDC | Stays low | EOT | 04 | 4 |
| 4 |  | Returns high |  |  |  |

*Assumes primary address $=15$.

Table C-4 gives a typical device-dependent command sequence. In this instance, ATN is true while the instrument is being addressed, but it is set high while sending the device-dependent command string.

Table C-4. Typical Device-Dependent Command Sequence

|  |  |  | Data Bus |  |  |
| :---: | :---: | :--- | :---: | :---: | :---: |
| Step | Command | ATN State | ASCII | Hex | Decimal |
| 1 | UNL | Set low | $?$ | $3 F$ | 63 |
| 2 | LAG* | Stays low | 1 | $2 F$ | 47 |
| 3 | Data | Set high | R | 52 | 82 |
| 4 | Data | Stays high | 0 | 30 | 48 |
| 5 | Data | Stays high | X | 58 | 88 |

*Assumes primary address $=15$.

## IEEE Command Groups

Command groups supported by the Model 590 are listed in Table C-5. Device-dependent commands are not included in this list.

Table C-5. IEEE Command Group

```
HANDSHAKE COMMAND GROUP
    DAC=DATA ACCEPTED
    RFD=READY FOR DATA
    DAV=DATA VALID
UNIVERSAL COMMAND GROUP
    ATN=ATTENTTON
    DCL=DEVICE CLEAR
    IFC=INTERFACE CLEAR
    LLO=LOCAL LOCKOUT
    REN=REMOTE ENABLE
    SPD=SERIAL POLL DISABLE
    SPE=SERIAL POLL ENABLE
ADDRESS COMMAND GROUN
LISTEN: LAG=LISTEN ADDRESS GROUP
    MLA=MY LISTEN ADDRESS
    UNL=UNLISTEN
    TALK: TAG=TALK ADDRESS GROUP
    MTA=MY TALK ADDRESS
    UNT=UNTALK
    OTA=OTHER TALK ADDRESS
ADDRESSED COMMAND GROUP
    ACG=ADDRESSED COMMAND GROUP
    GET=GROUP EXECUTE TRIGGER
    GTL=GO TO LOCAL
    SDC=SELECTIVE CLEAR
STATUS COMMAND GROUP
    RQS=REQUEST SERVICE
    SRQ=SERIAL POLL REQUEST
    STB=STATUS BYTE
    EOI=END
```


## APPENDIX D

## INTRODUCTION

This information will help you use the Model 590 with the Keithley Model 8573A IEEE－488 interface．The Model 8573A interfaces the IBM PC，XT，and AT computers（and cer－ tain IBM compatibles such as the Compaq）to the IEEE－488 bus．Information presented here is necessarily brief in nature，for more complete information，consult the Model 8573A Instruction Manual．

## PROGRAMMING STATEMENT SUMMARY

An abridged listing of Model 8573A programming state－ ments is given in Table on the next page．More complex applications may require other programming statements， as discussed in the Model 8573A Instruction Manual．

## SOFTWARE CONFIGURATION

Before using Model 8573A programs，you must configure the software using the procedure below．This procedure assumes that you will be using the Model 590 with its primary address at the default value of 15 ．

1．Build a working disk as discussed in the Model 8573A Instruction Manual．Among other files，this diskette must include the GPIB．COM，BIB．M，and CONFIG．SYS files，as discussed in that manual．
2．Boot up the computer using the working disk discussed in step 1 above and enter BASICA．
3．Load the Model 8573A declaration file called ＂DECL．BAS＂．Modify the program by changing the

XXXXX values as described in the Model 8573A Instruc－ tion Manual．
4．Delete lines 7－99 and add the following lines to the declaration file．



5．Now save this modified declaration file for use with BASIC programs you write．Remember that this modified file must appear at the front of every program．

Progamming Example－The program below will allow you to send simple device－dependent command strings for the Model 590．Keep in mind that the statements in the modified declaration file discussed above must be includ－ ed at－the front of every program．

| PROGRAM | COMMENTS |
| :---: | :---: |
| 10 U\％＝1：CALL IBSRE <br> （ERLDK：NK） | Set REN true． |
|  | Prompt for command string． |
| 30］CALL IBART（4590\％，［车） | Send command string to 590 ． |
| 408\＄＝SPACEs（100） | Define reading input buffer． |
| 50 CALL IBRIM M590\％，「朿） | Get reading string from 590. |
| 6G FRIHT R＊ 70GOTO20 | Display reading string． Repeat． |

## Table D-1.

| Model 8573A Statement | Description | Equivalent HP-85 Statement* |
| :---: | :---: | :---: |
| CALL IBMRT (M5901: ${ }^{\text {A }}$ ) | Send string to unit. | OLITPUT 715; $\mathrm{A}^{\text {a }}$ |
|  | Input string from unit. | EHTER 715; ${ }^{\text {a }}$ |
| CALL IBLOC (M590\%) | Send GTL to 590. | LOCAL 715 |
| CALL IBCLE(M590\%) | Send SDC to 590. | CLEAR 715 |
|  | Send DCL to all devices. | CLEAR 7 |
| W\%=1:CALL IBSRE (ERD6\%, W\%) | Set REN true. | REMOTE ? |
| U\%=0:CALL IBSRE (ERIWh, Wh) | Set REN false. | LOCAL 7 |
| CALL I BRSP (M59日\%, 5 BK ) | Serial poll unit. | SFOLL¢ 715 ) |
|  | Send local lockout. | LIDCAL LOCKOUT 7 |
| CALL IBTRG(4590\% | Send GET to device. | TRIGEER 715 |
| DALL IBSIC (BRD日\%) | Send IFC. | AEORTIO 7 |

*Assumes interface select code 7, primary address 15 .

## APPENDIX E

EQUIVALENT IEEE-488 COMMANDS FOR FRONT PANEL KEYS

| Front Panel Key | $\begin{gathered} \text { IEEE-488 } \\ \text { Command(s) } \\ \hline \end{gathered}$ |
| :---: | :---: |
| RANGE | R |
| FREQ | F |
| MODEL | O |
| FILTER | P |
| RATE | S |
| ZERO | Z |
| CAL | Q0 |
| TRIGGER MODE/SOURCE | T |
| BIAS ON | N |
| WAVEFORM | W |
| PARAMETER | W, V |
| PLOT | A0 |
| GRID | A1 |
| SETUP | A2-A8 |
| BUFFER | B1, B2 |
| A $\rightarrow$ B | B3 |
| CABLE CAL | IO, C1 |
| CABLE \# | CO |
| SELF TEST | J |
| SAVE | L1 |
| RECALL | L0 |
| $1 / C^{2}$ | O4 |
| $\mathrm{C} / \mathrm{C}_{0}$ | O5 |
| $\mathrm{C}_{\text {max }}$ | U16, U19 |
| $\mathrm{C}_{A}-\mathrm{C}_{B}$ | O6 |
| $\left[\mathrm{V}_{A} \mathrm{~V}_{B}\right] \mathrm{C}=\mathrm{CONST}$ | 07 |
| C vs t | U8, U15 |

## APPENDIX F

Worksheet \#1

| Operating Mode | Setup 0 | Setup 1 | Setup 2 | Setup 3 | Setup 4 | Setup 5 | Setup 6 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Range |  |  |  |  |  |  |  |
| Frequency |  |  |  |  |  |  |  |
| Filter |  |  |  |  |  |  |  |
| Rate |  |  |  |  |  |  |  |
| Zero |  |  |  |  |  |  |  |
| Trigger Source |  |  |  |  |  |  |  |
| Trigger Mode |  |  |  |  |  |  |  |
| Bias on/off |  |  |  |  |  |  |  |
| Waveform |  |  |  |  |  |  |  |
| Start Time |  |  |  |  |  |  |  |
| Stop Time |  |  |  |  |  |  |  |
| Step Time |  |  |  |  |  |  |  |
| First Bias |  |  |  |  |  |  |  |
| Last Bias |  |  |  |  |  |  |  |
| Step Bias |  |  |  |  |  |  |  |
| Default Bias |  |  |  |  |  |  |  |
| Count |  |  |  |  |  |  |  |

## Worksheet \#2

| Operating Mode | Setup 0 | Setup 1 | Setup 2 | Setup 3 | Setup 4 | Setup 5 | Setup 6 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Range |  |  |  |  |  |  |  |
| Frequency |  |  |  |  |  |  |  |
| Filter |  |  |  |  |  |  |  |
| Rate. |  |  |  |  |  |  |  |
| Zero |  |  |  |  |  |  |  |
| Trigger Source |  |  |  |  |  |  |  |
| Trigger Mode |  |  |  |  |  |  |  |
| Bias on/off |  |  |  |  |  |  |  |
| Waveform |  |  |  |  |  |  |  |
| Start Time |  |  |  |  |  |  |  |
| Stop Time |  |  |  |  |  |  |  |
| Step Time |  |  |  |  |  |  |  |
| First Bias |  |  |  |  |  |  |  |
| Last Bias |  |  |  |  |  |  |  |
| Step Bias |  |  |  |  |  |  |  |
| Default Bias |  |  |  |  |  |  |  |
| Count |  |  |  |  |  |  |  |

Worksheet \#3

| Operating Mode | Setup 0 | Setup 1 | Setup 2 | Setup 3 | Setup 4 | Setup 5 | Setup 6 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Range |  |  |  |  |  |  |  |
| Frequency |  |  |  |  |  |  |  |
| Filter |  |  |  |  |  |  |  |
| Rate |  |  |  |  |  |  |  |
| Zero |  |  |  |  |  |  |  |
| Trigger Source |  |  |  |  |  |  |  |
| Trigger Mode |  |  |  |  |  |  |  |
| Bias on/off |  |  |  |  |  |  |  |
| Waveform |  |  |  |  |  |  |  |
| Start Time |  |  |  |  |  |  |  |
| Stop Time |  |  |  |  |  |  |  |
| Step Time |  |  |  |  |  |  |  |
| First Bias |  |  |  |  |  |  |  |
| Last Bias |  |  |  |  |  |  |  |
| Step Bias |  |  |  |  |  |  |  |
| Default Bias |  |  |  |  |  |  |  |
| Count |  |  |  |  |  |  |  |

## Worksheet \#4

| Operating Mode | Setup 0 | Setup 1 | Setup 2 | Setup 3 | Setup 4 | Setup 5 | Setup 6 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Range |  |  |  |  |  |  |  |
| Frequency |  |  |  |  |  |  |  |
| Filter |  |  |  |  |  |  |  |
| Rate |  |  |  |  |  |  |  |
| Zero |  |  |  |  |  |  |  |
| Trigger Source |  |  |  |  |  |  |  |
| Trigger Mode |  |  |  |  |  |  |  |
| Bias on/off |  |  |  |  |  |  |  |
| Waveform |  |  |  |  |  |  |  |
| Start Time |  |  |  |  |  |  |  |
| Stop Time |  |  |  |  |  |  |  |
| Step Time |  |  |  |  |  |  |  |
| First Bias |  |  |  |  |  |  |  |
| Last Bias |  |  |  |  |  |  |  |
| Step Bias |  |  |  |  |  |  |  |
| Default Bias |  |  |  |  |  |  |  |
| Count |  |  |  |  |  |  |  |

Worksheet \#5

| Operating Mode | Setup 0 | Setup 1 | Setup 2 | Setup 3 | Setup 4 | Setup 5 | Setup 6 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Range |  |  |  |  |  |  |  |
| Frequency |  |  |  |  |  |  |  |
| Filter |  |  |  |  |  |  |  |
| Rate |  |  |  |  |  |  |  |
| Zero |  |  |  |  |  |  |  |
| Trigger Source |  |  |  |  |  |  |  |
| Trigger Mode |  |  |  |  |  |  |  |
| Bias on/off |  |  |  |  |  |  |  |
| Waveform |  |  |  |  |  |  |  |
| Start Time |  |  |  |  |  |  |  |
| Stop Time |  |  |  |  |  |  |  |
| Step Time |  |  |  |  |  |  |  |
| First Bias |  |  |  |  |  |  |  |
| Last Bias |  |  |  |  |  |  |  |
| Step Bias |  |  |  |  |  |  |  |
| Default Bias |  |  |  |  |  |  |  |
| Count |  |  |  |  |  |  |  |

## APPENDIX G

ENGINEERING UNITS AND SCIENTIFIC NOTATION CONVERSION

| Engineering Symbol | Prefix | Scientific Notation |
| :---: | :---: | :---: |
| femto- | f | $10^{-15}$ |
| pico- | p | $10^{-12}$ |
| nano- | n | $100^{-9}$ |
| micro- | $\mu$ | $10^{-6}$ |
| milli- | m | $10^{-3}$ |
| kilo- | k | $10^{0^{3}}$ |
| mega- | M | $10^{6}$ |
| giga- | G | $10^{9}$ |
| tera- | T | $10^{12}$ |
| peta- | P | $10^{15}$ |

Abort-To terminate or break off an operation.
Accuracy-The maximum error in terms of measurement made by an instrument. For digital instruments, accuracy is usually specified as a percent of reading plus so many counts of error.

A/D (Analog-to-Digital) Converter-A device that changes an analog signal into binary or digital values.

Analog-Pertaining to electronic devices in which the output varies as a continuous function of the input.

Analog Output-An output that provides an analog signal derived from the digital information within the instrument.

ASCII-Abbreviation for American Standard Code for Information Interchange (pronounced ask-ee). A standard code used extensively in computers and data transmission in which 128 letters, numbers, symbols, and special control characters are represented by 7 -bit binary numbers.

BASIC-Abbreviation for Beginners All-purpose Symbolic Instruction Code. A high-level programming language used in many small computers.

Bias Voltage-A voltage applied to a semiconductor for the purpose of establishing a reference level for the operation of the device during testing.

Binary-A number system based on the number 2; used extensively in computer-based equipment.

Bit-An abbreviation for binary digit. A unit of binary information is equal to one binary decision, or the designation of one of two possible states, generally represented by 1 and 0 .

BNC-A type of coaxial connector used in situations requiring shielded cable for signal connections.

Buffer-A dedicated area of memory in which some form of binary data is stored for later access. The two Model 590 buffers each store 450 words of capacitance, conductance, and bias voltage information.

Bus-In computerized equipment, one or more conductors used as a path over which information is transmitted from any of several sources to any of several destinations.

Byte-A group of bits processed together in parallel; by definition a byte is made up of eight bits.

Capacitance-Abbreviated C. In a capacitor or a system of conductors and dielectrics, that property which permits the storage of electrically separated charges when potential differences exist between the conductors. Capacitance is related to charge and voltage as follows: $C=Q / V$, where $C$ is the capacitance in farads, $Q$ is the charge in coulombs, and $V$ is the voltage in volts.

Chassis Ground-A connection to a common metal structure within the instrument. Generally, chassis ground is connected through power line ground to earth ground via a 3-wire power cord for safety purposes.

Clock-A pulse generator or signal waveform used to achieve synchronization of digital circuits.

Coaxdal Cable-A cable in which one conductor completely surrounds the other, the two being coaxial and separated by continuous solid dielectric.

Conductance-Abreviated G. The reciprocal (1/R) of resistance, usually specified in Siemens (S).

Command-A signal, originating within a computer, that triggers or initiates some form of action within the instrument.

Common Mode Voltage-A voltage applied between input low and chassis ground of the instrument.

Complex Waveform-A periodic waveform made up of a combination of several frequencies or several sine waves superimposed on one another.

Controllex-A device which governs the operation of the IEEE-488 bus; generally a controller is a small computer or microcomputer.

Count-The minimum step size that an instrument display can resolve. Display size is often defined in counts, as in a 20,000 count display.

CRT-Cathode Ray Tube. A term generally used when referring to a computer or terminal display screen.

Cursor-A brightened display digit or segment used to indicate the next digit affected by data entry.

DAC-Abbreviation for Digital-to-Analog Converter. A device which converts digital or binary information into an analog signal.

Data Entry-The process of keying in data from the front panel using the numeric keys.
$\mathrm{dB}-\mathrm{Abbreviation}$ for decibel, which is a logarithmic unit used to measure and compare voltage, current, and power levels.

Digital-Circuitry in which the data-carrying signals are restricted to one of two voltage levels. These voltage levels are used to represent the binary values 1 and 0 .

Digitize-To convert an analog signal into a series of binary numbers representing its amplitude at discrete intervals of time.

Earth Ground-A connection from an electrical circuit or instrument to the earth through a water pipe or metal rod driven into the ground.

EMI-Abbreviation for Electromagnetic Interference. A term that defines unwanted electromagnetic radiation from a device which could interfere with desired signals in electronic receiving equipment such as television and radio. RFI (Radio Frequency Interference) and EMI are often used interchangeably.

GPIB-Abbreviation for General Purpose Interface Bus. Another term for the IEEE-488 bus.

Hexadecimal-A number system based on the number 16 that uses values $0-9$, and $A$ through $F$ to represent the 16 possible values of a 4 -bit binary number. Hexadecimal numbers are represented by preceding them with a $\$$ or following them with a letter H . Thus, $\$ 7 \mathrm{~F}$ and 7 FH would be equivalent.

IC-Abbreviation for Integrated Circuit. A combination of interconnected circuit elements inseparably contained on or within a single substrate.

IEEE-488 Bus-A parallel instrumentation data and control bus standardized by the Institute of Electrical and Electronic Engineers.

I/O-Abbreviation for input/output,- which refers to the transmission of information from an instrument to an external device (output), or the transfer of information from an external device to an instrument (input).
$\mathrm{K}-\mathrm{Abbreviation} \mathrm{for} \mathrm{kilo} .\mathrm{In} \mathrm{computer} \mathrm{terms}$,1 K equals 1024. For example, a 16 K byte memory has 16,384 bytes.

LED-Light-Emitting Diode. A PN junction diode that emits light when forward biased. LEDs are used in front panel annunciators as well as the individual segments of numeric displays on instrumentation.

Listener-A device which, when connected to the IEEE-488 bus, is capable if receiving information over that bus.

Microprocessor-The control and processing portion of a small computer, microcomputer, or computerized device, which is usually contained within one LSI (Large Scale Integration) IC.

Module-A complete subassembly of the instrument combined in a single package (for example, a 5901100 kHz CV module).

Noise-Any unwanted signal appearing in an electronic device.

Normal Mode Voltage-A voltage applied between the input high and input low terminals of an instrument.

NVRAM-Abbreviation for Non-volatile Random Access Memory. A special type of electrically alterable ROM that is used to store information such a calibration constants on a semi-permanent basis. Stored information is retained when power is removed from the device.

Parallel-The simultaneous storage, transmission, or logical operation on a group of bits at one time.

Periodic Waveform-An electronic waveform that repeats itself regularly in time and form.

Plotter-A device that produces an inscribed display of the variation of a dependent variable ( Y axis) as a function of an independent variable ( X axis).

Programmable Instrument-An instrument whose operation can be determined by keystroke sequences entered from the front panel or with commands sent over the IEEE-488 bus.

RAM-Abbreviation for Random Access Memory. A type of memory where information can be stored (written) and accessed (read). RAM memory is usually volatile, meaning that data is lost when the power is turned off.

Random Access-Access to any location in instrument memory where each location can be accessed in the same amount of time.

Reading-A group of data consisting of capacitance, conductance and measured bias voltage. The result is then shown on the front panel display, stored in buffer, or sent over the IEEE-488 bus.

Resolution-The smallest increment of change in voltage that can be detected by the instrument.

ROM-Abbreviation for Read Only Memory. A type of memory which permanently stores program information for a microprocessor. ROM memory is non-volatile, which means that programmed information remains intact after power is removed.

Sequential Access-Serial access to instrument memory where lower or higher memory locations must be passed through before reaching the desired location.

Serial-The technique for handling a binary data word which has more than one bit. The bits are processed one at a time in single-file sequence.

Sinusoidal-Varying in proportion to the sine of an angle or time function (for example, ordinary alternating current).

Software-The program instruction coding within an instrument or computer that makes the unit operate.

Talker-A device that can transmit information over the IEEE-488 bus.

Transfer Standard-An accurate value used to calibrate an instrument. The accuracy of the standard is generally traceable to a known standard for the unit in question.

Transient Waveform-An electronic signal that results in a sudden change in circuit conditions which persists only for a brief period of time.

Translator Mode-A mode which allows English-like words to be used in place of instrument bus commands.

Trigger-A stimulus of some sort that initiates a one shot, single sweep, or continuous reading sequence, depending on the selected trigger mode. Trigger stimuli include: front panel, an external trigger pulse, and IEEE- 488 bus $X$, talk, and GET triggers.

Word-A group of characters stored in one location in a computer or computerized device. Generally, a word is made up of two or more bytes.

Zero-A mode that allows a baseline measurement to be subtracted from subsequent-measurements.

## APPENDIX I

BASIC 2.0/4.0 PROGRAM CONVERSIONS

All example programs included in this manual are written in HP-85 BASIC. The syntax used by other Hewlett-Packard computers running under BASIC 2.0 or BASIC 4.0 ( 9816,9826 and 9836) is very similar. However, there are a few differences between these programming languages, as indicated below.

Table I-1. HP-85 and BASIC 2.0/4.0 Programming Language Differences

| HP-85 Statement | BASIC 2.0(4.0) <br> Equivalent Statement(s)* | Comments |
| :---: | :---: | :---: |
| clear |  | Clear screen, home cursor |
| IISF | PRINT | Display variables or literals on CRT. |
| EHABLE INTR 7; 8 | EHABLE INTR 7: 2 | Enable SRQ interrupt |
| STATUS 7: 1 ; 5 | STATUS 7:5:5 | Clear SRQ interrupt |
| DISP:"MESSAGE" " IHPUT A | IHFUT "MESSAGE" ${ }^{\text {ch }}$ | Prompt for and input variable. |
| IF . . THEN. . ELSE. | IF . . THEN. | Conditional branching |
|  | ELSE. |  |
| ABORTIO 7 | EHIIIF <br> ABDRT 7 | Send IFC |

*Used by HP-9816, 9826 and 9836.

| Execute (X) |  |
| :--- | :--- |
| X | Execute Commands |
|  |  |
|  |  |
| Frequency ( F ) |  |
| F0 | 100 kHz |
| F1 | 1 MHz |
| F2 | Disconnect test signal |


| Range (R) |  |  |
| :---: | :---: | :---: |
|  | 100kHz | 1 MHz |
| RO | Autorange on | Autorange on |
| R1 | $2 \mathrm{pF} / 2 \mu \mathrm{~S}$ | 20pF/200 ${ }^{\text {S }}$ S |
| R2 | 20pF/20 $/ \mathrm{S}$ | 20pF/2004 |
| R3 | 200pF/2004S | $200 \mathrm{pF} / 2 \mathrm{~ms}$ |
| R4 | $2 \mathrm{nF} / 2 \mathrm{mS}$ | $2 \mathrm{nF} / 20 \mathrm{~ms}$ |
| R5 | R1 $\times 10$ on | Error |
| R6 | R2 $\times 10$ on | Error |
| R7 | R3 $\times 10$ on | Error |
| R8 | R4 $\times 10$ on | Error |
| R9 | Autorange off, stay on range |  |


| Reading Rate (S) |  |
| :--- | :--- |
| S0 | $1000 / 3 e \mathrm{c}, 31 / 2$ digits |
| S1 | $75 / \mathrm{sec}, 31 / 2$ digits |
| S2 | $18 / \mathrm{sec}, 41 / 2$ digits |
| S3 | $10 / \mathrm{sec}, 41 / 2$ digits |
| S4 | $1 / \mathrm{sec}, 41 / 2$ digits |

NOTE: Reading rates are nominal

| Trigger (T) |  |
| :--- | :--- |
| T0,0 | One-shot on talk |
| T0,1 | Sweep on talk |
| T1,0 | One-shot on GET |
| $T 1,1$ | Sweep on GET |
| $T 2,0$ | One-shot on X |
| $T 2,1$ | Sweep on X |
| $T 3,0$ | One-shot on external pulse |
| $T 3,1$ | Sweep on external pulse |
| $T 4,0$ | One-shot on front penel |
| $T 4,1$ | Sweep on front panel |


| Blas Voltage (V) |  |
| :---: | :---: |
| V(first)(,last)(step) (,default)(,count) | First = first bias; Last $=$ last blas; Step =step bias; Default $=$ defautt bias; $-20.000 \leq V \leq 20.000$ $1 \leq$ count $\leq 450$ (1,350 at $1,000 / \mathrm{sec}$ rate) |


| Buffer (B) |  |
| :--- | :--- |
| B0 |  |
| B1(first)(llast) | Current Reading |
| A/D buffer, first, last limits |  |
| B3,first)(liset) | Plot buffer, first, last limits <br> Transfer A/D buffer to plot |


| Waveform (W) |  |
| :---: | :---: |
| W(waveform) (start) (,stop) (step) | Waveform: $0=D C ; 1=$ Single stair; 2=Dual stair; 3=Pulse; 4 = Externa;; Start = start time; Stop $=$ stop time; Step $=$ step time: $1 \mathrm{msec} \leq T \leq 65 \mathrm{sec}$ |

NOTE: Multiply programmed times by 1.024 to obtain actual times.

| Blas Control (N) |  |
| :--- | :--- |
| NO | Blas off <br> N1 |


| Data Format (G) |  |
| :--- | :--- |
| G0 | Prefix on, suffix off, 1rdg <br> G1 |
| G2 | Prefix off, suffix off, 1 rdg |
| G3 | Prefix on, suffix on, 1 rofg |
| G4 | Prefix off, n rdgs |
| G5 off, suffix off, n rdgs |  |
|  | Prefix on, suffix on, n rdgs |
|  | n rdgs = \# reedings in buffer |


| Operation (0) |  |
| :---: | :---: |
| Ooutput(,model) $\left(, C_{0}\right)$ | Output: $0=\mathrm{C}, \mathrm{G}, \mathrm{V}$ (triple); <br> $1=\mathrm{C}$ onty; $2=\mathrm{G}$ only; <br> $3=V$ only; $4=1 / C^{2} ; 5=C / C_{0}$; <br> $6=\mathrm{C}_{A}-\mathrm{C}_{\text {n }} ; 7=\left[\mathrm{V}_{A}-\mathrm{V}_{\mathrm{B}}\right]_{\text {consr. }}$. <br> Model: $0=$ Parallet; $1=$ Series. <br> $\mathrm{C}_{0}$ (used with $\mathrm{C} / \mathrm{C}_{0}$ : <br> $0 \leq C_{0} \leq 20 E-9$ |



| Zero $(\mathbf{Z})$ |  |
| :--- | :--- |
| $Z 0$ | Disable zero <br> Enable zero |


| Filter (P) |  |
| :--- | :--- |
| P0 | Filter off <br> Filter on |


| Status (U) |  |
| :---: | :---: |
| U0 | Hardware/software revision |
| U1 | Error information |
| U2 | Buffer A range group |
| U3 | Buffer A trigger group |
| U4 | Buffer A zero group |
| U5 | Buffer A bias group |
| U6 | Buffer A bias voltage |
| U7 | Buffer A blas time |
| U8 | Buffer A position and time |
| U9 | Buffer B range group |
| U10 | Buffer B trigger group |
| U11 | Buffer B zero group |
| U12 | Buffer B bias group |
| U13 | Buffer B blas voltage |
| U14 | Buffer 8 bias time |
| U15 | Buffer B position and times |
| U16 | Buffer A maximum/minimum capacitance |
| 017 | Buffer A maximum/minimum conductance |
| U18 | Buffer A maximum/minimum voltage |
| U19 | Buffer B maximum/minimum capacitance |
| U20 | Buffer B maximum/minimum conductance |
| U21 | Buffor 8 maximum/minimum voltage |
| U22 | Ghobal parameters (series/parallel, $\mathrm{C}_{0}$ value) |
| U23 | Plotter parameters (plot, grid, line, etc.) |
| U24 | IEEE output parameters ( $\mathrm{O}, \mathrm{G}$, $B, Y, K)$ |
| U25 | IEEE input parameters (L, C, H , K, M) |
| U26 | Cable correction parameters |
| U27 | Translator user name list |
| U28 | Not used |
| U29 | Transtator reserved word list |
| U30 | Transtator NEW/OLD state |
| U31 | Translator user transtation ist |
| U32 | Not Used |


| SRO (M) |  |
| :--- | :--- |
| M0 | Disabled |
| M1 | Reading overflow |
| M2 | Module input overload |
| M4 | Sweep dons |
| M8 | Reading done |
| M16 | Ready |
| M32 | Error |
| M128 | IEEE output done |


| Save/Recall (L) |  |
| :--- | :--- |
| LO,n | Recall configuration $n$ <br> $(0 \leq n \leq 7)$ <br> Save conflguration $n(1 \leq n \leq 7)$ |


| Cable Parameters (1) |  |
| :---: | :---: |
| 10 | Measure cable parameters (driving point) |
| 11, n1, n2, n3, n4 | Assign cable parameters $K 0(n 1+j n 2), K 1(n 3+j n 4)$ |
| 12, n1, n2, n3, n4, | Assign test output cable parameters: $A(n 1+j n 2)$, Bin $3+i n 4$ ), |
| $n 5, n 6, n 7, n 8$ | $\mathrm{C}(\mathrm{n} 5+\mathrm{j} n 6), \mathrm{D}$ (n77+jn8) |
| 13, n1, n2, n3, n4 | Assign test INPUT cable parameters: $A(n 1+j n 2)$, |
| n5, n6, n7, n8 | $B(n 3+\ln 4), C \ln 5+j n 6)$ |
|  | $\mathrm{D}(\mathrm{n} 7+\mathrm{jn} 8)$ |
| 14 | Zero cable open |
| $15, C, G$ | Measure source parameters, step 1 |
| $16, C, G$ | Measure source parameters, step 2 |



| Calibration (Q) |  |
| :--- | :--- |
| Q0 | Drift correction |
| Q1 | NORMAL. MODE |
| Offsets |  |
| Q3, C, G | First capacitance cas point |
| Q4, C, G | Second capacitance cal point |
|  | Conductance cal point |
| Q5 | DRIVING POINT MODE |
| Q6, C, G | Offsets |
| Q7, C, G | First capacitance cal point |
| Q8 | Second capacitance cal point |
| Q9, V | Voltage calibration offsets |
|  | Calibrate voltmeter gain |


| Terminator (Y) |  |
| :--- | :--- |
| Y 0 | $\langle\mathrm{CR}\rangle\langle\mathrm{LF}\rangle$ |
| Y 1 | $\langle\mathrm{LF}\rangle\langle\mathrm{CR}\rangle$ |
| Y 2 | <CR $\rangle$ |
| Y 3 | $\langle\mathrm{LF}\rangle$ |


| EOI and Hoid-off (K) |  |
| :--- | :--- |
| K0 | EOI and hold-off enabled |
| K1 | EOI disabled, hoid-off enabied |
| K2 | EOI enabled, hold-off disabled |
| K3 | EOI and hold-off disabled |


| Display (D) |  |
| :--- | :--- |
| Dsaa | Display ASCll characters aa <br> (20 max) <br> Return display to normal |


| Hit Button (H) |  |
| :--- | :--- |
|  | Emulate button press: |
| H12 | SHIFT |
| H15 | ENTER |
| H16 | (A~B) |
| H20 | ON |
| H23 | MANUAL |
| H25 | ZERO |
| H26 | CAL |
| H27 | FILTER |
| H29 | RANGE |
| H30 | FREQ |
| H31 | MODEL |

## Service Form

| Serial No. |  | Date |
| :---: | :---: | :---: |
| Name and Telephone No. |  |  |
| Company |  |  |
| List all controi settings, describe problem and check boxes that apply to problem. |  |  |
| $\square$ Intermittent | Analog output follows display | $\square$ Particular range or function bad; specify |
| IEEE failure Front panel operational | Obvious problem on power-up <br> All ranges or functions are bad | $\begin{aligned} & \text { Batteries and fuses are OK } \\ & \text { Checked all cables } \end{aligned}$ |
| Display or output (check one) |  |  |
| Drifts Unstable Overload | Unable to zero <br> Will not read applied input |  |
| Calibration only Certificate of cailibration requiredData required |  |  |
| Show a block diagram of yo Also, describe sigral source. | easurement system including all instr | ts cornected (whether power is turned on or |

Where is the measurement being performed? (factory, controlled laboratory, out-of-doors, etc.)

What power line voltage is used? $\qquad$ Ambient temperature?

Relative humidity? $\qquad$ Other? $\qquad$
Any additional information. (If special modifications have been made by the usex, please describe.)

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[^0]:    Programming 1区 OUTPUT P15; "IPRESSwKETK" ! Display PRESS KEY message. Examples za OUTFUT 715; "IHADEL*S90x": ! Display MODEL 590 message.

[^1]:    *This range applicable only to Model 5904 Input Adapter.
    **Using Keithley Model 5905 or 5906 conductance sources.

[^2]:    *Capacitance and conductance values must be characterized and traceable to known standards. To maintain capacitance linearity specifications, use of Model 5905 and 5906 sources is recommended.
    **Although two DMMs are preferred, procedure may be performed with only one.

[^3]:    * Message sent or received with ATN true.

[^4]:    * Message sent or received with ATN true. Numbers shown represent primary address resulting in MLA (My Listen Address).

[^5]:    * Message sent or received with ATN true. Numbers shown are primary address resulting in MTA (My Talk Address).

[^6]:    *Don't Care.

[^7]:    'PPC (PARALLEL POLI CONFGURE). PPU (PARALLEL POLL UNCONFIGURE) AND
    TCT (TAKE CONTROL) NOT MMPEMENTED EY MODEL 590
    

